

Development Team Review Comments

The following comments have been provided by reviewers of your land use application. At this time, a resubmittal of your application is required before this case is ready to be scheduled for public hearing.

To prepare your resubmittal, you will be expected to provide:

- A response to each comment with a description of the revisions and the page of the response on the site plan;
- Any revised plans or renderings; and
- A list identifying any additional changes made to the original submission other than those required by staff.

Resubmittal documents must be provided electronically through e-mail or a flash drive delivered to the One-Stop Customer Service Center. The following items will be expected by our One-Stop Customer Service Center:

- One digital copy of all new materials
 - All digital materials shall be in a single PDF document
 - o The single PDF document shall be bookmarked
 - If a Subdivision Improvements Agreement, Legal Description, or Development Agreement is required, then an additional Microsoft Word version of these documents shall also be provided
 - Electronic copies can be emailed to <u>epermitcenter@adcogov.org</u> as a PDF attachment. If the files are too large to attach, the email should include an unlocked Microsoft OneDrive link. Alternatively, the resubmittal can be delivered to the One-Stop counter on a flash drive.

Community & Economic Development Department www.adcogov.org



4430 South Adams County Parkway 1st Floor, Suite W2000 Brighton, CO 80601-8204 PHONE 720.523.6800 FAX 720.523.6998

Re-submittal Form

| Ca | ase Name/ Number: |
|------|---|
| Ca | se Manager: |
| Re | e-submitted Items: |
| | Development Plan/ Site Plan |
| | Plat |
| | Parking/ Landscape Plan |
| | Engineering Documents |
| | Subdivision Improvements Agreement (Microsoft Word version) |
| | Other: |
| * Al | l re-submittals must have this cover sheet and a cover letter addressing review comments. |
| Ple | ease note the re-submittal review period is 21 days. |
| Th | e cover letter must include the following information: |
| | Restate each comment that requires a response |
| | • Provide a response below the comment with a description of the revisions |
| | • Identify any additional changes made to the original document |
| Γ | For County Use Only: |
| | Date Accepted: |
| | Staff (accepting intake): |
| | Resubmittal Active: Engineering; Planner; Right-of-Way; Addressing; Building Safety; |
| | Neighborhood Services; Environmental; Parks; Attorney; Finance Plan Coordination |

Community & Economic Development Department www.adcogov.org



4430 South Adams County Parkway 1st Floor, Suite W2000B Brighton, CO 80601-8218 PHONE 720.523.6880 FAX 720.523.6967 EMAIL: epermitcenter@adcogov.org

Development Review Team Comments

Date: 5/9/2024 Project Number: PLT2023-00056 Project Name: Berkeley Center Subdivision

Commenting Division: Plan Coordination 2nd Review Name of Reviewer: David DeBoskey Date: 05/09/2024 Email: Resubmittal Required

BOARD OF COUNTY COMMISSIONERS

Charles "Chaz" Tedesco DISTRICT 2 Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4

Commenting Division: Planner Review 2nd Review

Name of Reviewer: David DeBoskey

Date: 05/09/2024

Email:

Resubmittal Required

2nd Review

PLN3: Rezoning application has not been applied for within our system yet, which is fine, but we recommend t it is applied for during this subdivision review process (before the subdivision goes to it's hearings). If not, it will impact the subdivision criteria of approval. This can start a the same time as the next submittal of this application.KH RESPONSE: Noted, thank you. To be submitted after the submittal of the subdivision construction documents.

PLN5: Proposed lot line that zig zags separating lots 3 & 4 also creates mixed zoning on proposed parcels. When selecting new zones, please be sure that the proposed lots meet the minimum lot size and widths of the proposed zones. KH RESPONSE: Minimum lot size for both I-2 and C-5 have been verified and

all lots meet minimum size requirements.

PLN9:Now that the Subdivision Engineering Review has been initiated, the SIA and those particulars will mostly be initiated and dictated by that review but will be apart of this review near the agreement's completion. So, look out for that within that review. KH RESPONSE: Noted, thank you.

PLN10: FYI: Public Land Dedication fee estimate cannot be accurately completed because of split zoning on site, but it is required prior to hearings. KH RESPONSE: Noted, thank you.

PLN11: In CDOT's letter they wanted to review aspects of the development: the Drainage Study, and the Traffic Study. When you coordinated with CDOT, did you send them those? We can, if you did not. We want to make sure they have no concerns given the project's close proximity to CDOT roadways.

KH RESPONSE: We have reviewed and addressed CDOT's comments. Adams County to forward submittal documents to CDOT.

PLN12: Attached is a letter from Xcel Energy that was not given earlier during the first staff comment packet, I apologize for not getting this to you when it came in. They are requesting a 10ft dry utility easement along the perimeter and their plat note.

KH RESPONSE: Active coordination occurring with Xcel over easement.

Commenting Division: ROW Review 2nd Review

Name of Reviewer: David Dittmer

Date: 05/07/2024

Email:

Resubmittal Required

ROW1: Within the Dedication Statement revise to read:SUBDIVIDED THE SAME INTO LOTS AND A TRACT...the purpose statement provides the rest of the information. KH RESPONSE: Updated.

ROW2: Need to provide a NOTE as to ownership and maintenance of the TRACT, and it's use. Include this in a Land Use Chart that provides the lot sizes, the tract size and total gr ac. (this was on previous submittals and was removed) (Move the TRACT TABLE from sheet 3 to sheet 1 as the note) KH RESPONSE: Updated. ROW6: Define the use of the tract on sheet 3. KH RESPONSE: Updated.

Commenting Division: Development Engineering Review 2nd Review

Name of Reviewer: Laurie Clark

Date: 04/23/2024

Email:

Resubmittal Required

ENG1: Submit engineering documents (Drainage Report, Traffic Impact Study, Sediment & Erosion Control Plans and Construction Plans) via email to epermitcenter@adcogov.org, using the Subdivision Engineering Review application found at https://epermits.adcogov.org/submittal-checklists. The engineering documents will be formally reviewed separately from the subdivision case. KH RESPONSE: Submitted per direction.

Commenting Division: Application Intake 2nd Review

Name of Reviewer: Rayleen Swarts

Date: 04/18/2024

Email:

Complete

BOARD OF COUNTY COMMISSIONERS

Charles "Chaz" Tedesco DISTRICT 2 Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4 Lynn Baca District 5 Commenting Division: Planner Review Name of Reviewer: David DeBoskey Date: 02/02/2024 Email: Resubmittal Required

- BOARD OF COUNTY COMMISSIONERS

Eva J. Henry DISTRICT 1 Charles "Chaz" Tedesco DISTRICT 2

Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4 Lynn Baca District 5 PLN1: No action: Application for final plat minor subdivision to create four lots.

PLN2: On submitted project page, it states "Building Permit drawings will be submitted and processed in support of the Project." Can you explain this? We discourage the filing of building permits prior to completion of a subdivision on the same lot. We suggest you wait to file building permits until after the subdivision process is over.

We highly recommend this order of operations for this site: Subdivision, THEN Building permits/Change-In-Use permits. We can talk about this in the RCC meeting.

PLN3: As noted in the previous Conceptual Review Meeting (PRE2023-00049) "the industrially zoned property on the Northeast of the property has a split zoning of Industrial-1(I-1) and Industrial-2 (I-2) zoned property. Sec. 3-07-02 Summary of Dimensional Requirements requires that I-1 properties have at minimum lot size of 1 acre, I-2 properties require a minimum lot size of 2

acres. Additionally, staff would not be supportive of replating a lot with split zoning. Staff recommends rezoning the portion of land zoned I-2 into I-1 to be more in line with the adjacent properties fronting W. 64th Avenue.".. to improve the conformance of the subdivision recommend the following that standad

This will require a Zoning Map Amendment (Rezoning) application, separate from this application but can be 1. processed as this application (once you submit a complete application for that rezoning application) and 2. Can go to hearings simultaneously.

A rezoning is not required, but it is a component of the criteria of the subdvision approval process.

PLN4: The minimum lot size and lot minimums for C-5 (Proposed lots 1,2,3) are 0ft for size and 100 ft for width. Meets standard.

The minimum lot size and lot minimums for I-1 (Proposed lot 4) are 0ft for size and 100 ft for width. Meets standard.

PLN5: If you decide you don't want to rezone that I-2 area and instead want to create another lot with that zoning, you must verify via survey that it would meet minimum lot width. I-2 minimum lot width is 125 feet. County maps indicate that it possibly is not that wide of a potential lot.

Why is the zig zag the lot line?PLN6: This standard is met:5-03-03-06 LOT DEPTH TO WIDTH RATIONo lot shall have an average depth greater than three times the average width unless the lot width is a minimum of four-hundred-twenty-five (425) feet.

PLN7: The signature block on plat should be in this order, top to bottom: OWNER SURVEYOR PLANNNING COMMISSION BOARD OF COUNTY COMMISSIONERS COUNTY ATTORNEY CLERK AND RECORDER

PLN8: The submitted plat indicates the city of Denver multiple times. This is not Denver. Change this all throughout the plat document.

PLN9: Per Sec. 5-02-04 Subdivision Improvement agreement (SIA) will be required at resubmittal

PLN10: Public Land Dedication fees are required in the amount of \$XX.XX. See attached spreadsheet. Do not pay these fees until you are scheduled for public hearing ______7.65 acres but I-2 size is undetermined so PLD fees are uncertain.

PLN11: Crestview Water & Sanitation District has a sanitary sewer main situated on the east property line of the part of the property facing Federal. This sanitary sewer main runs north-south. There is also a meter vault providing water to Pioneer Village Mobile Home Park located in the northeast corner of 63rd and Federal. Potholing will be required for this water service.

BOARD OF COUNTY COMMISSIONERS

Charles "Chaz" Tedesco DISTRICT 2 Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4 Lynn Baca District 5 **Commenting Division:** Planner Review

Name of Reviewer: David DeBoskey Date: 02/02/2024 Email: Comment

BOARD OF COUNTY COMMISSIONERS

Eva J. Henry DISTRICT 1 Charles "Chaz" Tedesco DISTRICT 2

Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4 Lynn Baca District 5 For Future Development NOT for this subdivision.

PLN12: A fuel station is proposed for future development on the south east parcel. What is happening on the other proposed parcels?

PLN13: W. 64th Avenue is a section line, Per section 3-24-07-03-07 Minimum setback from Section line for Commercial-5 zoned lots will require a setback of 100 feet as part of any development on the northern properties. Per section 3-25-07-03-07 & 3-26-07-03-07 Minimum setback from Section line for the industrially zoned lots will require a setback of 145 feet from the section line.

PLN14: When developing the site, look at 4-09-02-04 Automobile Service stations for design standards specific for fuel stations.

PLN15: Per Section 4-19-06-01, All Commercially zoned areas on the site abut a residential neighborhood on the east of the subject property, therefore applicant will need to provide a landscape buffer in order to provide separation between the non-compatible uses.

Additionally, per section 4-19-07-01 Street Frontage Landscaping, applicant will need to landscape the areas along properly lines abutting public road right-of-way using one or a combination of the following landscape options:

1. Option 1: Install a twenty-five (25) foot wide area along the road right-of-way. Within the landscape area, one (1) tree and two (2) shrubs shall be planted per forty (40) linear feet of frontage. Drive aisles shall be counted as zero (0) feet in depth.

2. Option 2: Install a twenty (20) foot landscape area along the road right-of-way. Within the landscape area, one (1) tree and two (2) shrubs shall be planted per forty (40) linear feet of frontage. Drive aisles shall be counted as zero (0) feet in depth.

3. Option 3: Install a ten (10) foot landscape area along the road right-of-way. Within the landscape area, two (2) trees and five (5) shrubs shall be planted per forty (40) linear feet of frontage. Drive aisles shall be counted as zero (0) feet in depth.

4. Option 4: Install a five (5) foot landscape area along the road right-of-way. Within the landscape area, one (1) tree and two (2) shrubs shall be placed per forty (40) linear feet of frontage. A thirty (30) inch high decorative wall or the building shall be located between the parking area and the road frontage. Drive aisles shall be counted as zero (0) feet in depth.

5. Option 5: Install a landscape berm with a two (2) foot minimum average height. The berm shall have a slope of no greater than one (1) foot of rise to every four (4) feet of run. Within the landscape area, one (1) tree and five (5) shrubs shall be planted per sixty (60) linear feet of frontage.

PLN16: Per Section 4-19-07 Minimum Landscape Area: All developments shall be required to landscape a minimum of ten (10) percent of the lot area. At least fifty (50) percent of the required landscape area shall be placed so it abuts adjoining public rights-of-way, excluding alleys and drives.

PLN17: Per Sec. 4-11-01-04 Operational/ Physical compatibility standards, conditions may be imposed upon the approval of development applications when industrial uses are proposed adjacent to residentially zoned or used property to ensure new development will be compatible with existing neighborhood and uses, including, but not limited to, restrictions on:

- 1. Hours of operations and deliveries;
- 2. Location of activities generating potential adverse impacts on adjacent uses such as noise and glare;
- 3. Placement of trash receptacles;
- 4. Location and screening of loading and delivery zones;
- 5. Light intensity and hours of full illumination; and
- 6. Placement and illumination of outdoor vending machines.

Commenting Division: Development Engineering Review

Name of Reviewer: Laurie Clark

Date: 02/01/2024

Email:

Resubmittal Required

ENG1: According to the Federal Emergency Management Agency's January 20, 2016 Flood Insurance Rate Maps (FIRM Panels #08001C0584H and #08001C0592H), the project site is not located within a regulated 100-yr floodplain. A Floodplain Use Permit will not be required.

ENG2: A drainage report and drainage plans in accordance to Chapter 9 of the Adams County Development Review Manual are required to be completed by a registered professional engineer and submitted to Adams County for review and final approval. Drainage design shall have no adverse off-site impacts on neighboring properties or the public ROW.

ENG3: LOW IMPACT DEVELOPMENT (LID) STANDARDS AND REQUIREMENTS Section 9-01-03-14:

All construction projects shall reduce drainage impacts to the maximum extent practicable, and implement practices such as:

- 1. On-site structural and non-structural BMPs to promote infiltration, evapo-transpiration or use of stormwater,
- 2. Minimization of Directly Connected Impervious Area (MDCIA),
- 3. Green Infrastructure (GI),

4. Preservation of natural drainage systems that result in the infiltration, evapo-transpiration or use of stormwater in order to protect water quality and aquatic habitat.

5. Use of vegetation, soils, and roots to slow and filter stormwater runoff.

6. Management of stormwater as a resource rather than a waste product by creating functional, attractive, and environmentally friendly developments.

7. Treatment of stormwater flows as close to the impervious area as possible.

LID shall be designed and maintained to meet the standards of these Regulations and the Urban Drainage and Flood Control District's Urban Storm Drainage Criteria Manual, Volume 3.

ENG4: The applicant is required to complete a traffic trip generation analysis signed and stamped by a professional engineer. If the proposed scope of work shows the use of the site will generate over 20 vehicles per day, then a traffic impact study signed and stamped by a professional engineer will be required.

ENG5: The proposed site improvements are required to go through an engineering review process through the Subdivision application. The developer is required to submit for review and receive approval of all civil site construction plans and reports. Construction documents shall include, at a minimum, onsite and public improvements construction plans, drainage report, traffic impact study. All construction documents must meet the requirements of the Adams County Development Standards and Regulations. The developer shall submit to the Adams County One Stop Customer Center the following: Engineering Review Application, Engineering Review Fee, a copy of all construction documents, plans and reports in PDF format.

Commenting Division: Development Engineering Review

Name of Reviewer: Laurie Clark

Date: 02/01/2024

Email:

Comment

ENG6: Property IS in Adams County MS4 Stormwater Permit area. Because the proposed improvements disturb more than one (1) acre of land, OR are part of a larger development that disturbs over one (1) acre, a Stormwater Quality (SWQ) Permit WILL be required and the applicant would be required to prepare a Stormwater Management Plan (SWMP) using the Adams County ESC Template, and obtain both a County SWQ Permit and a State Permit COR400000. Builder/developer is responsible for adhering to all the regulations of Adams County Ordinance 11 regarding illicit discharge. Applicant is responsible for installation and maintenance of Erosion and Sediment Control BMPs.

ENG7: If the applicant proposes to import greater than 10 CY of soil to this site, additional permitting is required. Per Section 4-04-02-02, of the Adams County Development Standards and Regulations, a Temporary or Special Use Permit is required to ensure that only clean, inert soil is imported into any site within un-incorporated Adams County. A Conditional Use Permit will be required if the importation exceeds 500,000 CY.

ENG8: The developer is required to construct roadway improvements adjacent to the proposed site such as curb, gutter, and sidewalks. Additional roadway improvements will be determined based on the Traffic Impact Study and applicant is required to coordinate with CDOT.

ENG9: A Subdivision Improvements Agreement (SIA) will be required for all public improvements.

ENG10: No building permits will be issued until all public improvements have been constructed, inspected, and preliminarily accepted by the Adams County Public Works Department.

ENG11: The developer is responsible for the repair or replacement of any broken or damaged public infrastructure.

ENG12: All proposed drainage facilities with maintenance access shall be within dedicated easements.

ENG13: The engineering documents for the subdivision must be approved before development of individual lots within the proposed subdivision.

ENG14: Applicant is responsible for additional coordination with CDOT concerning bus corridor requirements for Federal Blvd.

Commenting Division: ROW Review

Name of Reviewer: David Dittmer

Date: 02/01/2024

Email:

Resubmittal Required

ROW1: Remove superfluous information in the Title

ROW2: Add the case number to top right-hand corner of all sheets (PLT2023-00056)

ROW3: Opening statement must be: OWNERSHIP AND DEDICATION CERTIFICATE, followed by the legal as provided, then the new m/b legal for the boundary of the new subdivision.

ROW4: Remove all mention of The City and County of Denver. We are not Denver. Revise all of the dedication statements, execution blocks, etc.

ROW5: Note 4 for the title commitment appears to be in error. The commitment provided is dated 10/12/2023 not 7/17/2023 and do not find the earlier date stated as effective as of that date.

ROW6: Must provide the approved Storm Water Facilities Statement as contained in the application guidelines and checklist.

ROW7: You must have CDOT approval of all access points from Federal Blvd. and county approved access permits on county ROW. If additional ROW dedication is required for either road pending engineering review of the traffic impact to the surrounding infrastructure, it can be dedicated by this plat to the county, and the county will deed to CDOT for anything along Federal.

ROW7: The order of appearance of signature/approval blocks:

OWNER

LIEN HOLDER ACCEPTANCE - If property is under a deed of trust the lien holder must approve the plat. SURVEYOR

PLANNING COMMISSION

BOARD OF COUNTY COMMISSIONERS

COUNTY ATTORNEY'S OFFICE - Approved as to form

ROW8: Must provide an approved dedication statement. See application guidelines and checklist.

ROW9: Revise all dates to current year.

ROW10: Note 4 - Define a US foot per C.R.S. and PLS Bylaws

ROW11: Provide a copy of a recorded Statement of Authority for QuikTrip Corporation or a copy of the operating agreement to verify signatories ability to encumber the corporation.

ROW12: Review line weights. It may be the copy but there appear to be signature lines that are heavier than others.

SHEET 2:

ROW13: Sheet 2 is the existing conditions and parcel lines. Do not provide where the new lots are to be located on this sheet. These parcel lines must be vacated. The parcels must be referenced as to the legal descriptions provided on sheet 1. You must state parcel lines being vacated by this plat.

ROW14: Stay consistent with document citations. See 20' easement citation for book 454, page 55. Name the type of easement. This easement cannot be vacated.

Commenting Division: ROW Review

Name of Reviewer: David Dittmer

Date: 02/01/2024

Email:

Comment

SHEET 3

ROW15: The easements that appear to be missing cannot be vacated by this plat and must remain in place. If needing to vacate these easements, it will be an agreement between the property owner and the owner of the utility easement. Once the vacation has been completed and recorded, cite the vacation reception number. If utilities are installed it will be at the owners expense to move these utilities and provide a new easement. The easement/ROW document cited above is exclusively for sanitary sewer. It can be crossed, but nothing can share the trench. Does the 9' wide drainage easement being dedicated abut the 5' wide utility easement as recorded at B1009567? The new one cannot lay on top of the existing.

ROW16: Use a heavy pen weight to draw attention to vacation and dedication statements.

ROW17: Pending access review and approvals from CDOT, it does not appear each lot will be allowed a separate access. Due to this, an access easement located within a TRACT will be required. This Tract will be owned and maintained by the owners or owners association due to individual ownership of the lots. Any Storm Water Quality facilities, detention area, must be located within a TRACT to be owned and maintained by the owners, or owners association, and dedicated to the county. Access to the detention area must be provided by an access easement. Due to individual ownership of the lots, utility easements must be provided for utilities to serve the individual lots. These should be along the front and rear lot lines, and pending comments from PSCO, side lot line easements may be necessary.

ROW

Commenting Division: Environmental Analyst Review

Name of Reviewer: Megan Grant

Date: 02/01/2024

Email:

Complete

ENV1.The subject parcel is located within the Adams County Mineral Conservation Overlay (MCO) district, the purpose of which is to establish reasonable and uniform limitations, safeguards, and controls for the conservation and wise utilization of natural resources and for rehabilitation of excavated land. Land within this classification is designated as containing commercial mineral deposits in sufficient size parcels and in areas where extraction and rehabilitation can be undertaken while still protecting the health, safety, and welfare of the inhabitants of the area and the County. Although this parcel is located within the MCO district and the parcel is greater than 5 acres, the parcel is previously developed and unlikely to provide a mineral resource of commercial quantity and quality; therefore, the MCO restrictions are exempted in this case.

Commenting Division: Neighborhood Services Review

Name of Reviewer: Cornelia WarnkeDate: 01/24/2024Email:CompleteThere are no open violations at this location at this time. No comment.

Commenting Division:Addressing ReviewName of Reviewer:David DittmerDate:01/11/2024

Email:

Complete

BOARD OF COUNTY COMMISSIONERS

Eva J. Henry DISTRICT 1 Charles "Chaz" Tedesco DISTRICT 2 Emma Pinter DISTRICT 3 Steve O'Dorisio DISTRICT 4 Lynn Baca District 5





1123 West 3rd Avenue Denver, Colorado 80223 Telephone: **303.285.6612** violeta.ciocanu@xcelenergy.com

January 17, 2024

Adams County Community and Economic Development Department 4430 South Adams County Parkway, 1st Floor, Suite W2000A Brighton, CO 80601

Attn: David DeBoskey

Re: Berkeley Center Subdivision, Case # PLT2023-00056

Public Service Company of Colorado's (PSCo) Right of Way & Permits Referral Desk has reviewed the request for **Berkeley Center Minor Subdivision**. Please be advised that Public Service Company has existing natural gas distribution facilities along north property line and overhead electric distribution facilities along north, east, and west property boundaries.

For these *commercial/industrial/retail* lots, and to ensure that adequate utility easements are available within this development and per state statute §31-23-214 (3), PSCo requests that the following language or plat note is placed on the preliminary and final plats for the subdivision:

Ten-foot (10') wide dry utility easements are hereby granted around the perimeter of platted areas <u>including lots</u>, tracts, parcels and/or open space areas. These easements are dedicated to the Adams County for the benefit of the applicable utility providers for the installation, maintenance, and replacement of electric, gas, television, cable, and telecommunications facilities (Dry Utilities). Utility easements shall also be granted within any access easements and private streets in the subdivision. Permanent structures, improvements, objects, buildings, wells, water meters and other objects that may interfere with the utility facilities or use thereof (Interfering Objects) shall not be permitted within said utility easements and the utility providers, as grantees, may remove any Interfering Objects at no cost to such grantees, including, without limitation, vegetation. Public Service Company of Colorado (PSCo) and its successors reserve the right to require additional easements and to require the property owner to grant PSCo an easement on its standard form.

Public Service Company also requests that all utility easements are depicted graphically on the preliminary and final plats. While these easements may accommodate certain utilities to be installed in the subdivision, some additional easements may be required as planning and building progresses.

The property owner/developer/contractor must complete the application process for any new natural gas or electric service, or modification to existing facilities via <u>xcelenergy.com/InstallAndConnect</u>. It is then the responsibility of the developer to contact the Designer assigned to the project for approval of design details.

Additional easements may need to be acquired by separate document. The Designer must contact the appropriate Right-of-Way Agent.

Not ready to apply? Our Builder Developer Representatives can provide you with capacity and process information during the concept phase of a project. Contact us at BDRCO@xcelenergy.com or learn more at Building and Remodeling (xcelenergy.com)

As a safety precaution, PSCo would like to remind the developer to contact Colorado 811 for utility locates prior to construction.

Violeta Ciocanu (Chokanu) Right of Way and Permits Public Service Company of Colorado dba Xcel Energy Office: 303-285-6612 – Email: violeta.ciocanu@xcelenergy.com

BERKLEY CENTER SUBDIVISION CASE NO. PLT2023-00056 A REPLAT OF LOT 1, BLOCK 1, ELLETT SUBDIVISION, LOT 1 BLOCK 1, LEXI PAPPAGEORGE SUBDIVISION AND A PORTION OF THE NORTHWEST 1/4 OF THE NORTHEAST 1/4 OF SECTION 8, ALL LYING WITHIN THE NORTHEAST 1/4 SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST OF THE 6TH PRINCIPAL MERIDIAN, COUNTY OF ADAMS, STATE OF COLORADO PURPOSE STATEMENT: GENERAL NOTES (continued):

THE PURPOSE OF THIS SUBDIVISION REPLAT IS TO COMBINE FIVE (5) INDIVIDUAL PARCELS INTO ONE SUBDIVISION AND CREATE 4 NEW LOTS AND 1 TRACT FOR COMMERCIAL DEVELOPMENT.

CERTIFICATE OF DEDICATION AND OWNERSHIP:

KNOW ALL MEN BY THESE PRESENTS THAT QUIKTRIP CORPORATION. AN OKLAHOMA CORPORATION, BEING THE SOLE OWNER OF THE FOLLOWING DESCRIBED TRACT OF LAND:

PARCEL A:

LOT 1, BLOCK 1, ELLETT SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THE NORTH 10 FEET THEREOF CONVEYED TO THE COUNTY OF ADAMS DESCRIBED IN RESOLUTION AND DEED RECORDED NOVEMBER 25, 1969 IN BOOK 1561 AT PAGE 44.

PARCEL B:

LOT 1, BLOCK 1, LEXI PAPPAGEORGE SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO. PARCEL C:

A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8 AND 320.00 FEET WEST OF THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE; THENCE S 90°00'00" W ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 270.38 FEET TO A POINT, SAID POINT BEING 75.00 FEET EAST OF 20.00 FEET SOUTH OF THE N1/4 CORNER OF SECTION 8; THENCE S 44°58'15" W A DISTANCE OF 28.28 FEET TO A POINT ON THE EAST RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, SAID POINT BEING 55.00 FEET EAST AND 40.00 FEET SOUTH OF THE N1/4 CORNER OF SECTION 8; THENCE S 0°03'30" E ALONG THE EAST RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, A DISTANCE OF 289.80 FEET TO THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE N 90°00'00" E ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8, A DISTANCE OF 141.89 FEET; THENCE N 0°31'25" W A DISTANCE OF 166.68 FEET; THENCE N 89°28'25" E DISTANCE OF 149.85 FEET; THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO A POINT ON THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, AND 20.00 FEET SOUTH OF THE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE BOARD OF COUNTY COMMISSIONERS OF THE COUNTY OF ADAMS, STATE OF COLORADO, AS DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 6, 1907 IN BOOK 33 AT PAGE 220.

AND EXCEPT THAT PORTION TAKEN IN RULE AND ORDER RECORDED OCTOBER 15, 1971 IN BOOK 1745 AT PAGE 484.

ALSO EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE STATE DEPARTMENT OF HIGHWAYS, DIVISION OF HIGHWAYS, STATE OF COLORADO DESCRIBED IN DEED RECORDED DECEMBER 11, 1984 IN BOOK 2945 AT PAGE 579.

AND FURTHER EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

PARCEL D:

A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8, AND 320.00 FEET WEST OF THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE AND THE POINT OF BEGINNING; THENCE S 90°00'00" E A DISTANCE OF 30.00 FEET; THENCE S 0°03'30" W A DISTANCE OF 309.80 FEET TO A POINT ON THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8; THENCE S 90°00'00" W ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8. A DISTANCE OF 178.49 FEET: THENCE N 0°31'25" W A DISTANCE OF 166.68 FEET: THENCE N 89°28'25" E A DISTANCE OF 149.85 FEET; THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVE., AND THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS. STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

PARCEL E:

A PARCEL OF LAND BEING A PORTION OF THE EAST 290.00 FEET OF THE N1/2, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

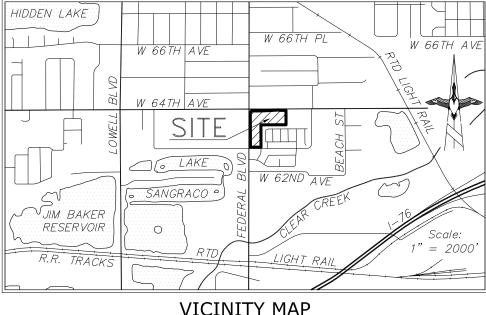
BEGINNING AT THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8. THENCE SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, WHICH IS THE TRUE POINT OF BEGINNING; THENCE CONTINUING SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4; THENCE WEST ALONG THE SOUTH LINE A DISTANCE OF 290.00 FEET; THENCE NORTH AND PARALLEL TO THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE: THENCE EAST ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 290.00 FEET TO THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS. STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

ALL OF WHICH BEING DESCRIBED BY METES AND BOUNDS AS FOLLOWS:

A PARCEL OF LAND LYING WITHIN THE NORTHWEST 1/4 OF THE NORTHEAST 1/4 OF SECTION 8. TOWNSHIP 3 SOUTH, RANGE 68 WEST OF THE 6TH PRINCIPAL MERIDIAN, COUNTY OF ADAMS, STATE OF COLORADO, BEING MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT THE NORTH 1/4 CORNER OF SAID SECTION 8, FROM WHICH THE NORTH LINE OF THE NORTHEAST 1/4 OF SAID SECTION 8 BEARS NORTH 89°49'13" EAST, WITH ALL BEARINGS CONTAINED HEREIN BEING REFERENCED TO SAID NORTH LINE; THENCE ALONG THE WEST LINE OF SAID NORTHEAST 1/4, SOUTH 00°18'56" EAST, A DISTANCE OF 65.02 FEET; THENCE DEPARTING SAID WEST LINE, NORTH 89°41'04" EAST, A DISTANCE OF 55.00 FEET TO THE EASTERLY RIGHT-OF-WAY OF NORTH FEDERAL BOULEVARD, A 110.00-FOOT-WIDE PUBLIC RIGHT-OF-WAY, BEING THE EAST LINE OF THE PARCEL OF LAND DESCRIBED IN THE RULE AND ORDER RECORDED OCTOBER 15, 1971 IN BOOK 1745, PAGE 484 IN THE OFFICE OF THE CLERK AND RECORDER FOR SAID COUNTY AND THE POINT OF BEGINNING; THENCE ALONG THE SOUTHERLY RIGHT-OF-WAY OF WEST 64TH AVENUE, A PUBLIC RIGHT-OF-WAY WITH A WIDTH THAT VARIES, THE FOLLOWING FOURTEEN (14) COURSES: 1) NORTH 44°45'13" EAST, A DISTANCE OF 35.17 FEET;



SHEET INDEX:

| SHEET 1 | COVER SHEET |
|---------|---|
| SHEET 2 | BOUNDARY, EXISTING PARCELS & EASEMENTS DETAIL |
| SHEET 3 | FINAL LOT AND EXISTING EASEMENTS DETAIL |

CERTIFICATE OF DEDICATION AND OWNERSHIP (continued): 2) NORTH 89°49'13" EAST, A DISTANCE OF 195.35 FEET; 3) NORTH 86°54'53" EAST, A DISTANCE OF 7.84 FEET; 4) SOUTH 03°05'07" EAST, A DISTANCE OF 1.00 FEET; 5) NORTH 86°54'56" EAST, A DISTANCE OF 210.82 FEET; 6) SOUTH 48°07'00" EAST, A DISTANCE OF 1.95 FEET; 7) NORTH 86°52'59" EAST, A DISTANCE OF 5.90 FEET; 8) NORTH 41°52'59" EAST, A DISTANCE OF 1.96 FEET; 9) NORTH 86°54'49" EAST, A DISTANCE OF 141.57 FEET; 10) NORTH 03°05'11" WEST, A DISTANCE OF 1.00 FEET; 11) NORTH 86°54'53" EAST, A DISTANCE OF 0.79 FEET TO THE BEGINNING OF A TANGENT CURVE CONCAVE SOUTHERLY, HAVING A RADIUS OF 970.00 FEET; 12) EASTERLY ALONG SAID TANGENT CURVE THROUGH A CENTRAL ANGLE OF 01°14'55", AN ARC LENGTH OF 21.14 FEET: 13) SOUTH 00°18'56" EAST, A DISTANCE OF 9.60 FEET; 14) NORTH 89°49'13" EAST, A DISTANCE OF 133.05 FEET TO THE EAST LINE OF LOT 1, BLOCK 1, ELLETT SUBDIVISION PER THE PLAT RECORDED NOVEMBER 17, 1969 AT RECEPTION NO. 878049 IN SAID OFFICE OF THE CLERK AND RECORDER, BEING 10.00 FEET SOUTH OF THE NORTHEAST CORNER OF SAID LOT 1, BEING THE SOUTHEAST CORNER OF THE PARCEL DESCRIBED IN THE RESOLUTION AND DEED RECORDED NOVEMBER 25, 1969 IN BOOK 1561, PAGE 44 IN SAID OFFICE OF THE CLERK AND RECORDER; THENCE ALONG SAID EAST LINE OF LOT 1, SOUTH 00°18'09" EAST, A DISTANCE OF 299.70 FEET TO THE SOUTHEAST CORNER OF SAID LOT 1; THENCE ALONG THE SOUTH LINE OF SAID LOT 1 AND THE WESTERLY PROLONGATION THEREOF, BEING THE NORTH LINE OF LOT 2, BLOCK 1, LEXI PAPPAGEORGE SUBDIVISION PER THE PLAT RECORDED JULY 2, 1991 AT RECEPTION NO. B1009567 IN SAID OFFICE OF THE CLERK AND RECORDER, SOUTH 89°50'23" WEST, A DISTANCE OF 523.60 FEET TO THE NORTHWEST CORNER OF SAID LOT 2, BEING THE NORTHEAST CORNER OF LOT 1, BLOCK 1, SAID LEXI PAPPAGEORGE SUBDIVISION; THENCE ALONG THE WEST LINE OF SAID LOT 2, BEING THE EAST LINE OF LOT 1, SOUTH 00°18'56" EAST, A DISTANCE OF 464.98 FEET TO THE SOUTHWEST CORNER OF LOT 2, BEING THE SOUTHEAST CORNER OF LOT 1; THENCE ALONG THE SOUTH LINE OF SAID LOT 1, BEING THE NORTHERLY RIGHT-OF-WAY OF WEST 63RD AVENUE, A 60.00-FOOT-WIDE PUBLIC RIGHT-OF-WAY, SOUTH 89°44'10" WEST, A DISTANCE OF 220.00 FEET TO THE SOUTHWEST CORNER OF LOT 1, BEING THE INTERSECTION OF THE NORTHERLY RIGHT-OF-WAY OF WEST 63RD AVENUE AND THE EASTERLY RIGHT-OF-WAY OF NORTH FEDERAL BOULEVARD; THENCE ALONG THE WEST LINE OF SAID LOT 1 AND THE NORTHERLY PROLONGATION THEREOF. BEING THE EASTERLY RIGHT-OF-WAY OF NORTH FEDERAL BOULEVARD, A 110.00-FOOT-WIDE PUBLIC RIGHT-OF-WAY, NORTH 00°18'56" WEST, A DISTANCE OF 729.93 FEET TO THE POINT OF BEGINNING.

CONTAINS 322,193 SQUARE FEET OR 7.397 ACRES, MORE OR LESS.

HAVE BY THESE PRESENTS LAID OUT, PLATTED AND SUBDIVIDED THE SAME INTO FOUR LOTS AND ONE TRACT AS SHOWN ON THIS PLAT UNDER THE NAME AND STYLE OF BERKLEY CENTER SUBDIVISION AND THE UNDERSIGNED DOES HEREBY DEDICATE, GRANT AND CONVEY TO ADAMS COUNTY THOSE DRAINAGE AND ACCESS EASEMENTS AS SHOWN ON THE PLAT; AND FURTHER RESTRICTS THE USE OF ALL PUBLIC EASEMENTS TO ADAMS COUNTY AND/OR ITS ASSIGNS, PROVIDED HOWEVER, THAT THE SOLE RIGHT AND AUTHORITY TO RELEASE OR QUIT CLAIM ALL OR ANY SUCH PUBLIC EASEMENTS SHALL REMAIN EXCLUSIVELY VESTED IN ADAMS COUNTY.

GENERAL NOTES:

- 1. BEARINGS ARE BASED ON THE THE STATE PLANE COORDINATE SYSTEM ESTABLISHED FOR THE COLORADO NORTH ZONE 0502, NORTH AMERICAN DATUM (NAD) OF 1983. DISTANCES SHOWN HEREON ARE GROUND UNITS, BEING THE NORTH LINE OF THE NORTHEAST 1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST OF THE 6TH PRINCIPAL MERIDIAN, WHICH BEARS NORTH 89°49'13" EAST BETWEEN THE FOUND MONUMENTS SHOWN AND DESCRIBED HEREON.
- 2. THIS PROPERTY IS NOT LOCATED WITHIN THE 100-YEAR FLOODPLAIN AS SHOWN ON THE FLOOD INSURANCE RATE MAP (FIRM) FOR ADAMS COUNTY COLORADO MAP NUMBER 08001C0592H, REVISED DATE MARCH 5, 2007.
- 3. THIS SURVEY DOES NOT CONSTITUTE A TITLE SEARCH BY ALTURA LAND CONSULTANTS, LLC TO DETERMINE OWNERSHIP OR EASEMENTS OF RECORD. FOR ALL INFORMATION REGARDING EASEMENTS, RIGHTS OF WAY AND TITLE OF RECORDS, ALTURA LAND CONSULTANTS, LLC RELIED UPON TITLE COMMITMENT NO. NCS-1180566-CO, WITH AN EFFECTIVE DATE OF JULY 17, 2023 AS PREPARED BY FIRST AMERICAN, TO DELINEATE THE AFORESAID INFORMATION.
- 4. PER C.R.S. 38-51-106. "ALL LINEAL UNITS DEPICTED ON THIS LAND SURVEY PLAT ARE U.S. SURVEY FEET. ONE METER EQUALS 39.37/12 U.S. SURVEY FEET, EXACTLY, ACCORDING TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY."
- 5. THE FIELD WORK FOR THIS SURVEY WAS PERFORMED BY ALTURA LAND CONSULTANTS, LLC ON JULY 14, 2023.
- 6. NOTICE: ACCORDING TO COLORADO LAW YOU MUST COMMENCE ANY LEGAL ACTION BASED UPON ANY DEFECT IN THIS SURVEY WITHIN THREE YEARS AFTER YOU FIRST DISCOVER SUCH DEFECT. IN NO EVENT MAY ANY ACTION BASED UPON ANY DEFECT IN THIS SURVEY BE COMMENCED MORE THAN TEN YEARS FROM THE DATE OF CERTIFICATION SHOWN HEREON.

SHEET 1 OF 3

- 7. ANY PERSON WHO KNOWINGLY REMOVES, ALTERS OR DEFACES ANY PUBLIC LAND SURVEY MONUMENT OF LAND MONUMENT OR ACCESSORY, COMMITS A CLASS TWO (2) MISDEMEANOR PURSUANT TO STATE STATUE 18-4-508, C.R.S.
- 8. PER THE STATE OF COLORADO BOARD OF LICENSURE FOR ARCHITECTS, PROFESSIONAL ENGINEERS, AND PROFESSIONAL LAND SURVEYORS RULE 1.6.B.2 THE WORD "CERTIFY"AS USED HEREON MEANS AN EXPRESSION OF PROFESSIONAL OPINION AND DOES NOT CONSTITUTE A WARRANTY OR GUARANTEE, EXPRESSED OR IMPLIED. THE SURVEY REPRESENTED HAS BEEN PERFORMED BY ME OR UNDER MY DIRECT SUPERVISION IN ACCORDANCE WITH APPLICABLE STANDARDS OF PRACTICE AND IS BASED UPON MY KNOWLEDGE, INFORMATION AND BELIEF.

STORM DRAINAGE FACILITIES STATEMENT:

THE POLICY OF THE COUNTY REQUIRES THAT MAINTENANCE ACCESS SHELL BE PROVIDED TO ALL STORM DRAINAGE FACILITIES TO ASSURE CONTINUOUS CAPABILITY OF THE SYSTEM. THE PROPERTY OWNERS SHALL BE RESPONSIBLE FOR THE MAINTENANCE OF ALL DRAINAGE FACILITIES INCLUDING INLETS, PIPES, CULVERTS, CHANNELS, DITCHES, HYDRAULIC STRUCTURES, AND DETENTION BASINS LOCATED ON THEIR LAND UNLESS MODIFIED BY THE SUBDIVISION DEVELOPMENT AGREEMENT. SHOULD THE OWNER FAIL TO MAINTAIN SAID FACILITIES. THE COUNTY SHALL HAVE THE RIGHT TO ENTER SAID LAND FOR THE SOLE PURPOSE OF OPERATIONS AND MAINTENANCE. ALL SUCH MAINTENANCE COST WILL BE ASSESSED TO THE PROPERTY OWNERS.

CERTIFICATE OF OWNERSHIP:

IN WITNESS THEREOF, QUIKTRIP CORPORATION, AN OKLAHOMA CORPORATION, HAS CAUSED THESE PRESENTS TO BE EXECUTED THIS ____ DAY OF ___ . 2024

OWNER: QUIKTRIP CORPORATION, AN OKLAHOMA CORPORATION

BY:_ JASON ACORD

TITLE: REGIONAL DIRECTOR OF REAL ESTATE / ASSISTANT SECRETARY

STATE OF KANSAS

)SS COUNTY OF JOHNSON)

THE FOREGOING PLAT AND DEDICATION WAS ACKNOWLEDGED BEFORE ME THIS ____ DAY OF A.D. 2024, BY JASON ACORD AS DIRECTOR OR REAL ESTATE / ASSISTANT SECRETARY FOR QUICK TRIP CORPORATION, AN OKLAHOMA CORPORATION WITNESS MY HAND AND OFFICIAL SEAL.

NOTARY PUBLIC

MY COMMISSION EXPIRES:

SURVEYOR'S CERTIFICATE:

I, JESUS A. LUGO, A LICENSED PROFESSIONAL LAND SURVEYOR IN THE STATE OF COLORADO, DO HEREBY CERTIFY THAT THIS PLAT WAS MADE BY ME OR UNDER MY DIRECT SUPERVISION ON THE 12TH DAY OF DECEMBER, 2023, AND THAT THE ACCOMPANYING MAP ACCURATELY AND PROPERLY SHOWS SAID SUBDIVISION.

SIGNED THIS __ DAY OF _____, 2024,

LICENSED PROFESSIONAL LAND SURVEYOR LICENSE NUMBER 38081

PLANNING COMMISSION APPROVAL

RECOMMENDED FOR APPROVAL BY THE ADAMS COUNTY PLANNING COMMISSION THIS ____ DAY , 2024.

CHAIR

BOARD OF COUNTY COMMISSIONERS' APPROVAL:

APPROVED BY THE ADAMS COUNTY BOARD OF COMMISSIONERS THIS DAY OF , 2024.

CHAIR

ADAMS COUNTY ATTORNEY'S OFFICE:

APPROVED AS TO FORM

CLERK AND RECORDER'S CERTIFICATE:

THIS FINAL PLAT WAS FILED FOR RECORD IN THE OFFICE OF THE ADAMS COUNTY CLERK AND RECORDER, IN THE STATE OF COLORADO, AT _____M., ON THIS ___ DAY OF _ A.D. 2024.

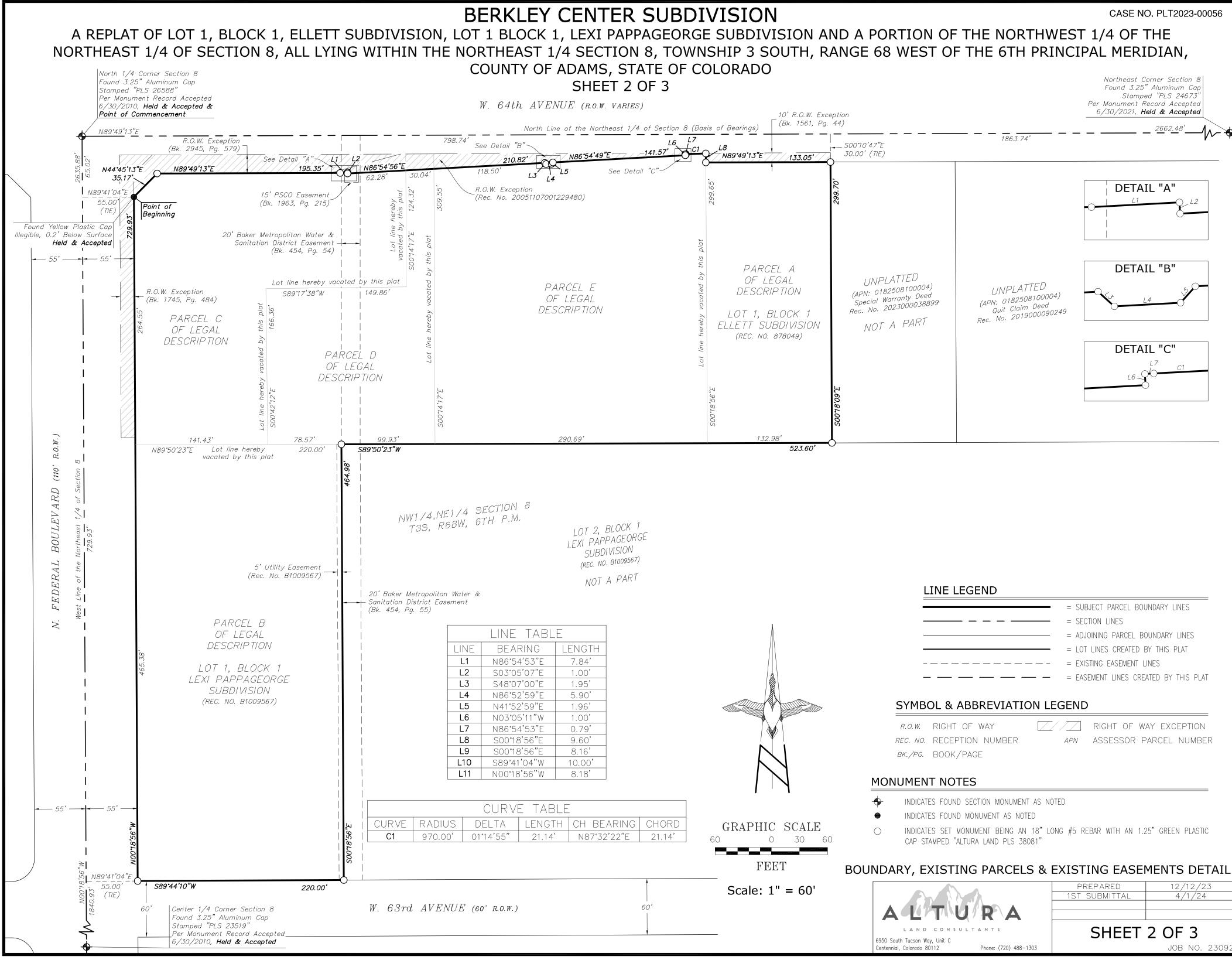
DEPUTY CLERK AND RECORDER

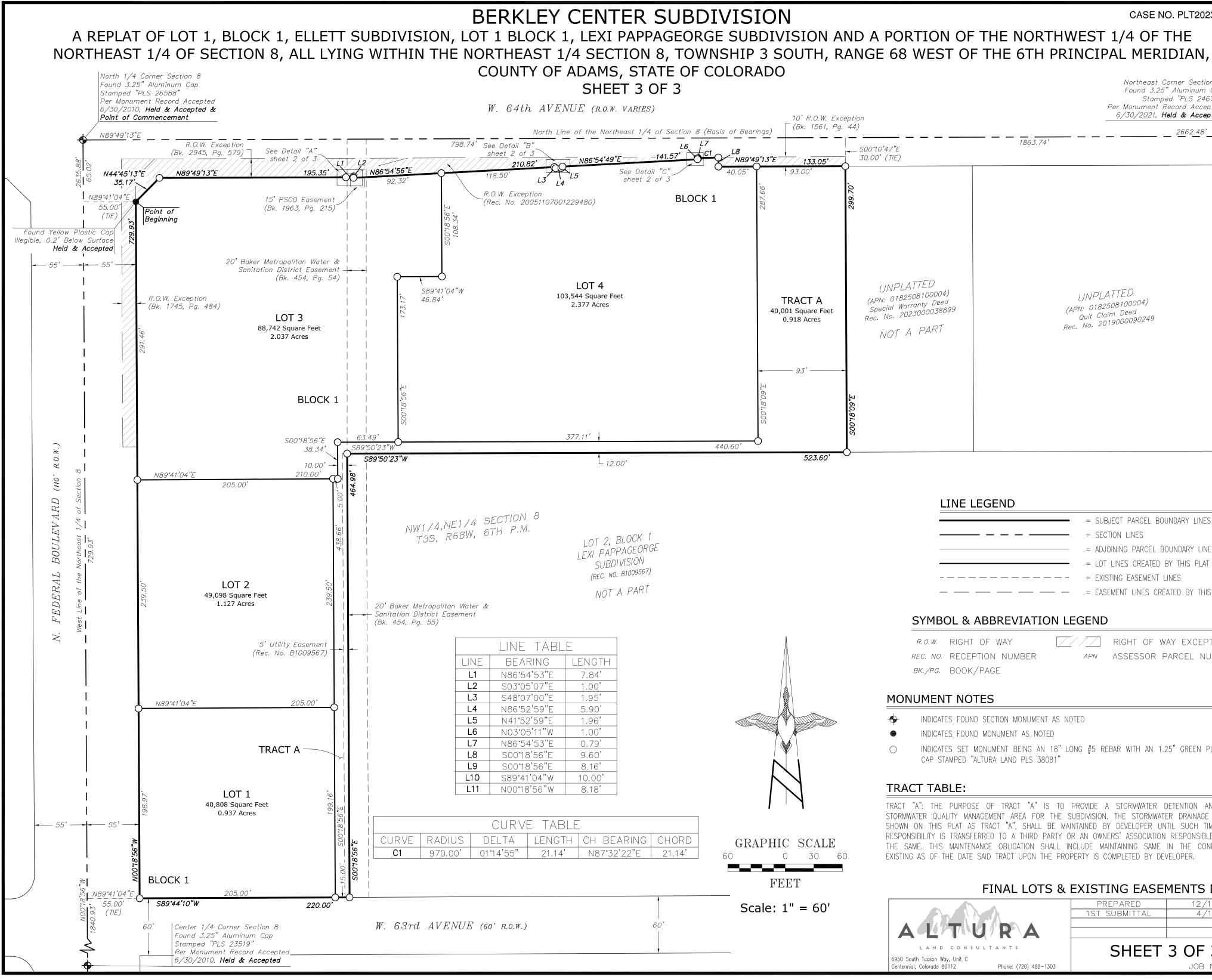
6950 South Tucson Way, Unit C

Centennial, Colorado 80112

RECEPTION NUMBER

COVER SHEET PREPARED 12/12/23 1ST SUBMITTAL 4/1/24 SHEET 1 OF 3 Phone: (720) 488-1303 JOB NO. 2309.





CASE NO. PLT2023-00056 Northeast Corner Section 8 Found 3.25" Aluminum Cap Stamped "PLS 24673" Per Monument Record Accepted 6/30/2021, Held & Accepted 10' R.O.W. Exception ⁻ (Bk. 1561, Pg. 44) North Line of the Northeast 1/4 of Section 8 (Basis of Bearings) <u>2662.48'</u> 1863.74' _ S00°10'47"E 1**C1** -141.57' 🖉 30.00' (TIE) _N89*****49'13"E 133.05' See Detail "C 40 (93.00 sheet 2 of 3 **BLOCK 1** UNPLATTED UNPLATTED (APN: 0182508100004) Special Warranty Deed Rec. No. 2023000038899 (APN: 0182508100004) TRACT A Quit Claim Deed 40,001 Square Feet Rec. No. 2019000090249 0.918 Acres NOT A PART 440.60' 523.60' LINE LEGEND = SUBJECT PARCEL BOUNDARY LINES = SECTION LINES = ADJOINING PARCEL BOUNDARY LINES = LOT LINES CREATED BY THIS PLAT = EXISTING EASEMENT LINES = EASEMENT LINES CREATED BY THIS PLAT _ SYMBOL & ABBREVIATION LEGEND RIGHT OF WAY EXCEPTION R.O.W. RIGHT OF WAY APN ASSESSOR PARCEL NUMBER *rec. NO*. RECEPTION NUMBER *bk./pg.* BOOK/PAGE MONUMENT NOTES INDICATES FOUND SECTION MONUMENT AS NOTED INDICATES FOUND MONUMENT AS NOTED \bigcirc INDICATES SET MONUMENT BEING AN 18" LONG #5 REBAR WITH AN 1.25" GREEN PLASTIC CAP STAMPED "ALTURA LAND PLS 38081" TRACT TABLE: TRACT "A": THE PURPOSE OF TRACT "A" IS TO PROVIDE A STORMWATER DETENTION AND/OR STORMWATER QUALITY MANAGEMENT AREA FOR THE SUBDIVISION. THE STORMWATER DRAINAGE AREA SHOWN ON THIS PLAT AS TRACT "A", SHALL BE MAINTAINED BY DEVELOPER UNTIL SUCH TIME AS RESPONSIBILITY IS TRANSFERRED TO A THIRD PARTY OR AN OWNERS' ASSOCIATION RESPONSIBLE FOR GRAPHIC SCALE THE SAME. THIS MAINTENANCE OBLIGATION SHALL INCLUDE MAINTAINING SAME IN THE CONDITION 21.14' 0 30 60 EXISTING AS OF THE DATE SAID TRACT UPON THE PROPERTY IS COMPLETED BY DEVELOPER. 60 FEET FINAL LOTS & EXISTING EASEMENTS DETAIL PREPARED 12/12/23 Scale: 1" = 60' 1ST SUBMITTAL 4/1/24 60' SHEET 3 OF 3 LAND CONSULTANTS 6950 South Tucson Way, Unit C Phone: (720) 488-1303 JOB NO. 23092

Centennial, Colorado 80112



Project Name: Berkley Center Subdivision

Print Date: 6/5/2024

Highway: 287

Mile Marker: 287.751

A comment response letter is REQUIRED along with the next submittal.

Review POC: Eyl, Aaron

Environmental Comments:

For ANY ground disturbance/work within CDOT ROW----

Required:

Arch/History/Paleo:

Since this is a permit, a file search for Arch, Paleo and History is required. If the file search identifies anything, a more extensive report will be required. If nothing is identified, then the file search should be sufficient. For the file search contact:

Cultural/History File Search: https://www.historycolorado.org/file-access Email: hc_filesearch@state.co.us

Paleo File Search: Colorado University Museum of Natural History https://www.colorado.edu/cumuseum/research-collections/paleontology/policies-procedure) Email: jacob.vanveldhuizen@colorado.edu and from the Denver Museum of Nature and Science – Email: kristen.mackenzie@dmns.org https://www.dmns.org/science/earth-sciences/earth-sciences-collections/

KH RESPONSE: File search is actively being coordinated.

Hydraulics Comments:

JB 5/28/24

The proposed conditions mainly keep historic drainage patterns. There is no increase in stormwater discharge into CDOT ROW/Federal Boulevard based on the offsite discussion on page 10 in the drainage report.

No further drainage comments or concerns at this time.

KH RESPONSE: Thank you for your review.

Permits Comments:

5/23/24 SB Any utilities being relocate to facilitate the access work will require their own individual permits and any landscaping will require it's own permits KH RESPONSE: Understood.

5.30.24

-There are a total of 8 existing access along Federal at this site. 6 of these accesses will need to be closed. Each closure requires an access permit. The other 2 accesses will also require access permits. These are for the proposed RIRO accesses. These accesses would be considerad a relocation on the access permit application. KH RESPONSE: Noted, we will gather all relevant permits related to access along Federal.

-The east side of the 64th ave and Federal intersection will also require an access permit. Per the traffic study the volume will increase by more then 20%. Because 64th ave is a county street the county would be the permittee on the permit application. KH RESPONSE: Noted, will update to county on permit application

-The full movement access located on 64th ave is off system and will not require a permit.

KH RESPONSE: Noted, thank you -The access permit application can be found at the following link: https://www.codot.gov/business/permits/accesspermits/forms/cdot0137 KH RESPONSE: Thank you

-The state highway access permit will cover any access work, sidewalk work, street lighting, and stormwater work. Any work outside of that including, but not limited to, landscaping, survey, or utility work will require a separate permit. Application is made online at the following link:

https://cdotpermits.force.com/portal/s/login/?ec=302&startURL=%2Fportal%2Fs%2F -- Aaron Eyl 5.30.24

KH RESPONSE: Thank you

Residential Engineer Comments:

5/24/24 - AMP

Portions of the CDOT M standard drawings M-608-1 (10 sheets) and M-609-1 (4 sheets) are shown in the plans. Key and relevant information and notes are found on the other sheets, so the entire 10- and 4-sheet sets should be included. KH RESPONSE: Updated callouts to reference CDOT details in plans.

Add this note to the plans: "Any and all work within CDOT right-of-way must be performed according to the standards set forth in the latest editions of the CDOT M&S Standard Plans and Standard Specifications for Road and Bridge Construction." KH RESPONSE: Note added to plans on sheet C002 section General Notes.

The existing curb ramp at 63rd Ave. is too far from the intersection such that pedestrian visibility may be reduced. The proposed ramp need not match the existing location but should be located closer to Federal Boulevard.

KH RESPONSE: Existing Ramp is 18.3' off curb, proposed ramp is 12.8' off of curb. In the proposed condition the ramp is closer to Federal and there is no other location to place ramp as overhead electric and stop sign limit location.

Right Of Way Comments:

Jim Daley Comment - 05/21/24: There are no ROW dedications shown on provided plat, so assume no ROW changes will be made. If ROW is to be dedicated it should be transferred by Plat to the Municipality/County first, and deeded to CDOT at a later date. There are no A-Lines on the ROW shown on ROW plans, so no access control line modifications required based on this information (uploaded highlighted CDOT ROW plans to this permit).

KH RESPONSE: No ROW is being dedicated.

5/31/24 KM - No concerns from Property Mgmt based on the current submission.

KH RESPONSE: Thank you for your review

Traffic Comments:

Comments from CDOT R1 Traffic & Safety - 6/5/24

General Comments

The construction plans need to include details of the driveway / intersection geometrics including curb ramp, driveway access, and other geometric and traffic control details.

KH RESPONSE: Provided, please see updated submittal application sheet C115.

Traffic Impact Study Comments

The statement on page 1, first paragraph, about the subdivision being completed in the next several years does not appear to be consistent with a 2026 short-term buildout horizon. The analysis needs to include a short-term buildout scenario that corresponds to the year during or after full buildout of the development.KH RESPONSE: Updated

Per section 4.4 and 4.1 of the State Highway Access Code (SHAC), minimum driveway access spacing is 325' with a 45 mph speed limit. The distance between the two proposed driveways on Federal is only 275'. Please try to move the south driveway on Federal further to the south to meet the minimum spacing requirement. If the SHAC requirement can't be met, a variance will be required from CDOT. KH RESPONSE: Variance to be provided with additional coordination w/ CDOT.

In the second bullet on page 2 of the TIS (and elsewhere in the document), the 20% increase discussed in the first sentence refers to the site-generated vehicle trips, not roadway ADT. The second sentence about traffic increasing on the east leg of the Federal & 64th Ave intersection is not really relevant. Permits are required for all of the proposed access locations based on the first sentence in Section 2.3(3) of the SHAC which states "to obtain permission to construct, modify, relocate, or close a vehicular access... a state highway access permit is required." KH RESPONSE: Permits to be provided.

On page 6 of the TIS, it might be desirable to include the figure in the List of Figures. KH RESPONSE: Updated.

Trip Generation (4.1)

Please reformat the Trip Generation Summary Report in Appendix C of the TIS. Even when printed at 11x17 it is difficult to work with. Text size should be Arial 11pt or equivalent height. Show the percent assumptions for internal capture and pass-by trip reductions. Make the colors of the columns consistent across the Total Trips, Net Trips after IC, and Net Trips after IC and PB tables. KH RESPONSE: Updated.

Please check the pass-by calculation in the PM peak for ITE code 934 Fast Food Restaurant w/Drive Thru. The pass-by percentage should be 50% for the PM peak but it appears a larger percentage was used (82/76 ? 37/34). Minor comment. KH RESPONSE: Updated.

It appears a 76% reduction in vehicle trips was assumed in the AM and PM peak hours for Land Use Code 945. However, according to Tables E.37 and E.38 in the Trip Generation Manual, the pass-by trip reductions should be 62% and 56%, respectively.

Please state the assumptions used to calculate daily and AM peak hour trips for Land Use Code 948, Automated Car Wash, since the Trip Generation Manual only shows a trip rate for the PM peak hour. KH RESPONSE: Updated.

Table 1 should include 4 rows that show the detail for the Total Trips after Internal Capture and Pass-by, similar to the 4 rows for Trips after Internal Capture. Also add 5 rows to the top of Table 1 showing the initial gross trips generated from the base trip rates / fitted curves. KH RESPONSE: Updated.

Trip Distribution (4.2)

No comments.

Traffic Assignment (4.3)

No comments.

Traffic Operations Analysis (5.0)

In Section 5.2, please add the delay and LOS results for the individual approaches in addition to the overall intersection results in Table 3. Add a statement that all individual approaches operate at an acceptable LOS in existing, background, and buildout conditions for 2026 and 2045. KH RESPONSE: Updated.

Consider adding two more items to Table 3 showing 2026 and 2045 Background + Pass-by project trips and corresponding delay and LOS since the development is not responsible for impacts to the local roadway system from pass-by trips, similar to background trips. This is not absolutely necessary given the extra Synchro runs and analyses, but it would provide information about the magnitude of the development's responsibilities at intersection #1 for example. KH RESPONSE: Updated.

Turn Bay Length Analysis (5.3)

On page 26, second sentence of the first bullet under intersection #1, the required deceleration length at 45 mph should be 435' per Table 4-6 of the SHAC and possibly longer when adjusting for grade. The subsequent statement that the SB left turn lane doesn't meet SHAC requirements in the existing condition is somewhat misleading because it provides 225' of storage where only about 70' is required. KH RESPONSE: Updated.

The last sentence of that bullet is also somewhat misleading. In our opinion, the existing median could be modified to significantly shorten the SBLT taper to increase storage. On of our primary safety concerns with left turn lanes is the possibility of LT queue spillback into the inside thru lane. These crashes can involve dangerous high-speed differentials between vehicles. It appears up to 90 - 100' of additional storage could be achieved, which would meet/exceed the 275' storage requirement. Modification of the median would be the responsibility of the developer given the additional traffic the proposed development will generate for the SBLT movement.

KH RESPONSE: Additional coordination required to discuss this requirement. Vehicle Queuing Analysis (5.4)

Please update the queuing analysis based on any changes to the assumptions mentioned above (e.g., pass-by reductions) and update Table 5. Of primary interest are the SBLT queue lengths. KH RESPONSE: Updated.

Conclusions and Recommendations (6.0)

Update this section base on comments above. Add information about the SBLT lane and median modifications as appropriate. KH RESPONSE: Updated.

Signs

On pages 2, 24, 29, and possibly others, the text states that an R1-1 STOP sign should be placed on the right side of the driveways on Federal for egress/exiting traffic and R3-2 No Left Turn signs should be placed below the STOP signs. In our opinion, R6-1R ONE WAY signs should be installed on the Federal median directly in front of the 2 driveway openings. The R3-2 No Left Turn signs are considered optional/supplemental. KH RESPONSE: Signs added to plans with correct reference to sign detail. END – 6/5/24 EB

Other Comments:

6/3: Install 8' sidewalk along Federal Blvd (CDOT ROW) to match CDOT's plans for Federal Blvd BRT construction. 5' sidewalk does not meet CDOT's plans/requirements. Maintain 8' sidewalk width approaching curb ramps. Curb ramp width shall match sidewalk width at 8' per PROWAG.

6/3: Plans show attached sidewalk. Install 8' detached sidewalk so sidewalk does not conflict with overhead electric poles. Landscaping plans may need to be modified to accommodate 8' sidewalk.

KH RESPONSE: Sidewalk updated to 8' width. Sidewalk jogs around overhead electric poles at those locations but is not detached overall. Conflict with overhead electric lines and landscaping in this area would occur, sidewalk to remain attached.

CONSTRUCTION DOCUMENTS FOR BERKLEY CENTER SUBDIVISION

LEGAL DESCRIPTION:

PARCEL A: LOT 1, BLOCK 1, ELLETT SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THE NORTH 10 FEET THEREOF CONVEYED TO THE COUNTY OF ADAMS DESCRIBED IN RESOLUTION AND DEED RECORDED NOVEMBER 25, 1969 IN BOOK 1561 AT PAGE 44.

PARCEL B: LOT 1, BLOCK 1, LEXI PAPPAGEORGE SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO. PARCEL C:

A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8 AND 320.00 FEET NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE THENCE S 90°00'00" W ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 270.38 FEET TO A POINT, SAID POINT BEING 75.00 FEET EAST OF 20.00 FEET SOUTH OF THE N1/4 CORNER OF SECTION 8: THENCE S 44°58'15" W A DISTANCE OF 28.28 FEFT TO A POINT OF THE EAST RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, SAID POINT BEING 55.00 FEET EAST AND 40.00 FEET SOUTH OF THE N1/4 CORNER OF SECTION 8: THENCE S 0°03'30" E ALONG THE EAS RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, A DISTANCE OF 289.80 FEET TO THE SOUTH LINE OF THE N1/2. NW1/4. NW1/4, NE1/4 OF SECTION 8; THENCE N 90°00'00" E ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8, A DISTANCE OF 141.89 FEET; THENCE W A DISTANCE OF 166.68 FEET; THENCE N 89°28'25" E DISTANCE OF 149.85 FEET THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO A POINT ON THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, AND 20.00 FEET SOUTH OF THE POINT OF BEGINNING, COUNTY OF ADAMS STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE BOARD OF COUNTY COMMISSIONERS OF THE COUNTY OF ADAMS, STATE OF COLORADO, AS DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 6, 1907 IN BOOK 33 AT PAGE 220.

AND EXCEPT THAT PORTION TAKEN IN RULE AND ORDER RECORDED OCTOBER 15, 1971 IN BOOK 1745 AT PAGE 484.

ALSO EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE STATE DEPARTMENT OF HIGHWAYS, DIVISION OF HIGHWAYS, STATE OF COLORADO DESCRIBED IN DEED RECORDED DECEMBER 11, 1984 IN BOOK 2945 AT PAGE 579.

AND FURTHER EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

PARCEL D:

A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST. SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8, AND 320.00 FEET WEST OF THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE AND THE POINT OF BEGINNING; THENCE S 90°00'00" E A DISTANCE OF 30.00 FEET; THENCE S 0°03'30" W A DISTANCE OF 309.80 FEET TO A POINT ON THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4. OF SECTION 8; THENCE S 90°00'00" W ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8, A DISTANCE OF 178.49 FEET; THENCE N 0°31'25" W A DISTANCE OF 166.68 FEET; THENCE N 89°28'25" E A DISTANCE OF 149.85 FEET; THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVE., AND THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

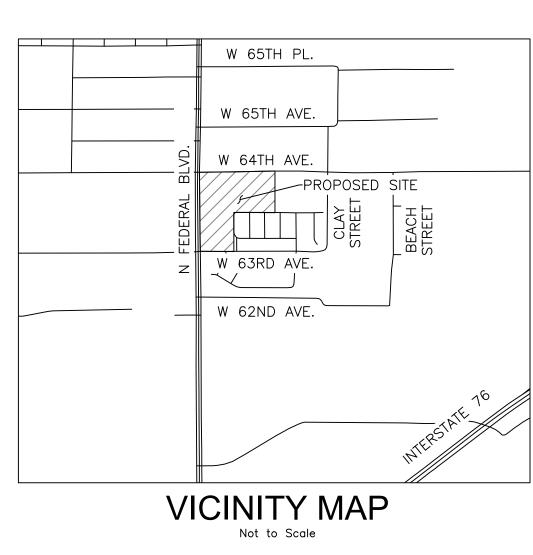
EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

PARCEL E: A PARCEL OF LAND BEING A PORTION OF THE EAST 290.00 FEET OF THE N1/2, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, THENCE SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, WHICH IS THE TRUE POINT OF BEGINNING; THENCE CONTINUING SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4; THENCE WEST ALONG THE SOUTH LINE A DISTANCE OF 290.00 FEET; THENCE NORTH AND PARALLEL TO THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE; THENCE EAST ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 290.00 FEET TO THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

ADAMS COUNTY, CO FEDERAL BLVD. & W. 64TH AVE.



MUNICIPAL CONTACT LIST:

ADAMS COUNTY

PLANNING DIVISION 4430 SOUTH ADAMS COUNTY PARKWAY. 1ST FLOOR, SUITE W2000A BRIGHTON, CO 80601 TEL: 720-523-6847 CONTACT: DAVID DEBOSKEY

FIRE DEPARTMENT ADAMS COUNTY FIRE PROTECTION DISTRICT 8055 NORTH WASHINGTON ST. DENVER, CO 80229 TEL: 303-539-6800

WATER UTILITIES CRESTVIEW WATER AND SANITATION DISTRICT TEL: 303-429-1881

STORM/SANITARY UTILITIES CRESTVIEW WATER AND SANITATION DISTRICT TEL: 303-429-1881

ELECTRIC COMPANY XCEL ENERGY

TEL: (800) 895-4999 GAS COMPANY XCEL ENERGY

TEL: (800) 895-4999 TELEPHONE COMPANY CENTURY LINK TEL: (866) 449-1979

PROJECT CONTACT LIST:

SURVEYOR OF RECORD ALTURA LAND CONSULTANTS 6950 S TUCSON WAY, UNIT C CENTENNIAL, CO 80112 TEL: (303) 902-7791 CONTACT: JESSE LUGO, PLS

ENGINEER OF RECORD KIMLEY-HORN AND ASSOCIATES, INC. 3325 SOUTH TIMBERLINE ROAD, SUITE 130 FORT COLLINS, CO 80525 TEL: (970) 822 7911 CONTACT: JAMES WALLER, PE

CLIENT/DEVELOPER QUIKTRIP CORPORATION 12000 WASHINGTON ST, STE 175 THORNTON, CO 80241 (303) 248-0436 CONTACT: BRITTANY SIKORSKI

<u>CLIENT/DEVELOPER</u> QUIKTRIP CORPORATION 4705 SOUTH 129TH EAST AVE TULSA, OK 74134 (918) 615-7685 CONTACT: JOSH POTTER, PE

ARCHITECT: LICKEL ARCHITECTURE 14 W 3RD ST #100 KANSAS CITY, MO 64105 TEL: (913) 389-7866 CONTACT: AMANDA SPITZER

LANDSCAPE ARCHITECT KIMLEY-HORN AND ASSOCIATES, INC. 6200 SOUTH SYRACUSE WAY, SUITE 300 GREENWOOD VILLAGE, CO 80111 TEL: (303) 228-2319 CONTACT: CHRIS HEPLER, PLA

FLOOD CERTIFICATION:

VERTICAL RELIEF WAS MADE FROM AN ON THE GROUND SURVEY, CONTOURS SHOWN HERON ARE AT 1' INTERVALS USING THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAV 88), GEOID 12A. SITE VERTICAL WAS ESTABLISHED BY USING COUNTY OF DENVER BENCH MARK "156B" LOCATED AT THE SOUTHEAST CORNER OF 50TH AVENUE AND FEDERAL BOULEVARD.

CASE NO. PLT2023-0056

| SI | neet List Table |
|--------------|----------------------------|
| Sheet Number | Sheet Title |
| C001 | COVER SHEET |
| C002 | GENERAL NOTES |
| C030 | DEMOLITION PLAN |
| C100 | OVERALL SITE PLAN |
| C101 | DETAILED SITE PLAN |
| C102 | DETAILED SITE PLAN |
| C103 | DETAILED SITE PLAN |
| C104 | DETAILED SITE PLAN |
| C110 | OVERALL GRADING PLAN |
| C111 | DETAILED GRADING |
| C112 | DETAILED GRADING |
| C113 | DETAILED GRADING |
| C114 | DETAILED GRADING |
| C115 | DRIVEWAY DETAILED GRADING |
| C300 | STORM SEWER PLAN & PROFILE |
| C500 | SITE DETAILS |
| C501 | SITE DETAILS |
| C502 | SITE DETAILS |
| L100 | OVERALL LANDSCAPE PLAN |
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| L102 | DETAILED LANDSCAPE PLAN |
| L103 | DETAILED LANDSCAPE PLAN |
| L200 | LANDSCAPE NOTES |

WETLANDS NOTICE:

ANY DEVELOPMENT, EXCAVATION, CONSTRUCTION, OR FILLING IN A U.S. CORPS OF ENGINEERS DESIGNATED WETLAND IS SUBJECT TO LOCAL, STATE AND FEDERAL APPROVALS. THE CONTRACTOR SHALL COMPLY WITH ALL PERMIT REQUIREMENTS AND/OR RESTRICTIONS AND ANY VIOLATION WILL BE SUBJECT TO FEDERAL PENALTY. THE CONTRACTOR SHALL HOLD THE OWNER/ DEVELOPER, THE ENGINEER AND THE LOCAL GOVERNING AGENCIES HARMLESS AGAINST SUCH VIOLATION.

WARRANTY/DISCLAIMER:

THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER THE ENGINEER NOR ITS PERSONNEL CAN OR DO WARRANT THESE DESIGNS OR PLANS AS CONSTRUCTED EXCEPT IN THE SPECIFIC CASES WHERE THE ENGINEER INSPECTS AND CONTROLS THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

NOTICE TO BIDDERS:

ALL QUESTIONS REGARDING THE PREPARATION OF THE GENERAL CONTRACTOR'S BID SHALL BE DIRECTED TO THE OWNER'S CONSTRUCTION REPRESENTATIVE. SUBCONTRACTORS MUST DIRECT THEIR QUESTIONS THROUGH THE GENERAL CONTRACTOR. THE CONSULTING ARCHITECT AND/OR THE CONSULTING ENGINEER SHALL NOT BE CONTACTED DIRECTLY WITHOUT PRIOR AUTHORIZATION FROM THE OWNER/DEVELOPER.

THE FEDERAL EMERGENCY MANAGEMENT AGENCY, FLOOD INSURANCE RATE MAPS NO. 08001C0584H AND NO.08001C0592H, EFFECTIVELY DATED 03/05/2007, INDICATES THIS PARCEL OF LAND TO BE LOCATED IN ZONE X (AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN).

BENCHMARKS

ELEVATION = 5379.63 FEET (NAVD 1988)

BASIS OF BEARINGS

BEARINGS ARE BASED ON THE STATE PLANE COORDINATE SYSTEM ESTABLISHED FOR THE COLORADO NORTH ZONE 0502, NORTH AMERICAN DATUM (NAD) OF 1983. DISTANCES SHOWN HEREON ARE GROUND UNITS. BEING THE NORTH LINE OF THE NORTHEAST 1/4 OF SECTION 8, BEARING S89°49'13"W, BETWEEN MONUMENTS SHOWN HEREON.

| LT2023-0056 | DATE APPR. |
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| AN AN AN AN | PTOP NO BODE STORY AND ASSOCIATES, INC. MANUAL STORY AND ASSOCIATES, INC. 2325 SOUTH TIMBERLINE ROAD, SUITE 130 AT COLLINS, COLORADO 80525 (970) 822-791 Tot Collins, COLORADO 80525 (970)-822-79 |
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| | FOR REVIEW ONLY NOT_FOR CONSTRUCTION Kimley » Horn Kimley-Horn and Associates, Inc. |
| | PROJECT NO. 096888037 |
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Know what's **below**.

GENERAL NOTES

- I. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR SHALL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS. ANY CONSTRUCTION OBSERVATION BY THE ENGINEER OF THE CONTRACTOR'S PERFORMANCE IS NOT INTENDED TO INCLUDE REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES, IN, ON OR NEAR THE CONSTRUCTION SITE.
- 2. THE CONTRACTOR IS RESPONSIBLE FOR ENSURING THAT ALL NECESSARY PERMITS HAVE BEEN OBTAINED FROM THE GOVERNING AGENCIES AND COORDINATING ALL GOVERNING AGENCY INSPECTIONS REQUIRED THROUGHOUT THE DURATION OF THE PROJECT.
- 3. CONTRACTOR SHALL BE RESPONSIBLE FOR RAZING AND REMOVAL OF THE EXISTING STRUCTURES, RELATED UTILITIES, PAVING, AND ANY OTHER EXISTING IMPROVEMENTS AS NOTED. REFERENCE SITE WORK SPECIFICATIONS.
- 4. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.
- 5. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGE TO ADJACENT PROPERTIES AND NEW CONSTRUCTION IN PLACE DURING THE CONSTRUCTION PHASES OF THIS PROJECT. ANY DISTURBED IMPROVEMENTS SHALL BE REPLACED IN KIND AT THE CONTRACTORS EXPENSE.
- 6. ANY QUANTITIES PROVIDED ON THESE PLANS ARE FOR GENERAL REFERENCE PURPOSES ONLY. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING THE QUANTITIES REQUIRED FOR CONSTRUCTION.
- 7. THE EXISTING FEATURES SHOWN ON THESE PLANS ARE THOSE NOTED IN THE FIELD AND THOSE TAKEN FROM RECORD DRAWINGS. THERE IS NO GUARANTEE THAT ALL FEATURES (ABOVE OR BELOW GROUND) ARE SHOWN ON THE PLANS. IT IS THE CONTRACTOR'S RESPONSIBILITY TO VERIFY ALL EXISTING FEATURES PRIOR TO BIDDING THE PROJECT.
- 8. THE CONTRACTOR SHALL LOCATE ALL UTILITIES PRIOR TO BEGINNING CONSTRUCTION BY CONTACTING THE LOCAL UTILITY COMPANIES AND/OR UTILIZING THE LOCAL ONE-CALL SYSTEM. ANY DAMAGE DONE TO EXISTING UTILITIES (THAT ARE TO REMAIN IN PLACE) DURING CONSTRUCTION OPERATIONS WILL BE THE CONTRACTOR'S RESPONSIBILITY AND REPAIRED AT THE CONTRACTOR'S EXPENSE.
- 9. ALL SITE WORK FOR THIS PROJECT SHALL MEET OR EXCEED THE OWNERS CONTRACT DOCUMENTS AND SPECIFICATIONS. ALL WORK SHALL MEET OR EXCEED THE RELEVANT UTILITY COMPANIES AND REGULATORY AGENCIES, CONTRACT DOCUMENTS AND SPECIFICATIONS. ALL WORK WITHIN PUBLIC AND STATE RIGHT OF WAY SHALL BE IN ACCORDANCE WITH THE GOVERNING AGENCIES STANDARDS AND SPECIFICATIONS.
- 10. TRAFFIC CONTROL SHALL CONFORM TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD), CURRENT EDITION. IT IS THE CONTRACTOR'S RESPONSIBILITY TO ENSURE PROPER TRAFFIC CONTROL IS IN PLACE FOR EACH PHASE OF CONSTRUCTION. THE CONTRACTOR IS ALSO RESPONSIBLE FOR PROPERLY MAINTAINING TRAFFIC CONTROL DEVICES THROUGHOUT THE DURATION OF THE WORK. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING TRAFFIC CONTROL PLANS TO THE CITY AND DEPARTMENT OF TRANSPORTATION AS REQUIRED.
- 11. ANY AND ALL WORK WITHIN CDOT RIGHT-OF-WAY MUST BE PERFORMED ACCORDING TO THE STANDARDS SET FORTH IN THE LATEST EDITIONS OF THE CDOT M&S STANDARD PLANS AND STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION.

ENGINEERING DEMOLITION NOTES

- 1. THE GENERAL CONTRACTOR IS RESPONSIBLE FOR ENSURING THAT THIS PROJECT IS CONSTRUCTED IN ACCORDANCE WITH THESE DOCUMENTS AND IN COMPLIANCE WITH CODES INDICATED HEREIN. THE QUALITY OF WORKMANSHIP AND INSTALLATION OF MATERIALS SPECIFIED BY THE OWNER OR ENGINEER ARE THE RESPONSIBILITY OF THE CONTRACTOR. THE CEC WILL NOT BE HELD RESPONSIBLE FOR ANY SUBSTANDARD OR INSUFFICIENT WORKMANSHIP, MATERIALS OR SERVICES PROVIDED IN THE EXECUTION OF ANY PHASE OF CONSTRUCTION OF THIS PROJECT.
- 2. ALL MATERIALS ARE TO BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S REQUIREMENTS AND ALL GENERAL CONTRACTORS ARE TO ENSURE THAT ALL MANUFACTURER'S WARRANTIES SHALL BE HONORED.
- 3. ALL DEMOLITION MATERIALS NOT REUSED OR RELOCATED SHALL BE REMOVED BY THE CONTRACTOR COORDINATE WITH THE OWNER REGARDING MATERIALS TO BE SALVAGED BY THE OWNER.
- 4. GENERAL CONTRACTOR IS RESPONSIBLE FOR RECEIVING, UNLOADING, STORING AND PROTECTING OF EXISTING MATERIALS TO BE REUSED ON-SITE OR OWNER SUPPLIED MATERIALS AND EQUIPMENT UNTIL IT HAS BEEN INSTALLED AND ACCEPTED BY THE OWNER.
- 5. THE GENERAL CONTRACTOR IS RESPONSIBLE FOR ENSURING THE SAFETY OF ALL PERSONS ON THE JOB SITE AT ALL TIMES INCLUDING (BUT NOT LIMITED TO) ALL GENERAL CONTRACTORS, VENDORS, DESIGN STAFF PROFESSIONALS AND INSPECTION PERSONNEL.
- 6. ALL DEMOLITION SHALL BE CARRIED OUT IN A SAFE MANNER AND IN STRICT ACCORDANCE WITH OSHA REGULATIONS.
- 7. DURING DEMOLITION AND RECONSTRUCTION, THE CONTRACTOR SHALL COORDINATE ANY SAFETY BARRIERS AND/OR BARRICADES USED.
- 8. IT IS THE CONTRACTOR'S RESPONSIBILITY TO PROVIDE ADEQUATE SHORING, BRACING AND SUPPORT SYSTEMS AND TO KEEP EXISTING SYSTEMS INTACT AND IN SAFE CONDITION DURING THE REMOVAL OF ITEMS AND NEW CONSTRUCTION. IT IS THE CONTRACTOR'S RESPONSIBILITY FOR MEANS AND METHODS OF DEMOLITION AND NEW CONSTRUCTION.
- 9. ALL CONDITIONS SHOWN TO BE "EXISTING" SHALL BE VERIFIED IN THE FIELD BY THE GENERAL CONTRACTOR PRIOR TO START OF CONSTRUCTION. ANY DISCREPANCIES SHALL BE NOTED AND SUBMITTED TO THE OWNER AND THE ENGINEER FOR REVIEW. CHANGES TO THE ORIGINAL DESIGN OF THIS PROJECT DUE TO EXISTING SITE CONDITIONS MUST BE APPROVED BY BOTH THE OWNER AND THE ENGINEER PRIOR TO MAKING ANY CHANGES. 10. THE CONTRACTOR SHALL FIELD VERIFY THE EXTENT OF DEMOLITION.
- 11. WHEN UTILITIES ARE REMOVED, THE CONTRACTOR SHALL CAP AND SEAL UTILITIES AS DIRECTED BY THE ENGINEER AND AS PER COUNTY STANDARDS.
- 13. UPON COMPLETION OF ALL CONSTRUCTION, A DRAINAGE CERTIFICATION LETTER, AND APPROPRIATE AS-BUILT 12. THE CONTRACTOR SHALL USE A WET SAW FOR SLAB SAWING. NO JACK HAMMERS WILL BE ALLOWED WITHOUT CONSTRUCTION DRAWINGS AND INFORMATION WILL BE REQUIRED. THIS LETTER WILL BE STAMPED AND SIGNED BY PRIOR APPROVAL FROM THE OWNER. THE ORIGINAL DESIGN ENGINEER.

ENGINEERING DRAINAGE AND STORM NOTES

- 1. ON-SITE DRAINAGE HAS BEEN PROVIDED TO MAINTAIN THE EXISTING DRAINAGE PATTERNS.
- 2. ALL BEDDING SHALL BE ASTM C-33 NO. 67 STONE. THE BEDDING SHALL BE 6-8" DEEP UNDER THE PIPE AND BACKFILLED TO SPRING LINE, EXCEPT IN AREAS OF UNSUITABLE BACKFILL, THEN BEDDING MATERIAL SHALL BE PLACED TO A LEVEL 12" ABOVE PIPE.
- 3. A MINIMUM CLEARANCE OF TWENTY-FOUR (24) INCHES IS REQUIRED WHENEVER A WATER MAIN CROSSES OVER A SANITARY SEWER. CONCRETE ENCASEMENT OF THE SANITARY SEWER WILL BE REQUIRED IF THE CLEARANCE IS LESS THAN TWENTY-FOUR (24) INCHES AND WILL BE INSTALLED. ENCASEMENT WILL EXTEND TEN (10) FEET EITHER SIDE OF THE CROSSING FOR A TOTAL LENGTH OF TWENTY (20) FEET.
- 4. PRECAST STRUCTURES MAY BE USED AT CONTRACTORS OPTION.
- 5. IF DEWATERING IS REQUIRED, THE CONTRACTOR SHALL OBTAIN ANY APPLICABLE REQUIRED PERMITS. THE CONTRACTOR IS TO COORDINATE WITH THE OWNER PRIOR TO EXCAVATION.

ENGINEERING SITE NOTES

- 1. CONTRACTOR IS RESPONSIBLE FOR PROTECTION OF ALL PROPERTY CORNERS.
- 2. CONTRACTOR SHALL MATCH PROPOSED CURB AND GUTTER, CONCRETE, AND PAVEMENT TO EXISTING GRADE AT ALL TIE IN LOCATIONS.
- 3. CONTRACTOR SHALL REMOVE PAVEMENT AND CONCRETE IN ACCORDANCE WITH DETAILS AND SPECIFICATIONS OF ADAMS COUNTY AND AS DIRECTED BY THE ENGINEER.
- 4. THE EARTHWORK FOR ALL BUILDING FOUNDATIONS AND SLABS SHALL BE IN ACCORDANCE WITH ARCHITECTURAL BUILDING PLANS AND SPECIFICATIONS.
- 5. CONTRACTOR SHALL PROVIDE PIPE BOLLARDS SHOWN ON SITE PLAN FOR PROTECTION OF ALL ABOVE GROUND UTILITIES AND APPURTENANCES IN DRIVE AREA, AS WELL AS TO PROTECT ALL ACCESSIBLE SIGNS.
- CONTRACTOR SHALL REFER TO ARCHITECTURAL PLANS AND SPECIFICATIONS FOR ACTUAL LOCATION OF ALL UTILITY ENTRANCES, TO INCLUDE, SANITARY SEWER LATERALS, DOMESTIC AND FIRE PROTECTION WATER SERVICE, ELECTRICAL, AND TELEPHONE SERVICE. CONTRACTOR SHALL COORDINATE INSTALLATION OF UTILITIES IN SUCH A MANNER AS TO AVOID CONFLICTS AND ASSURE PROPER DEPTHS ARE ACHIEVED, AS WELL AS, COORDINATE WITH ANY UTILITY COMPANIES FOR APPROVED LOCATIONS AND SCHEDULING OF TIE-INS/CONNECTIONS TO THEIR FACILITIES.
- 7. CONTRACTOR IS RESPONSIBLE FOR REPAIRING THE DAMAGE DONE TO ANY EXISTING ITEM DURING CONSTRUCTION, SUCH AS, BUT NOT LIMITED TO, DRAINAGE, UTILITIES, PAVEMENT, STRIPING, CURB, ETC. REPAIRS SHALL BE EQUAL TO, OR BETTER THAN, EXISTING CONDITIONS. CONTRACTOR IS RESPONSIBLE TO DOCUMENT ALL EXISTING DAMAGE AND NOTIFY CONSTRUCTION MANAGER PRIOR TO CONSTRUCTION START.
- CONTRACTOR TO REMOVE OR RELOCATE, WHEN APPLICABLE, ALL EXISTING BUILDINGS, FOUNDATIONS, BASEMENTS, CONNECTING IMPROVEMENTS, DRAIN PIPES, SANITARY SEWER PIPES, POWER POLES, AND GUY WIRES, WATER METERS AND WATER LINES, WELLS, SIDEWALKS, SIGN POLES, UNDERGROUND GAS, SEPTIC TANKS, AND ASPHALT, SHOWN AND NOT SHOWN, WITHIN CONSTRUCTION LIMITS AND WHERE NEEDED, TO ALLOW FOR NEW CONSTRUCTION AS SHOWN.
- 9. ALL PAINT USED FOR PARKING STRIPING SHALL BE PER SITE SPECIFIC SPECIFICATIONS.
- 10. CONTRACTOR SHALL IDENTIFY CONSTRUCTION WATER SOURCE AND INCLUDE THE COST IN THE BASE BID.

ENGINEERING GRADING NOTES

- CONTOURS ON SIDEWALKS AND PRIVATE / PUBLIC ROADWAYS ARE TO FINISH GRADE.
- 2. FOR GROUND TREATMENT OF ALL OPEN AREAS WITHIN THE PROJECT SITE, REFER TO LANDSCAPE PLANS.
- 3. FIELD DENSITY TESTS SHALL BE TAKEN AT A FREQUENCY AS REQUIRED IN THE SPECIFICATIONS.
- 4. SOD OR SEED/MULCH MUST BE INSTALLED AND MAINTAINED ON EXPOSED SLOPES WITHIN 48 HOURS OF COMPLETING FINAL GRADING, AND AT ANY OTHER TIME AS NECESSARY, TO PREVENT EROSION, SEDIMENTATION OR TURBID DISCHARGES.
- 5. THE CONTRACTOR MUST CONSTRUCT AND MAINTAIN A PERMANENT VEGETATIVE PROTECTIVE COVER FOR EROSION AND SEDIMENT CONTROL ON ALL LAND SURFACES EXPOSED OR DISTURBED BY CONSTRUCTION OF THE PERMITTED PROJECT. THE PROTECTIVE COVER MUST BE INSTALLED WITHIN FOURTEEN DAYS AFTER FINAL GRADING OF THE AFFECTED LAND SURFACE. A PERMANENT VEGETATIVE COVER MEETING THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT'S (CDPHE'S) GENERAL PERMIT COVERAGE REQUIREMENT MUST BE ESTABLISHED.
- 6. THE CONTRACTOR SHALL GRADE THE SITE TO THE ELEVATIONS INDICATED AND SHALL REGRADE WASHOUTS WHERE THEY OCCUR AFTER EVERY RAINFALL UNTIL A GRASS STAND OR OTHER FINAL LANDSCAPE PLANTING IS WELL ESTABLISHED.
- 7. THE CONTRACTOR SHALL ENSURE THAT ISLAND PLANTING AREAS AND OTHER PLANTING AREAS ARE NOT COMPACTED AND DO NOT CONTAIN COMPACTED BASE MATERIAL. THE CONTRACTOR SHALL ALSO EXCAVATE AND REMOVE ALL UNDESIRABLE MATERIAL FROM ALL AREAS ON THE SITE TO BE PLANTED.

GENERAL CONSTRUCTION NOTES

- 1. A PRE-CONSTRUCTION MEETING IS REQUIRED PRIOR TO THE COMMENCEMENT OF CONSTRUCTION. TO SCHEDULE A PRE-CONSTRUCTION MEETING CONTACT THE ADAMS COUNTY CONSTRUCTION INSPECTOR SUPERVISOR AT 720-523-6965. 2. ALL CONCRETE CURB, GUTTER AND WALK MUST BE POURED MONOLITHICALLY USING 4,500 PSI CONCRETE WITH
- FIBER MESH. 3. ALL MATERIAL SUBMITTALS MUST BE APPROVED, STAMPED AND SIGNED, BY THE ENGINEER OF RECORD AND, SUBMITTED TO THE ADAMS COUNTY CONSTRUCTION INSPECTOR FOR APPROVAL PRIOR TO
- CONSTRUCTION /INSTALLATION. 4. THE CONTRACTOR IS REQUIRED TO SUBMIT COPIES OF ALL CONCRETE AND ASPHALT TICKETS TO THE ADAMS COUNTY CONSTRUCTION INSPECTOR.
- 5. THE CONTRACTOR IS RESPONSIBLE FOR ALL QUALITY CONTROL TESTING AND, IS REQUIRED TO SUBMIT ALL TEST RESULTS TO THE ADAMS COUNTY CONSTRUCTION INSPECTOR. 6. THE CONTRACTOR IS REQUIRED TO REMOVE A MINIMUM OF TWO (2) FEET OF EXISTING ASPHALT FOR ALL CURB
- AND GUTTER REPLACEMENT. 7. ALL UTILITY CUTS IN EXISTING STREETS ARE REQUIRED TO BE BACKFILLED WITH FLOWFILL AND, PATCHED WITH A MINIMUM OF 9-INCH ASPHALT PATCH.
- 8. A COPY OF THE GEOTECHNICAL REPORT SPECIFYING THE PAVEMENT THICKNESS DESIGN MUST BE SUBMITTED FOR REVIEW. 9. PERMITS WILL BE REQUIRED FOR THE INSTALLATION OF ALL UTILITIES. THE DEVELOPER/CONTRACTOR/ENGINEER.
- MUST SUPPLY THE LINEAL FOOTAGES AND THE NUMBER OF SERVICE CUTS REQUIRED FOR ALL UTILITIES. 10. PERMITS WILL BE REQUIRED FOR THE INSTALLATION OF ALL CONCRETE AND ASPHALT FACILITIES. PRIOR TO THE ISSUANCE OF THESE PERMITS, THE DEVELOPER/CONTRACTOR/ENGINEER, MST SUPPLY THE SQUARE YARDAGE/SQUARE FOOTAGES OF ALL CONCRETE AND ASPHALT BEING INSTALLED.
- 11. THE SIA MUST BE COMPLETED WITH APPROPRIATE COLLATERAL, ALONG WITH THE PROPOSED PLAT, PRIOR TO THE ISSUANCE OF ANY ROW ACCESS/CONSTRUCTION PERMIT. 12. NO C.O.'S WILL BE ISSUED FOR ANY BUILDING CONSTRUCTION UNTIL ALL ROW IMPROVEMENTS HAVE BEEN COMPLETED AND HAVE BEEN GRANTED PRELIMINARY ACCEPTANCE.

- MATERIAL.
- USE FOR SUCH WORK.
- CONSTRUCTION.

- PRIOR TO CONSTRUCTION.

- THE FINAL CONNECTION OF SERVICES.

- CONTROL.
- CORNERS.

ENGINEERING PAVING NOTES

- CONTINUOUS GRADE.

ENGINEERING CONSTRUCTION NOTES

THE CONTRACTOR SHALL BE RESPONSIBLE TO FURNISH ALL MATERIAL AND LABOR TO CONSTRUCT THE FACILITY AS SHOWN AND DESCRIBED IN THE CONSTRUCTION DOCUMENTS IN ACCORDANCE WITH THE APPROPRIATE APPROVING AUTHORITIES, SPECIFICATIONS AND REQUIREMENTS. CONTRACTOR SHALL VISIT THE SITE PRIOR TO BIDDING TO DETERMINE EXISTING CONDITIONS. CONTRACTOR SHALL CLEAR AND GRUB ALL AREAS UNLESS OTHERWISE INDICATED, REMOVING TREES, STUMPS, ROOTS, MUCK AND ALL OTHER DELETERIOUS

ALL EXISTING UTILITIES SHOWN ARE LOCATED ACCORDING TO THE INFORMATION AVAILABLE TO THE ENGINEER AT THE TIME THE DRAWINGS WERE PREPARED AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR THE ENGINEER. GUARANTEE IS NOT MADE THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN OR THAT THE LOCATION OF THOSE SHOWN ARE ENTIRELY ACCURATE. THE LOCATIONS SHOWN ARE FOR BIDDING PURPOSES ONLY. FINDING THE ACTUAL LOCATIONS OF ANY EXISTING UTILITIES IS THE CONTRACTOR'S RESPONSIBILITY AND SHALL BE DONE BEFORE HE COMMENCES ANY WORK IN THE VICINITY. FURTHERMORE, THE CONTRACTOR SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES DUE TO THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. THE OWNER OR ENGINEER WILL ASSUME NO LIABILITY FOR ANY DAMAGES SUSTAINED OR COST INCURRED BECAUSE OF THE OPERATIONS IN THE VICINITY OF EXISTING UTILITIES OR STRUCTURES, NOR FOR TEMPORARY BRACING AND SHORING OF SAME. IF IT IS NECESSARY TO SHORE, BRACE, SWING OR RELOCATE A UTILITY, THE UTILITY COMPANY OR DEPARTMENT AFFECTED SHALL BE CONTACTED AND THEIR PERMISSION OBTAINED REGARDING THE METHOD TO

IT IS THE CONTRACTOR'S RESPONSIBILITY TO CONTACT THE VARIOUS UTILITY COMPANIES WHICH MAY HAVE BURIED OR AERIAL UTILITIES WITHIN OR NEAR THE CONSTRUCTION AREA BEFORE COMMENCING WORK. THE CONTRACTOR SHALL PROVIDE 48 HOURS MINIMUM NOTICE TO ALL UTILITY COMPANIES PRIOR TO BEGINNING

CONTRACTOR SHALL CONTACT UTILITY NOTIFICATION CENTER FOR THE LOCATION OF UNDERGROUND UTILITIES AT LEAST 48 HOURS PRIOR TO COMMENCEMENT OF CONSTRUCTION (1-800-922-1987).

5. CONSTRUCTION SHALL COMPLY WITH ALL GOVERNING CODES AND BE CONSTRUCTED TO SAME.

6. THE CONTRACTOR SHALL BE RESPONSIBLE TO OBTAIN ALL REQUIRED CONSTRUCTION PERMITS AND BONDS

7. THE CONTRACTOR SHALL HAVE AVAILABLE AT THE JOB SITE AT ALL TIMES ONE COPY OF THE COUNTY APPROVED DOCUMENTS INCLUDING PLANS, SPECIFICATIONS, SPECIAL CONDITIONS AND COPIES OF ANY REQUIRED CONSTRUCTION PERMITS, AND EROSION CONTROL PLANS AND INSPECTION REPORTS (SWMP).

ANY DISCREPANCIES ON THE DRAWINGS SHALL BE IMMEDIATELY BROUGHT TO THE ATTENTION OF THE OWNER AND ENGINEER BEFORE COMMENCING WORK. NO FIELD CHANGES OR DEVIATIONS FROM DESIGN ARE TO BE MADE WITHOUT PRIOR APPROVAL OF THE OWNER AND NOTIFICATION TO THE CEC.

9. ALL COPIES OF COMPACTION, CONCRETE AND OTHER REQUIRED TEST RESULTS ARE TO BE SENT TO THE OWNER AND CIVIL ENGINEER CONSULTANT OF RECORD DIRECTLY FROM THE TESTING AGENCY.

10. ALL NECESSARY INSPECTIONS AND/OR CERTIFICATIONS REQUIRED BY CODES, JURISDICTIONAL AGENCIES AND/OR UTILITY SERVICE COMPANIES SHALL BE PERFORMED PRIOR TO ANNOUNCED BUILDING POSSESSION AND

11. RECORD SURVEY: THE CONTRACTOR SHALL BE RESPONSIBLE FOR SUBMITTING TO THE ENGINEER A CERTIFIED RECORD SURVEY SIGNED AND SEALED BY A PROFESSIONAL LAND SURVEYOR REGISTERED IN THE STATE OF COLORADO DEPICTING THE ACTUAL FIELD LOCATION OF ALL CONSTRUCTED IMPROVEMENTS THAT ARE REQUIRED BY THE JURISDICTIONAL AGENCIES FOR THE CERTIFICATION PROCESS. SEE THE SPECIAL CONDITIONS INCLUDED IN THE CONTRACT DOCUMENTS FOR IMPROVEMENTS THAT REQUIRE A RECORD SURVEY. ALL SURVEY COST WILL BE THE CONTRACTORS RESPONSIBILITY.

12. THE CONTRACTOR SHALL FURNISH ALL NECESSARY MATERIALS, EQUIPMENT, MACHINERY, TOOLS, MEANS OF TRANSPORTATION AND LABOR NECESSARY TO COMPLETE THE WORK IN FULL AND COMPLETE IN ACCORDANCE WITH THE SHOWN, DESCRIBED AND REASONABLY INTENDED REQUIREMENTS OF THE CONTRACT DOCUMENTS AND JURISDICTIONAL AGENCY REQUIREMENTS. IN THE EVENT THAT THE CONTRACT DOCUMENTS AND THE JURISDICTIONAL AGENCY REQUIREMENTS ARE NOT IN AGREEMENT, THE MOST STRINGENT SHALL GOVERN.

13. THE CONTRACTOR SHALL RESTORE ALL DISTURBED VEGETATION IN KIND. UNLESS SHOWN OTHERWISE.

14. ALL PAVING, CONSTRUCTION, MATERIALS, AND WORKMANSHIP IN THE ADAMS COUNTY RIGHT-OF-WAY SHALL BE IN ACCORDANCE WITH CDOT STANDARDS & SPECIFICATIONS, CURRENT EDITION.

15. CONTRACTOR SHALL PROVIDE ALL LIGHTS, SIGNS, BARRICADES, FLAGGERS, AND ALL OTHER DEVICES NECESSARY TO PROVIDE FOR PUBLIC SAFETY IN ACCORDANCE WITH MUTCD CONSTRUCTION AREA TRAFFIC

16. CONTRACTOR TO VERIFY ELEVATIONS OF ALL EXISTING IMPROVEMENTS WHERE CONNECTIONS ARE TO BE MADE AND SHALL ADVISE ENGINEER OF ALL DISCREPANCIES PRIOR TO CONSTRUCTION.

17. CONTRACTOR SHALL BE RESPONSIBLE FOR DOCUMENTING AND MAINTAINING AS-BUILT INFORMATION (WHICH SHALL BE RECORDED) AS CONSTRUCTION PROGRESSES OR AT THE COMPLETION OF APPROPRIATE CONSTRUCTION INTERVAL(S) AND SHALL BE RESPONSIBLE FOR PROVIDING ALL APPLICABLE DATA OBTAINED TO THE OWNER AND ENGINEER FOR THE PURPOSE OF PREPARING FINAL AS-BUILT (RECORD) DRAWINGS. ALL AS-BUILT DATA SHALL BE COLLECTED BY A STATE OF COLORADO PROFESSIONAL LAND SURVEYOR WHOSE SERVICES ARE ENGAGED BY THE CONTRACTOR. AS-BUILT INFORMATION FOR FITTINGS AND OTHER BURIED APPURTENANT FEATURES SHALL INCLUDE SWING TIES TO THE FEATURE FROM TWO OF THE CLOSEST BUILDING

CONTRACTOR SHALL ADJUST AND/OR CUT EXISTING PAVEMENT AS NECESSARY TO ASSURE A SMOOTH FIT AND

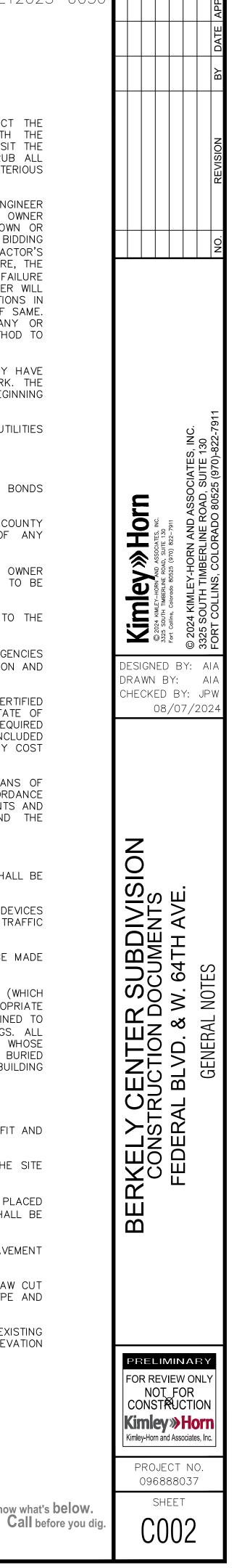
2. UNLESS OTHERWISE INDICATED ON THE PLANS OR THE SPECIFICATIONS, ALL CONCRETE USED ON THE SITE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 4,500 PSI IN 28 DAYS.

3. ALL CONCRETE SIDEWALKS SHALL HAVE CONTROL JOINTS CUT ON 5' CENTERS AND EXPANSION JOINTS PLACED ON 100' CENTERS, SEE ADAMS COUNTY CONCRETE SIDEWALK DETAIL. CONCRETE PAVEMENT JOINTS SHALL BE SPACED AT 12' CENTERS MAXIMUM OR AS DIRECTED BY THE COUNTY.

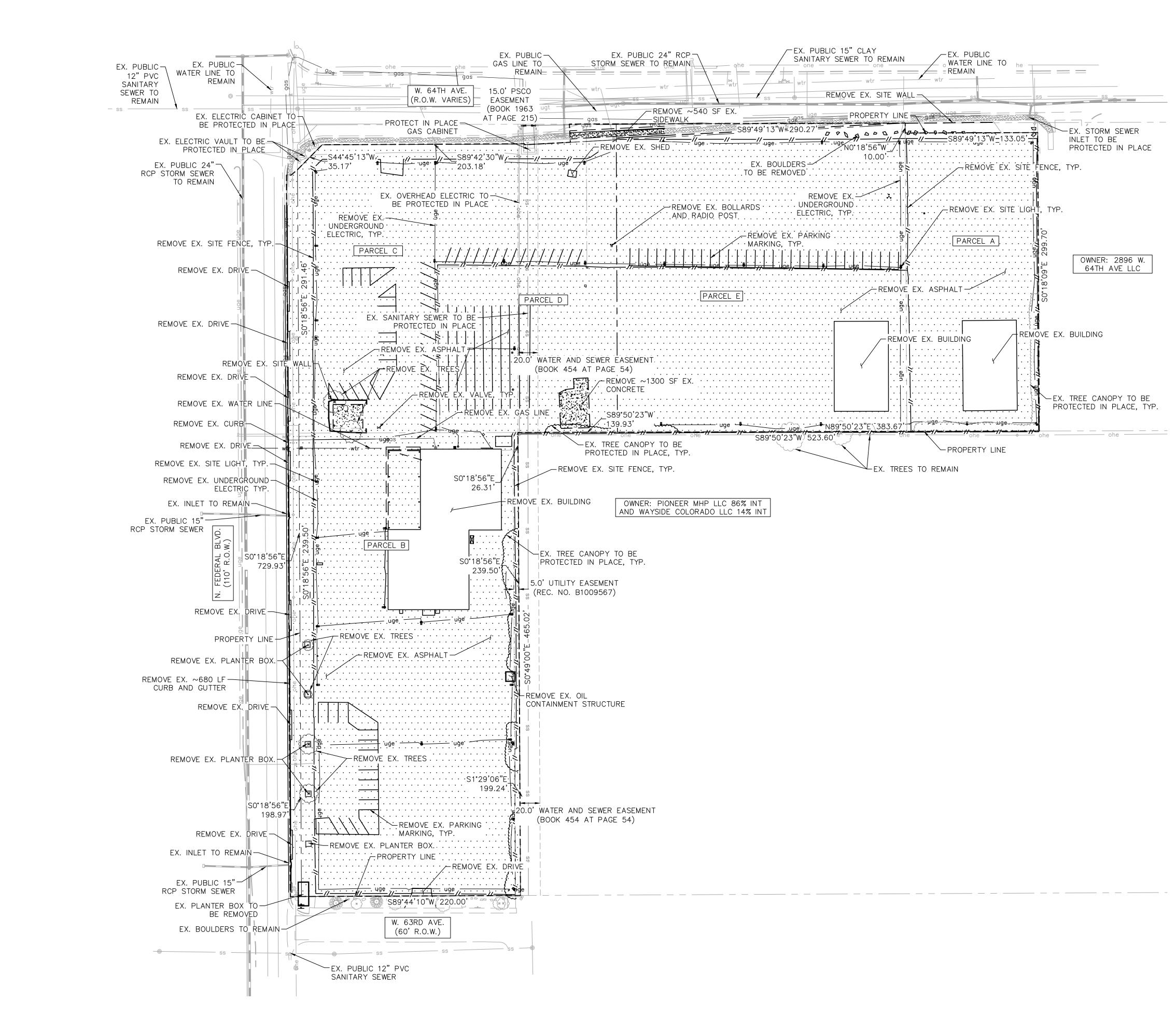
ALL AREAS INDICATED AS PAVEMENT SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE TYPICAL PAVEMENT SECTIONS AS INDICATED ON THE DRAWINGS. ROW PAVEMENT SHALL BE AS DIRECTED BY THE COUNTY.

WHERE EXISTING PAVEMENT IS INDICATED TO BE REMOVED AND REPLACED. THE CONTRACTOR SHALL SAW CUT FULL DEPTH FOR A SMOOTH AND STRAIGHT JOINT AND REPLACE THE PAVEMENT WITH THE SAME TYPE AND DEPTH OF MATERIAL AS EXISTING OR AS INDICATED BY THE COUNTY.

WHERE NEW PAVEMENT MEETS THE EXISTING PAVEMENT, THE CONTRACTOR SHALL SAW CUT THE EXISTING PAVEMENT FULL DEPTH FOR A SMOOTH AND STRAIGHT JOINT AND MATCH THE EXISTING PAVEMENT ELEVATION WITH THE PROPOSED PAVEMENT UNLESS OTHERWISE INDICATED.







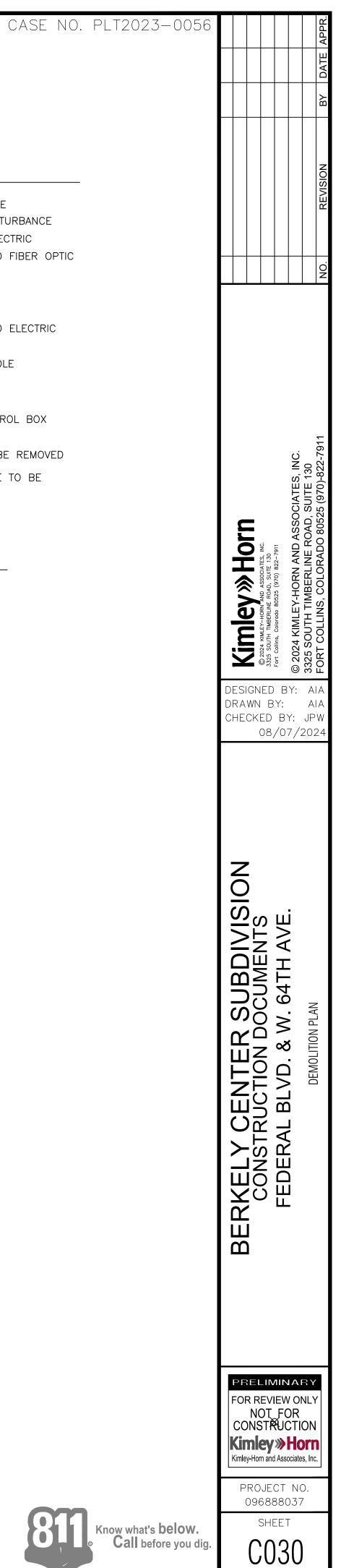
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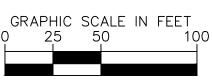
PROPERTY LINE LIMITS OF DISTURBANCE OVERHEAD ELECTRIC UNDERGROUND FIBER OPTIC GAS LINE WATER LINE SEWER LINE UNDERGROUND ELECTRIC LIGHT POLE UTILITY MANHOLE UTILITY METER UTILITY VALVE TRAFFIC CONTROL BOX CURB LINE ASPHALT TO BE REMOVED EX. CONCRETE TO BE REMOVED SAWCUT LINE

MISCELLANEOUS DEMOLITION NOTES

- . ALL ITEMS IN BOLD ARE TO BE DEMOLISHED. ALL TREES AND SHRUBS (EXCEPT THOSE SPECIFIED
- TO REMAIN) ON PROPERTY TO BE REMOVED. 3. CONTRACTOR SHALL COORDINATE WITH XCEL ENERGY
- FOR THE REMOVAL OF EXISTING OVERHEAD ELECTRIC AND ELECTRICAL STRUCTURES.

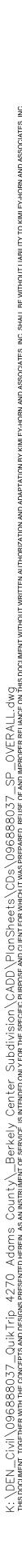


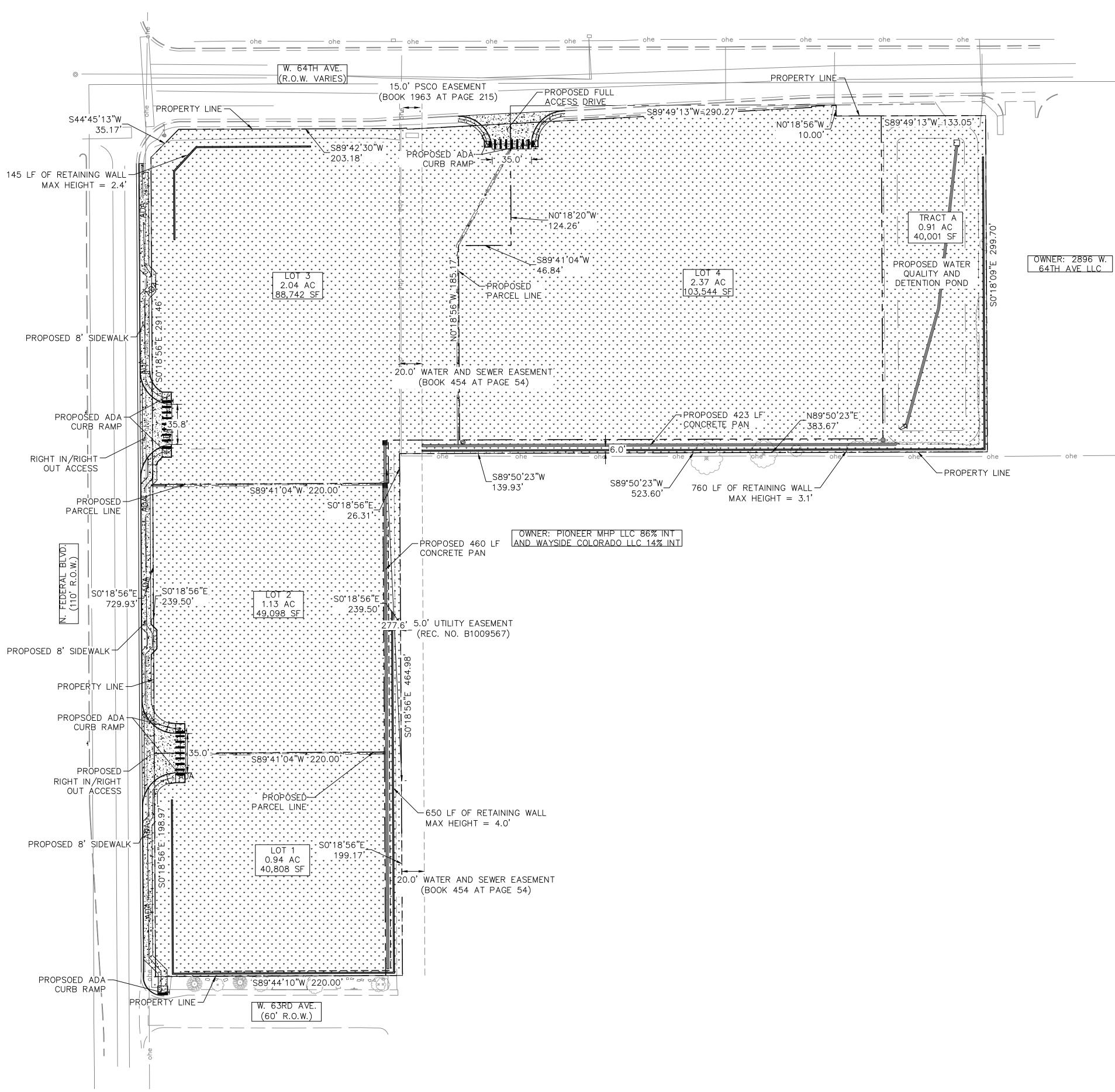




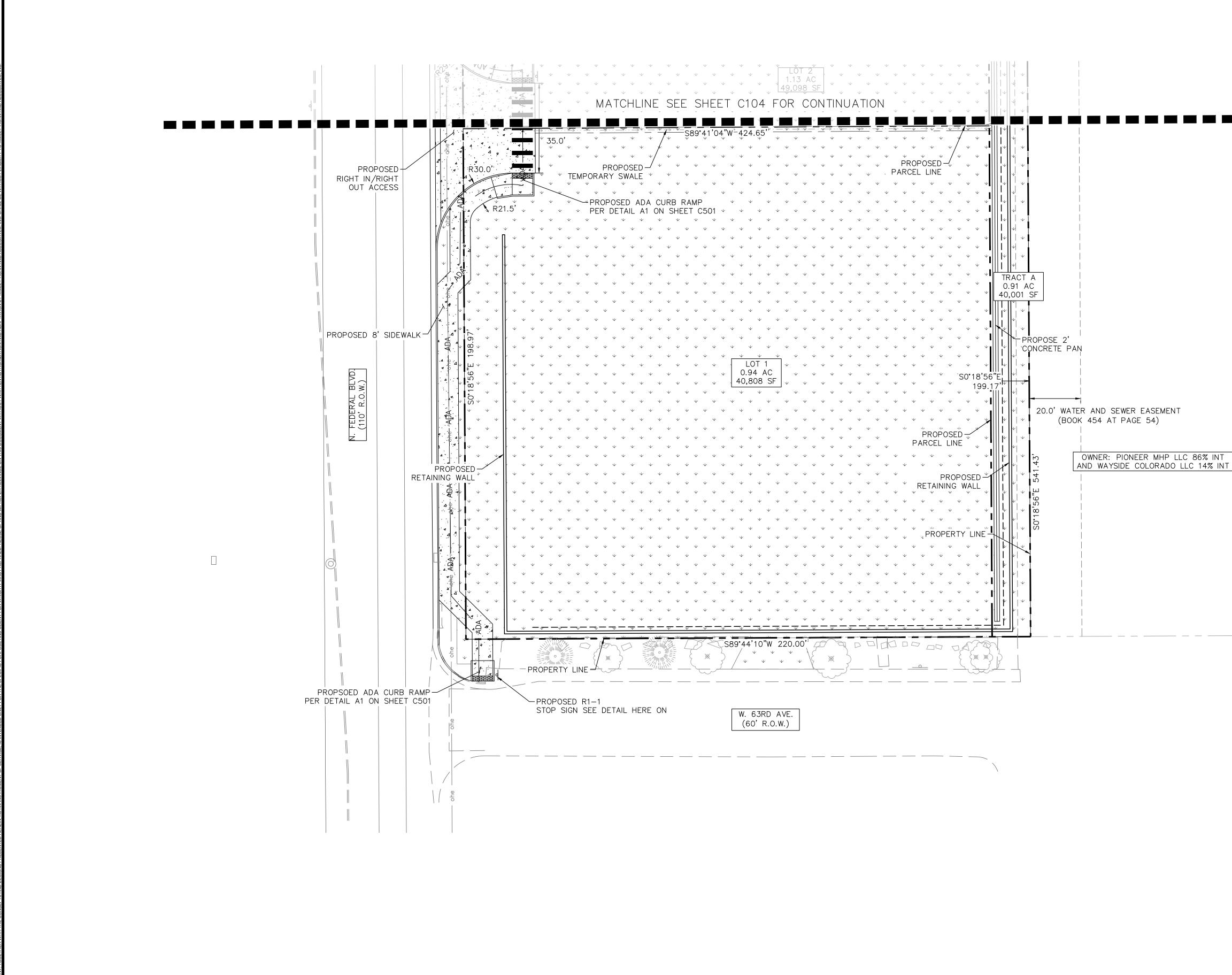


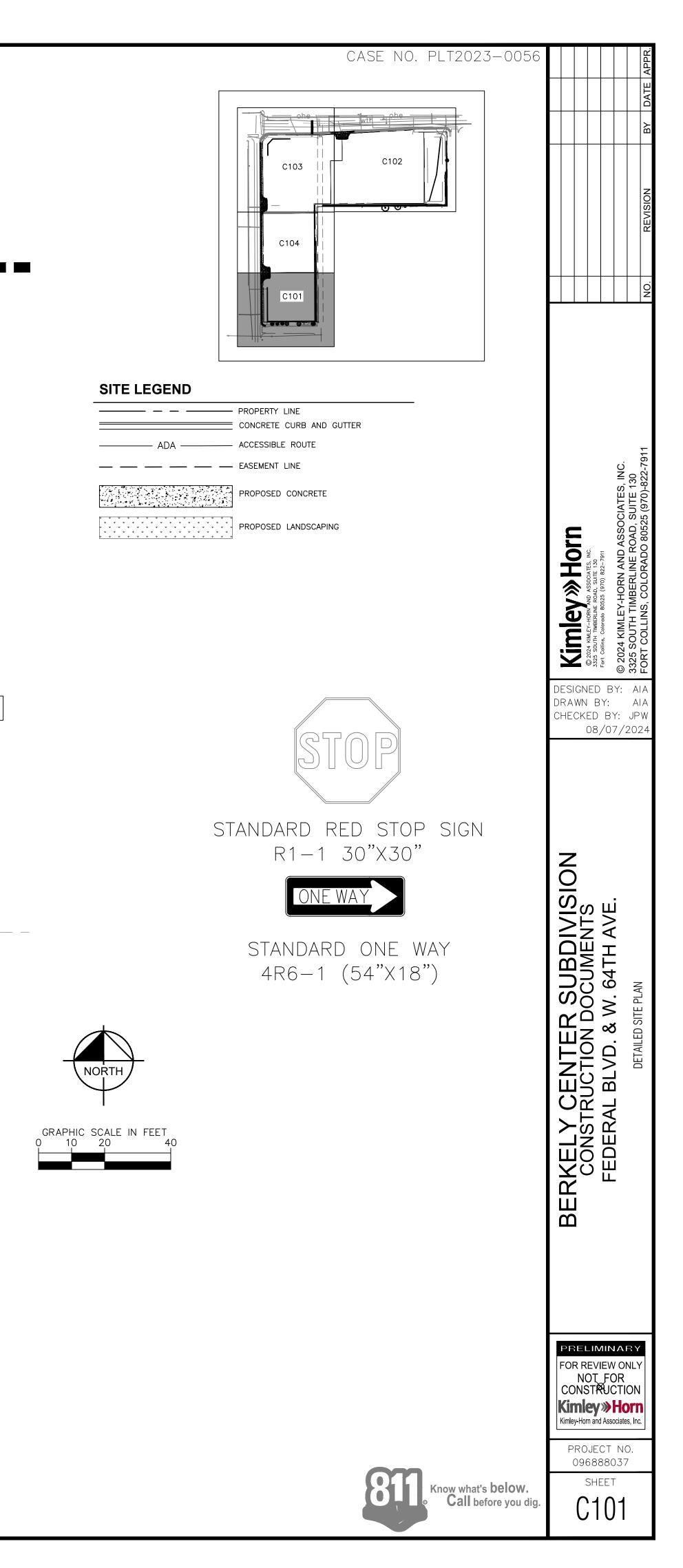
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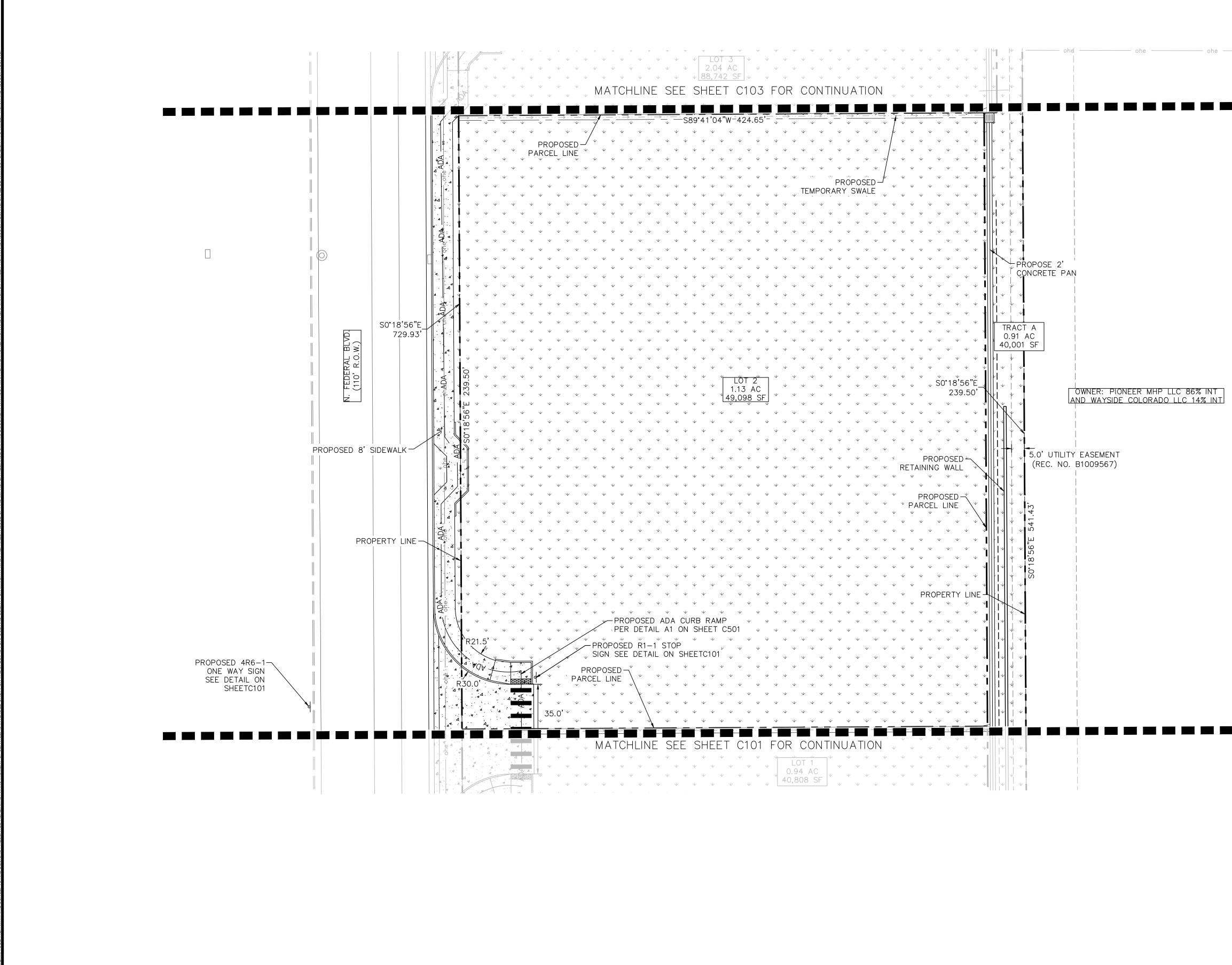


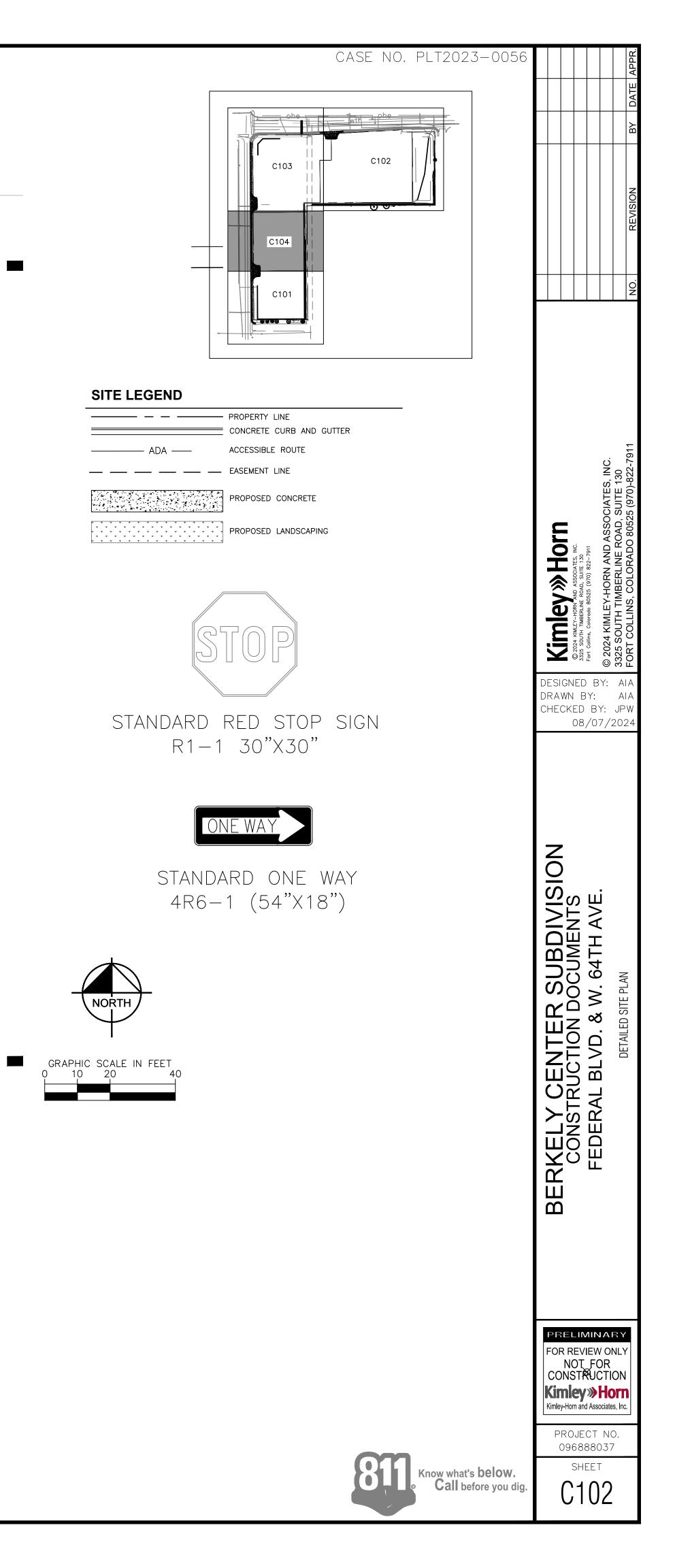


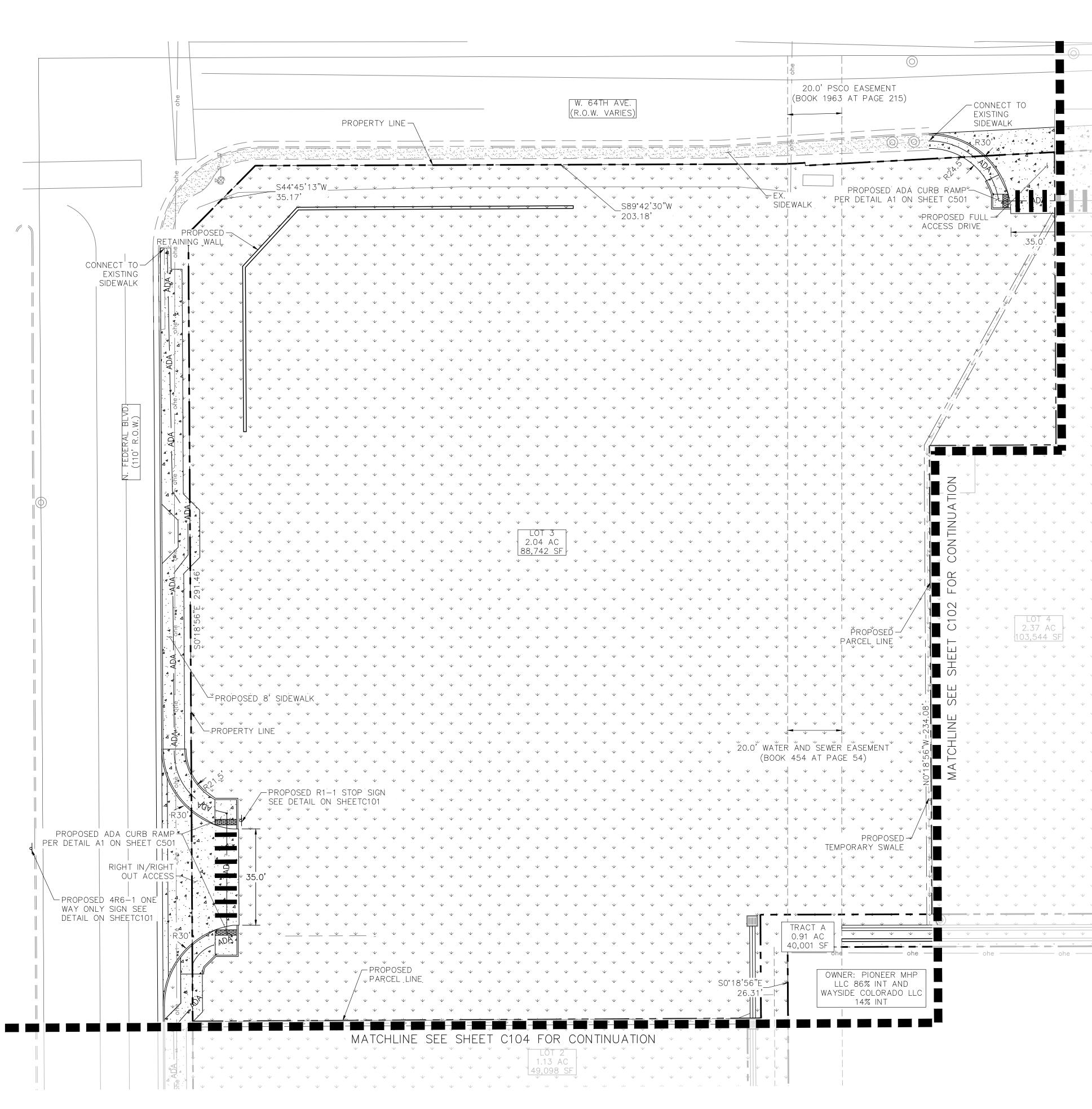
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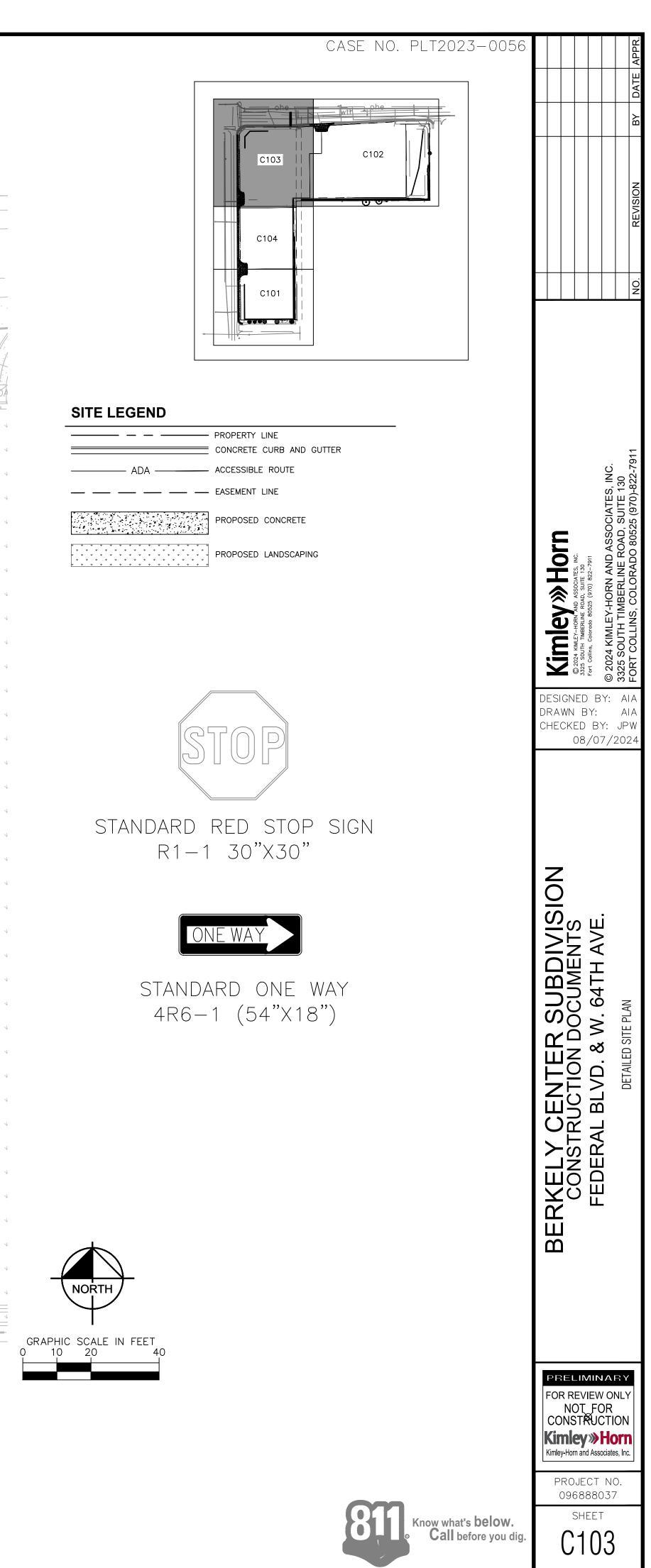




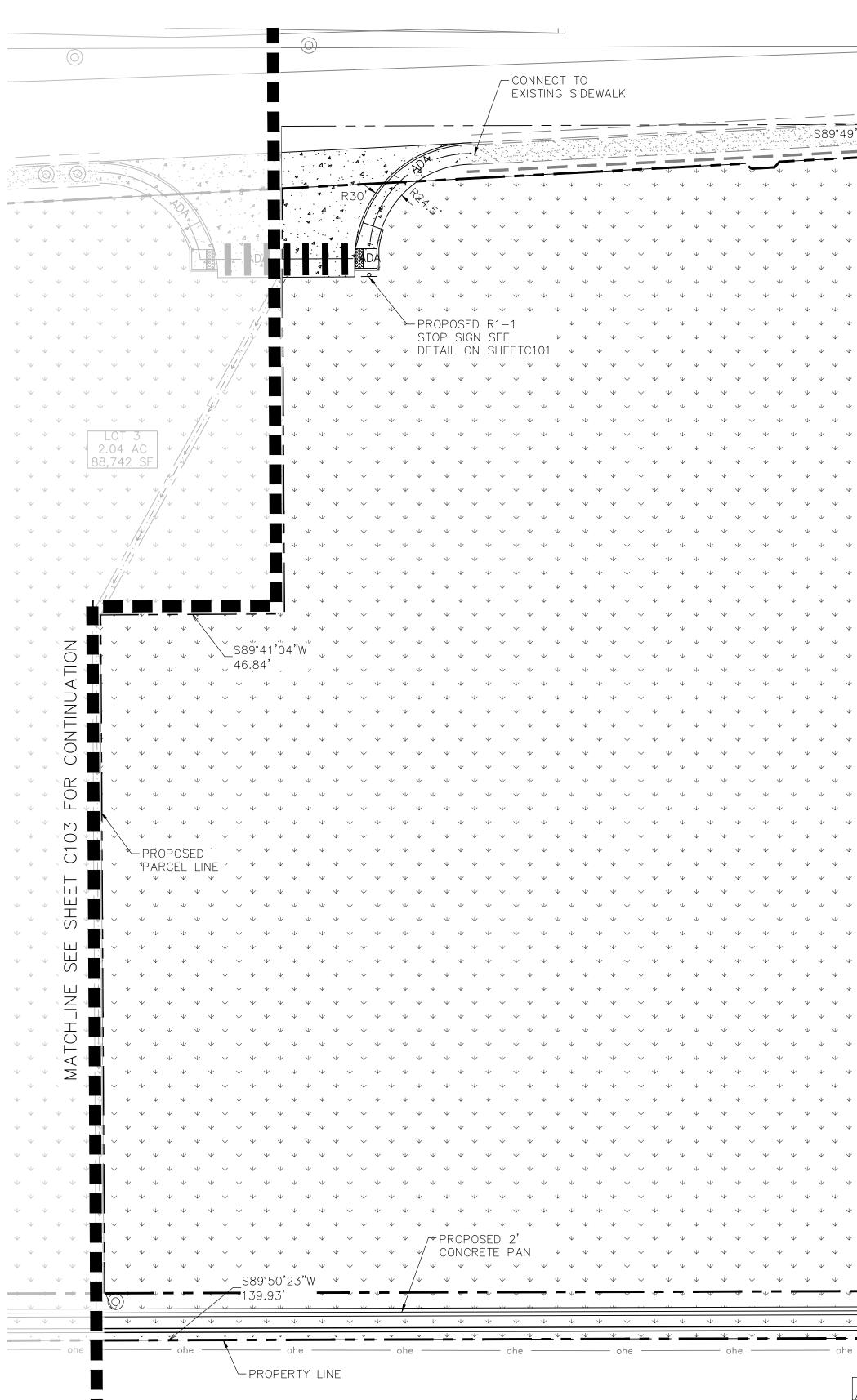




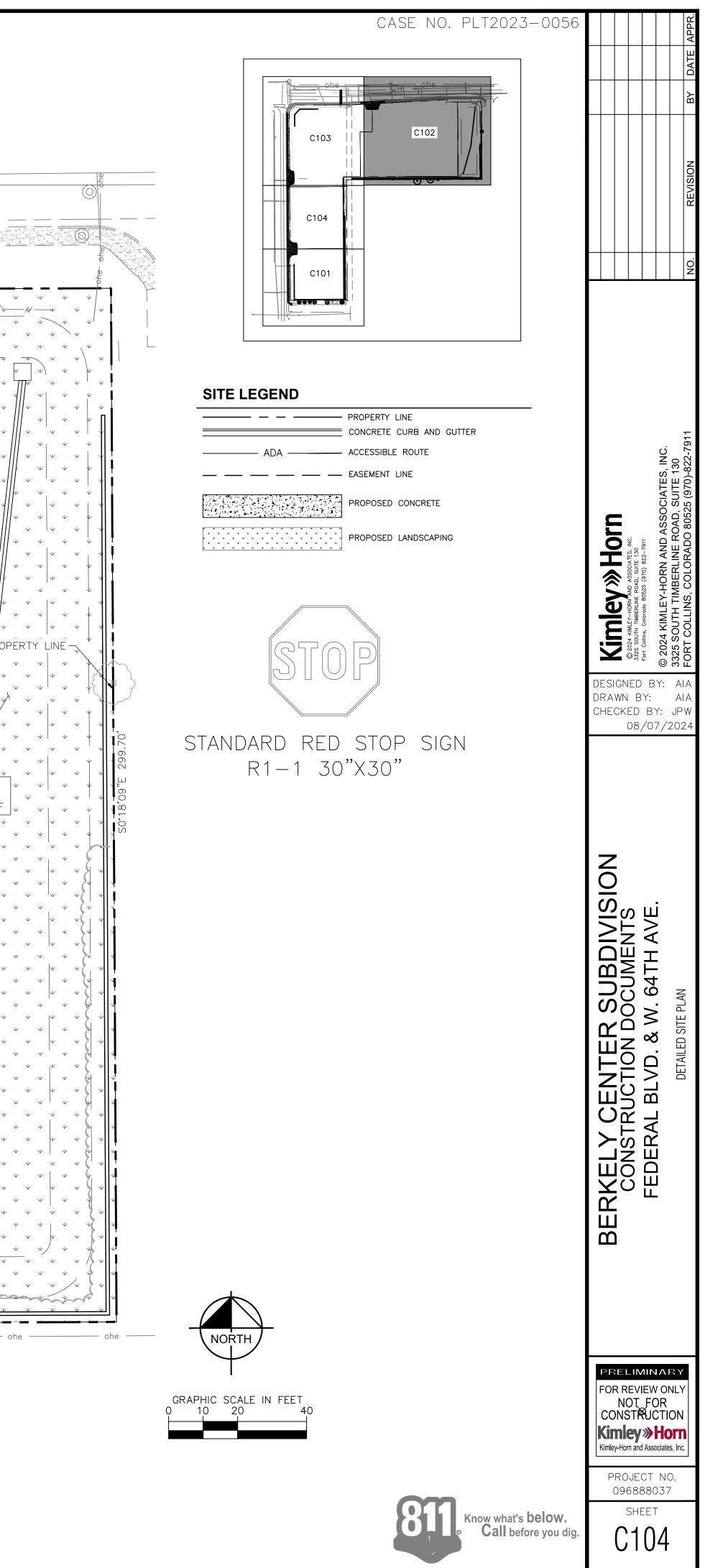


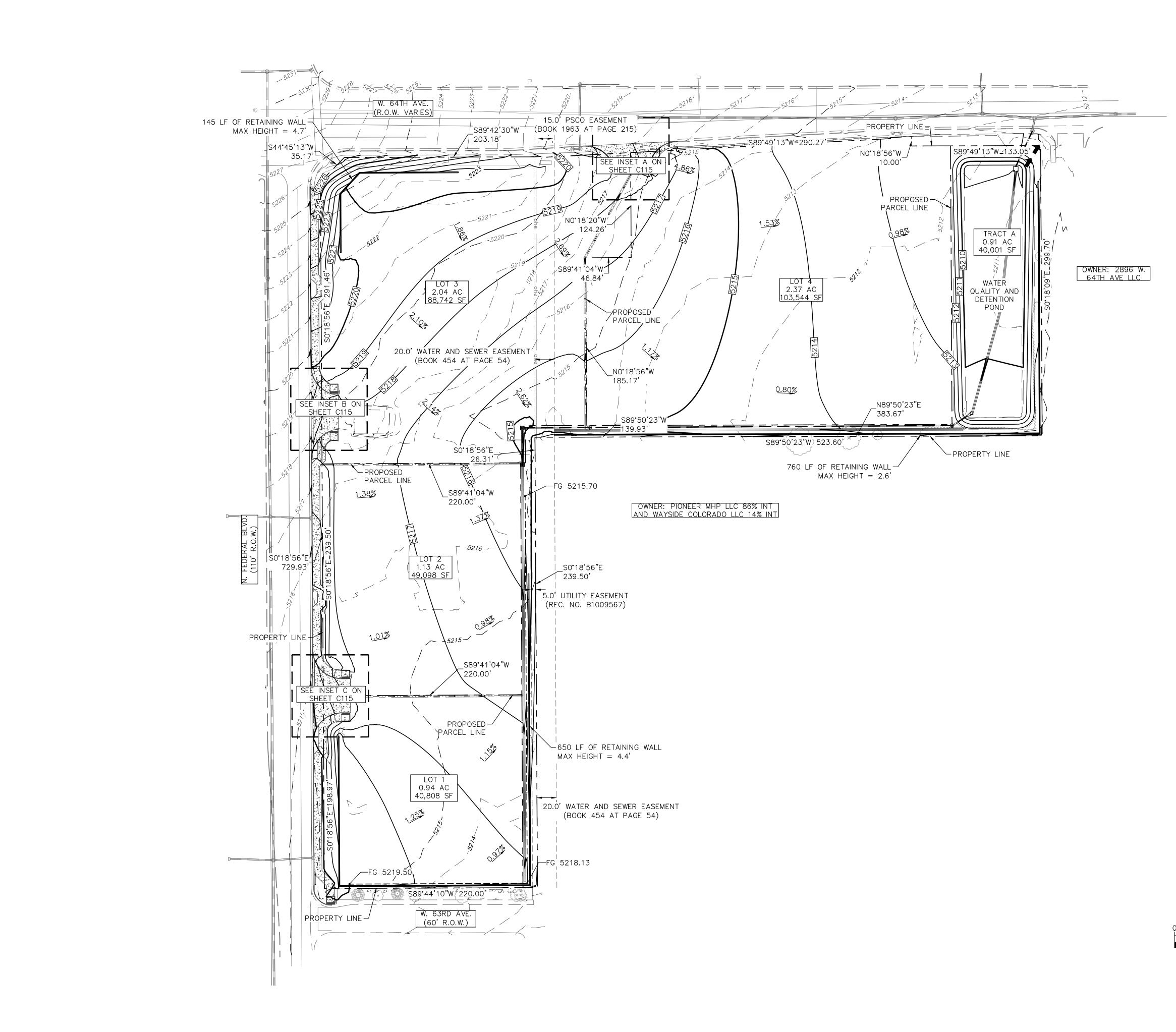


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CASE NO. PLT2023-0056

GRADING LEGEND

| XXXX XXXX XXXX XXXX | PROPERTY LINE MAJOR CONTOUR (NEW) MINOR CONTOUR (NEW) MAJOR CONTOUR (EXISTING) MINOR CONTOUR (EXISTING) LIMITS OF DISTURBANCE |
|--|--|
| TW XXXX.XX BW XXXX.XX TC XXXX.XX FL XXXX.XX | TOP OF WALL ELEVATION (NEW) BOTTOM OF WALL ELEVATION (NEW) TOP OF CURB ELEVATION (NEW) FLOWLINE ELEVATION (NEW) |
| FG XXXX.XX SW XXXX.XX ME XXXX.XX | FINISHED GRADE ELEVATION (NEW) SIDEWALK ELEVATION (NEW) SPOT ELEVATION (EXISTING) STORM GRATE (NEW) |
| | GRADE BREAK EASEMENT LINE |

BENCHMARKS

VERTICAL RELIEF WAS MADE FROM AN ON THE GROUND SURVEY, CONTOURS SHOWN HEREON ARE AT 1' INTERVALS USING THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAD88), GEOID 12A. SITE VERTICAL WAS ESTABLISHED BY USING COUNTY OF DENVER BENCH MARK "156B" LOCATED AT THE SOUTHEAST CORNER OF 50TH AVENUE AND FEDERAL BOULEVARD.

UNADJUSTED EARTHWORK QUANTITIES

CUT: 4,414 CY FILL: 15,284 CY NET: 10,870 CY (FILL)

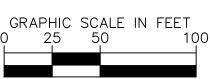
QUANTITIES NOTED ARE UNADJUSTED AND DO NOT ACCOUNT FOR OVER-EXCAVATION, PAVEMENT SECTIONS, OR SHRINK/WELL.

MISCELLANEOUS GRADING NOTES

- 1. GAS CANOPY INSTALLER SHALL INSTALL THE CANOPY COLUMN DRAIN PIPE AND OVERFLOW FITTING. THE STORM WATER INSTALLER SHALL CONNECT THEIR PIPING TO THE GAS INSTALLER'S OVERFLOW FITTING.
- WHEN PLAN GRADES DEPICT RUNOFF TO BE DIRECTED AWAY FROM THE CURB, USE DRAIN AWAY CURB (SPILL CURB) ALTERNATE. (RE: "CURB DETAIL-BARRIER" DETAIL)
- 3. SEE CITY OF LAKEWOOD GRADING NOTES ON SHEET COO2 OF THIS PLAN SET.

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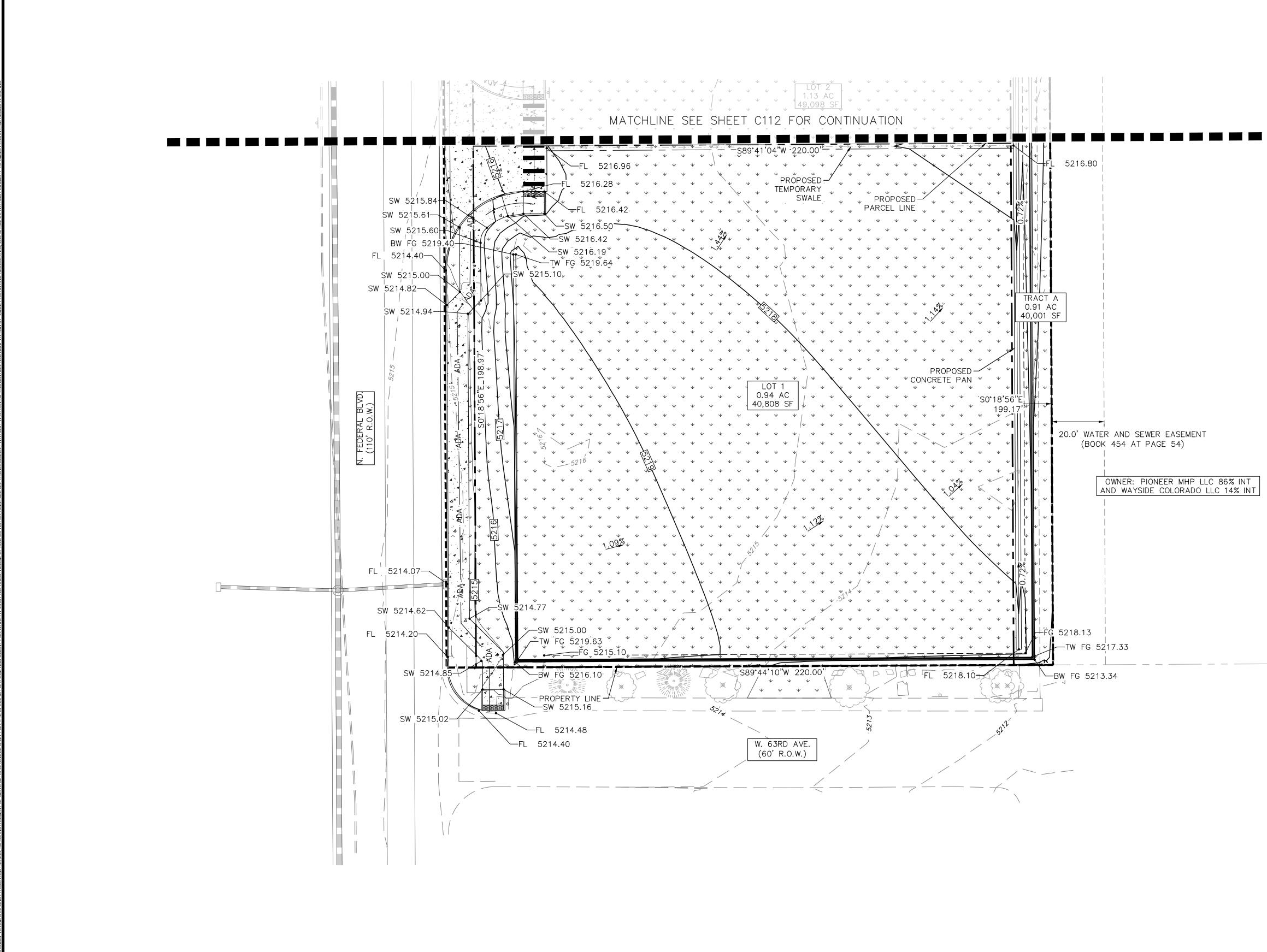
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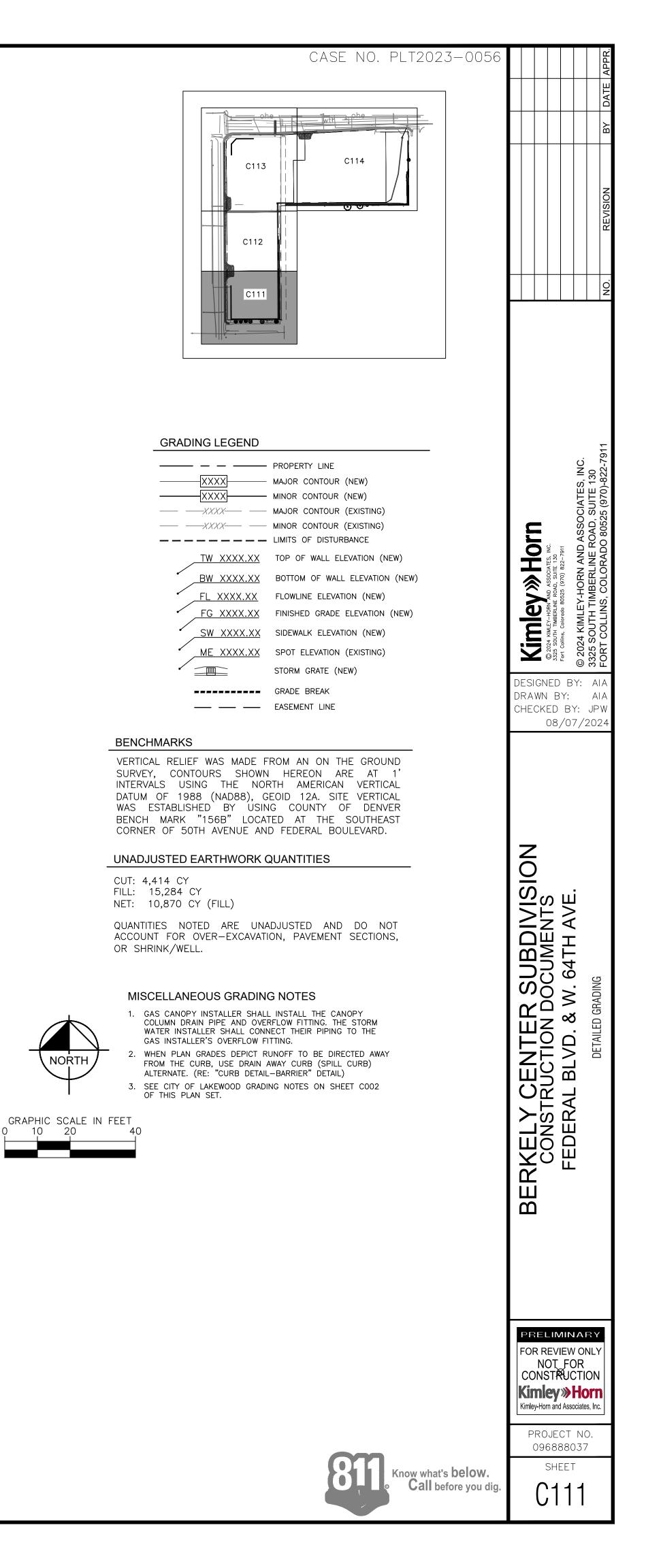
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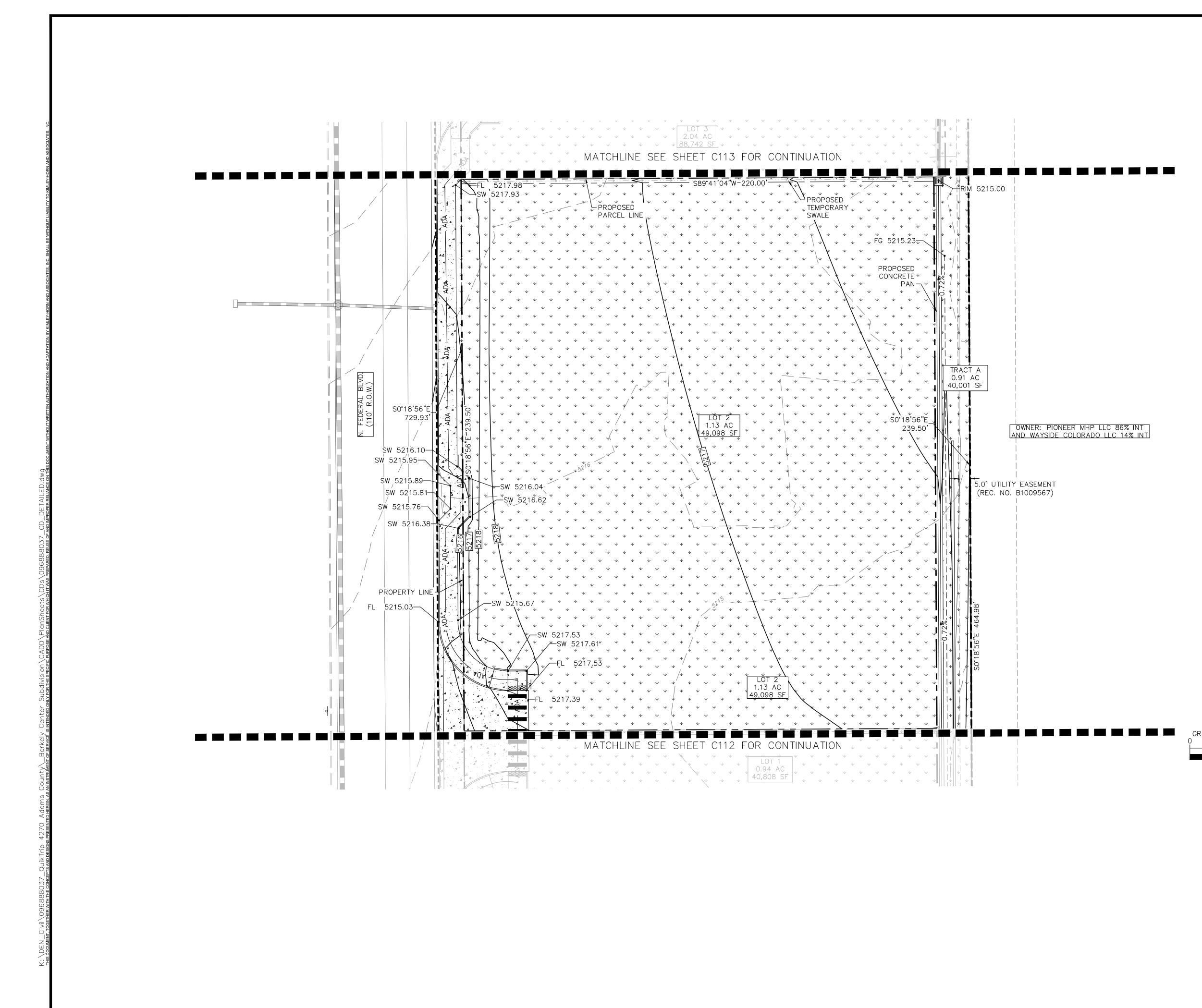
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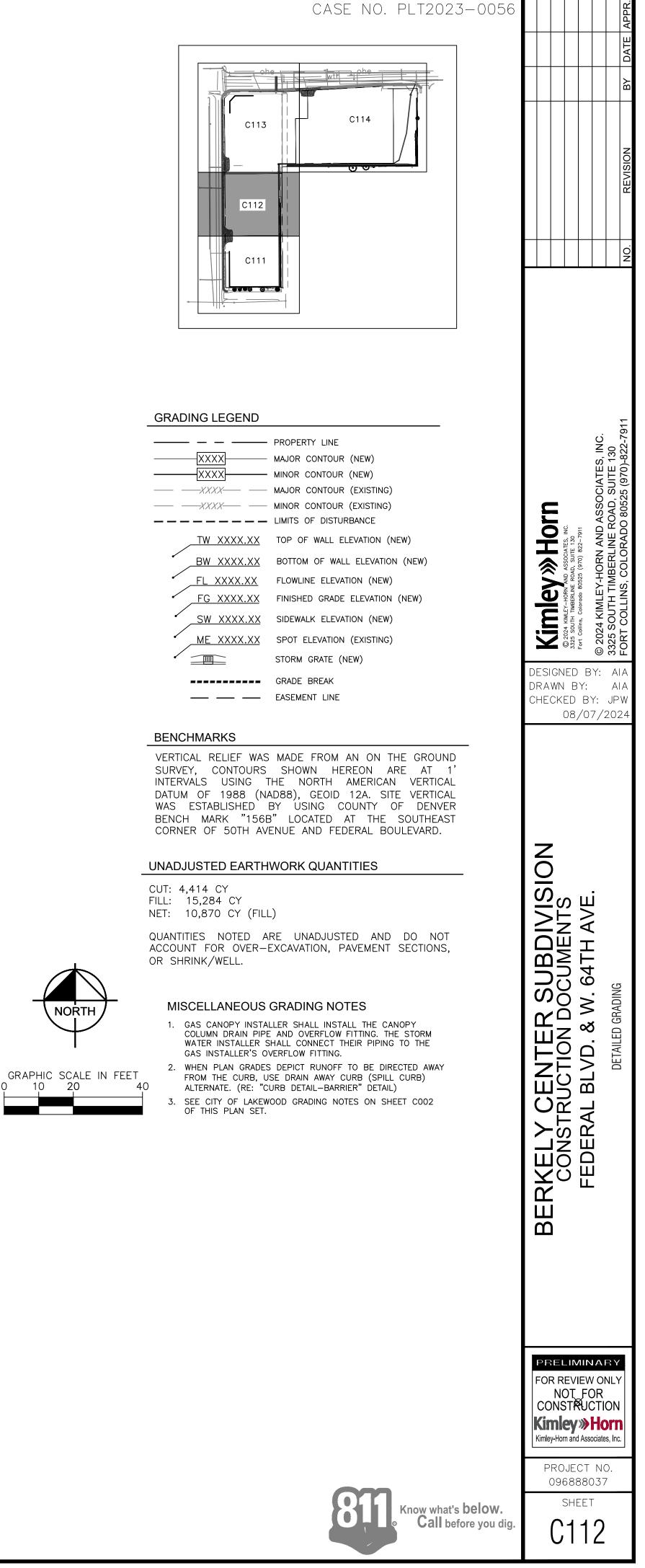
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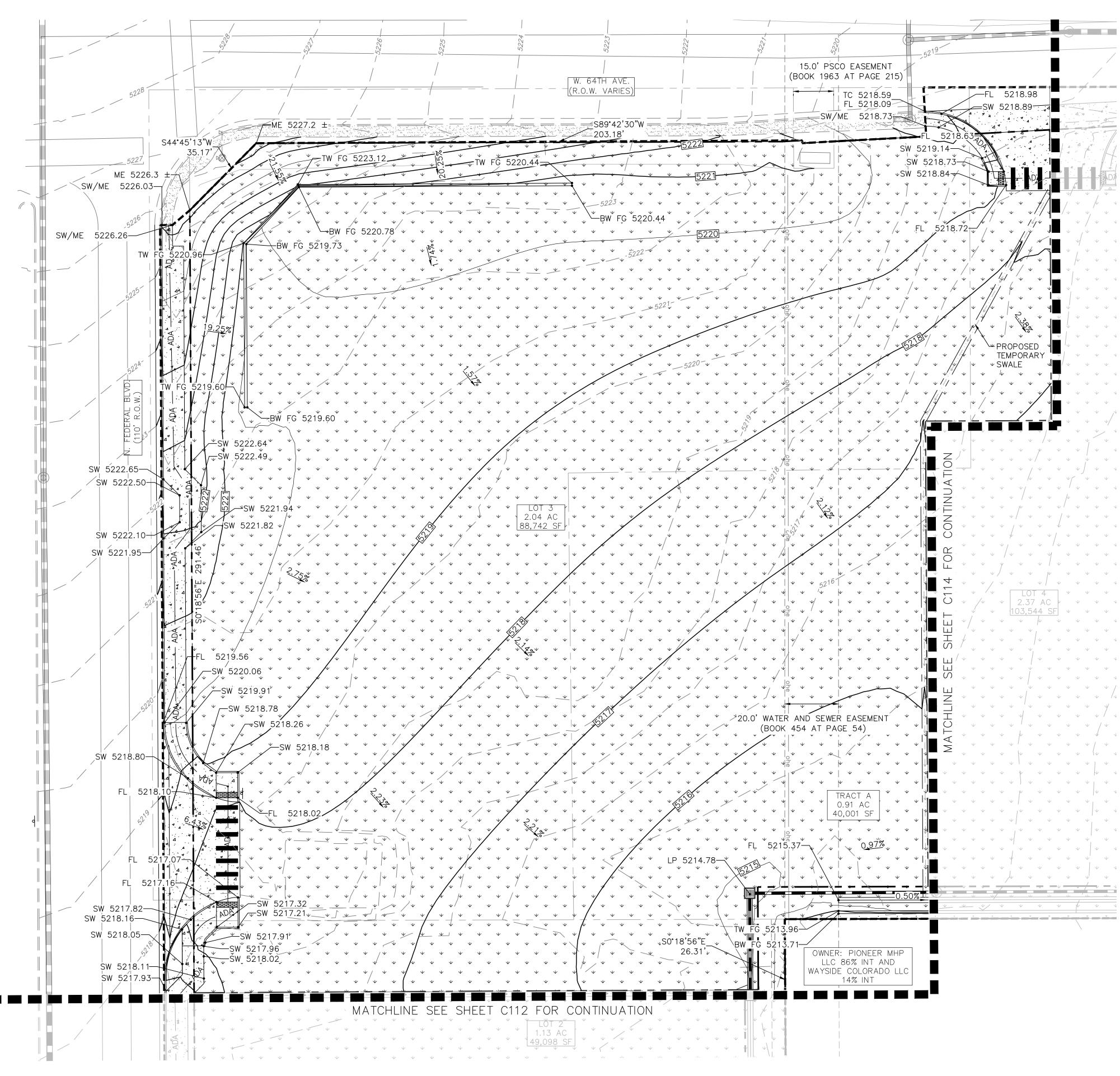


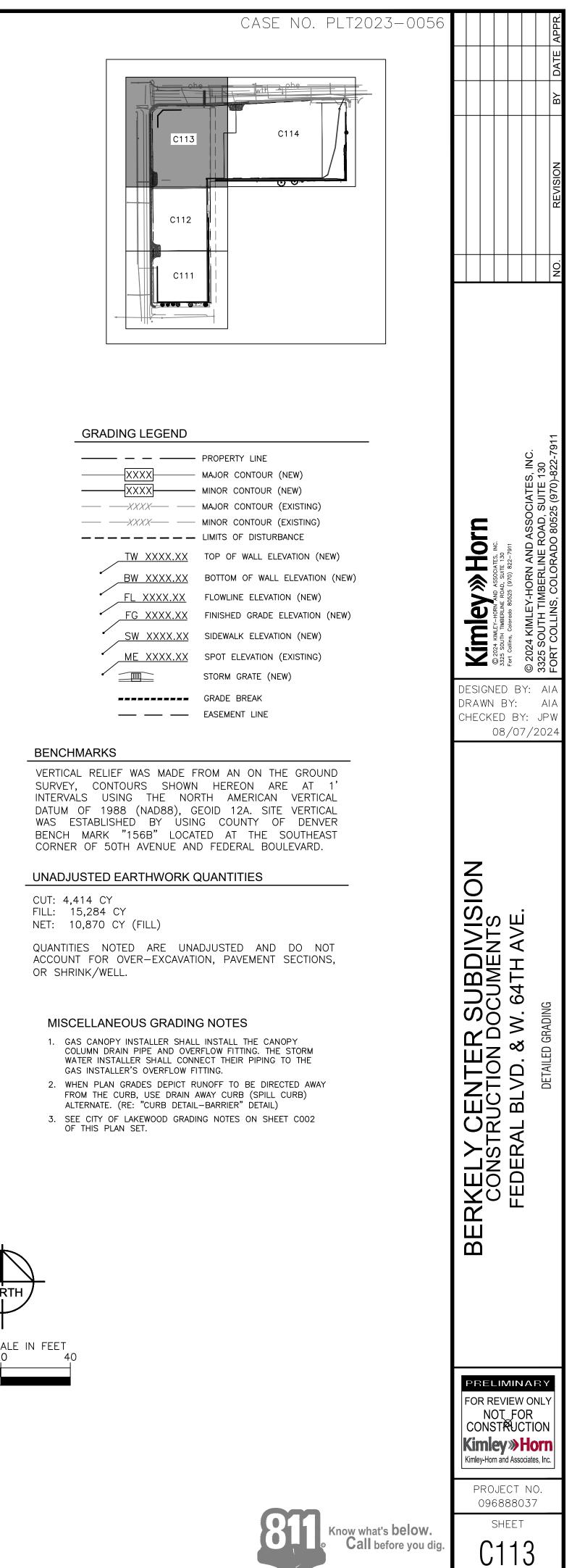




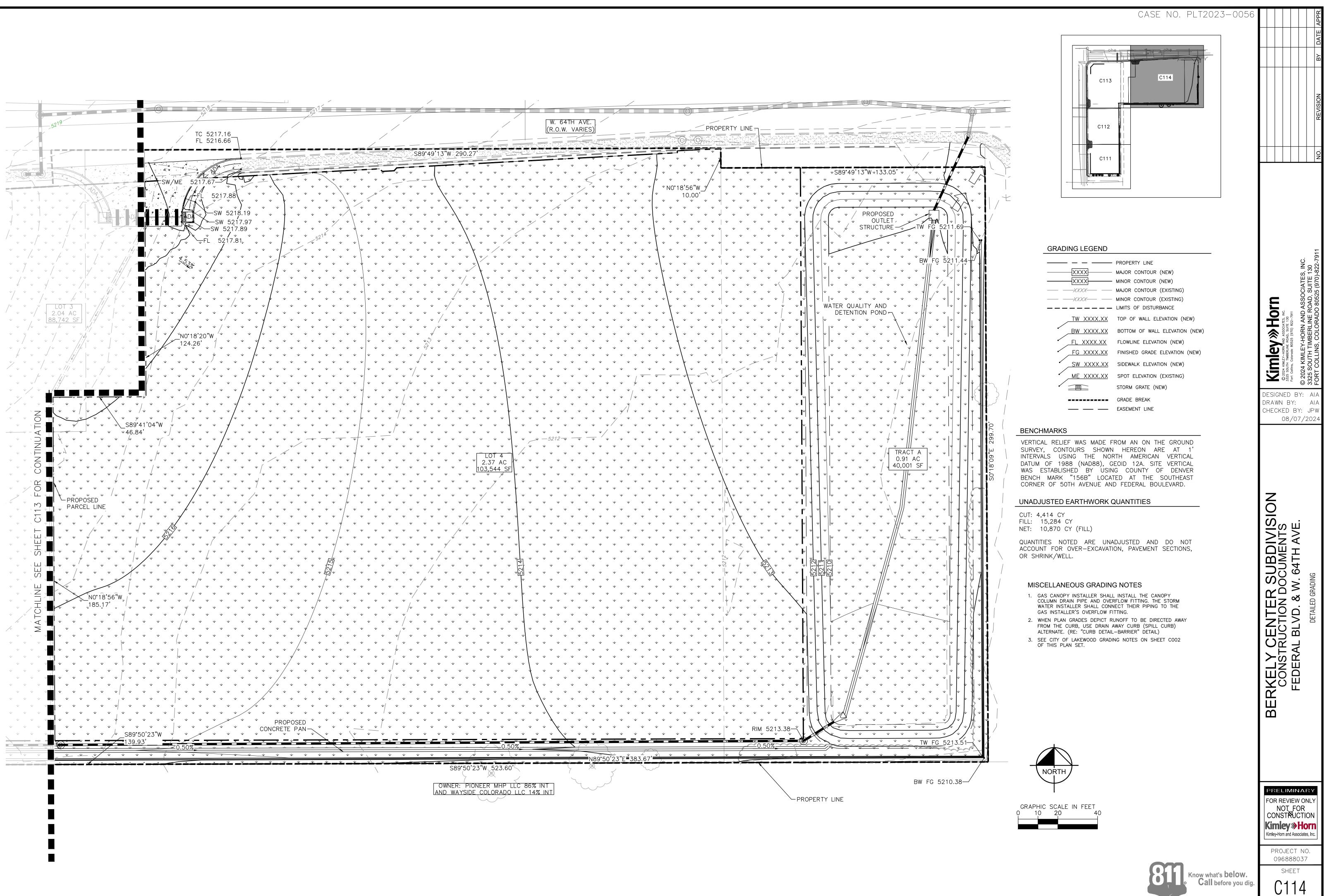


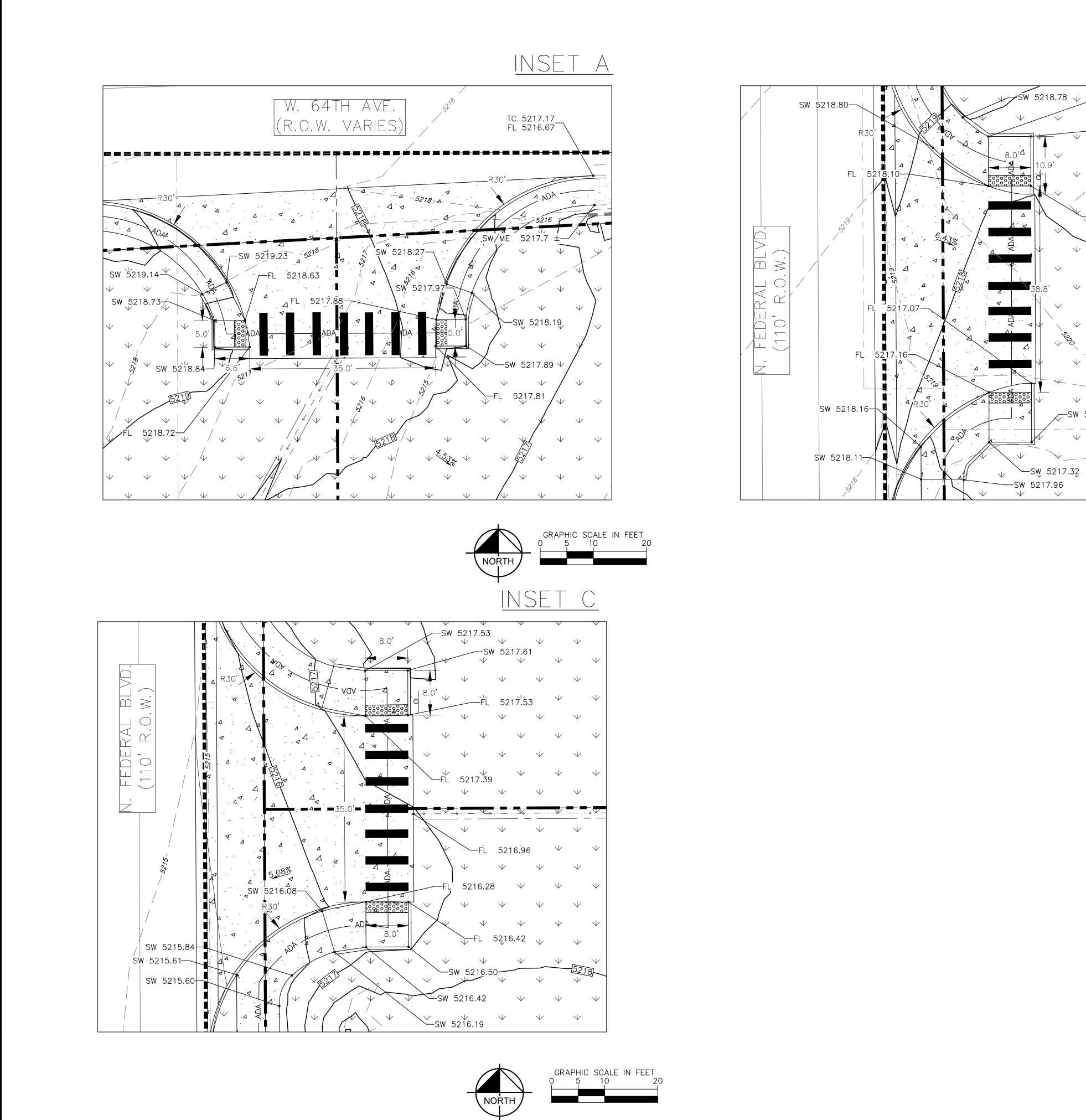


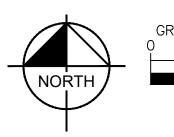




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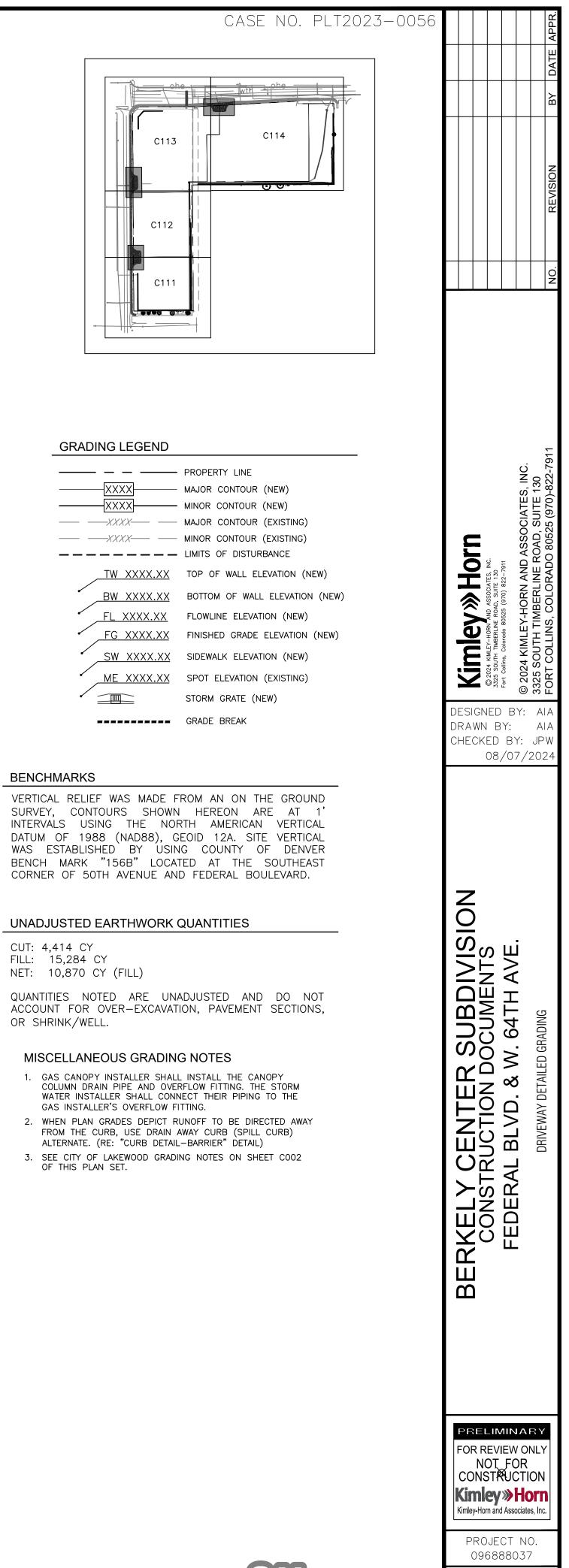
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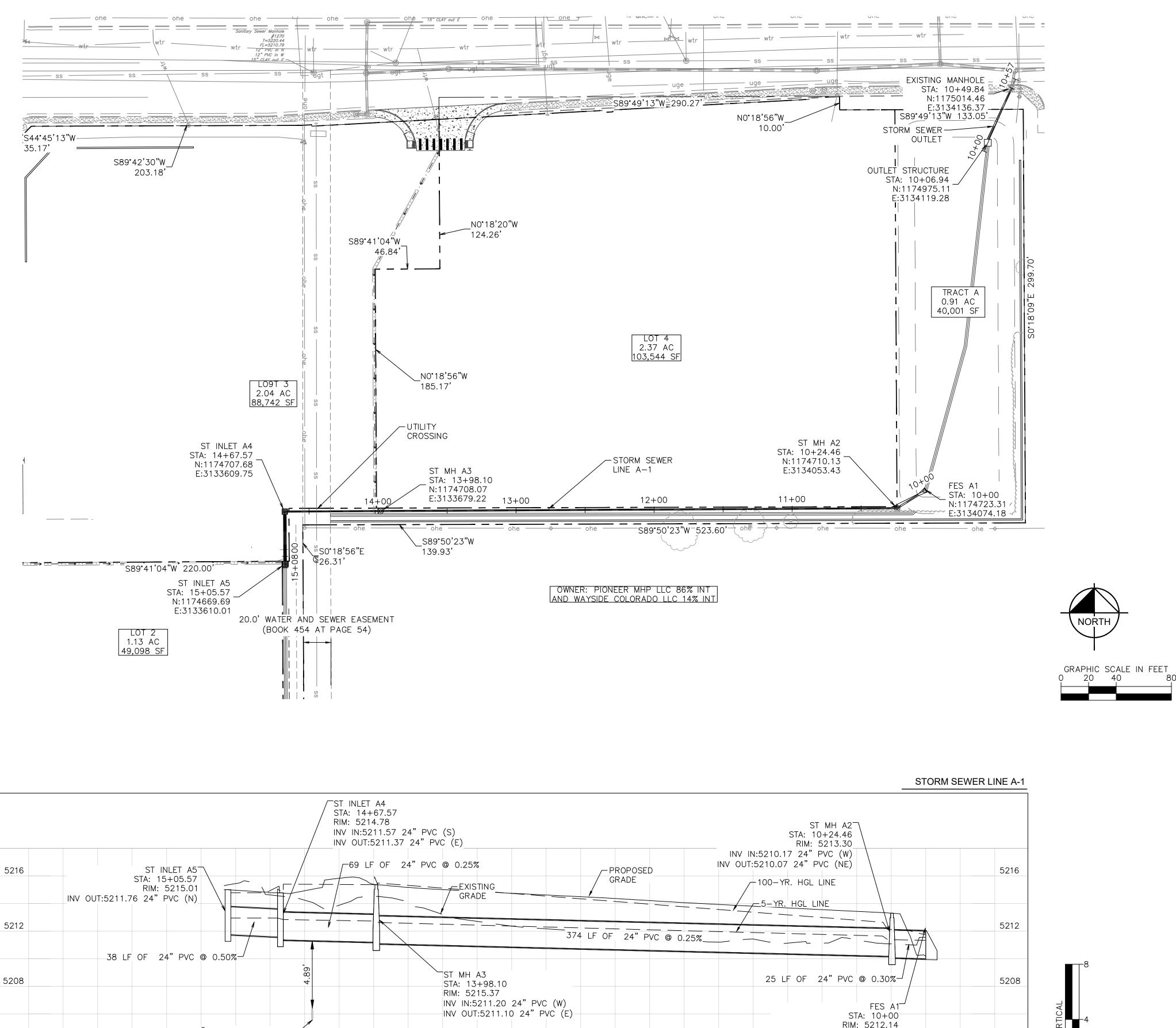
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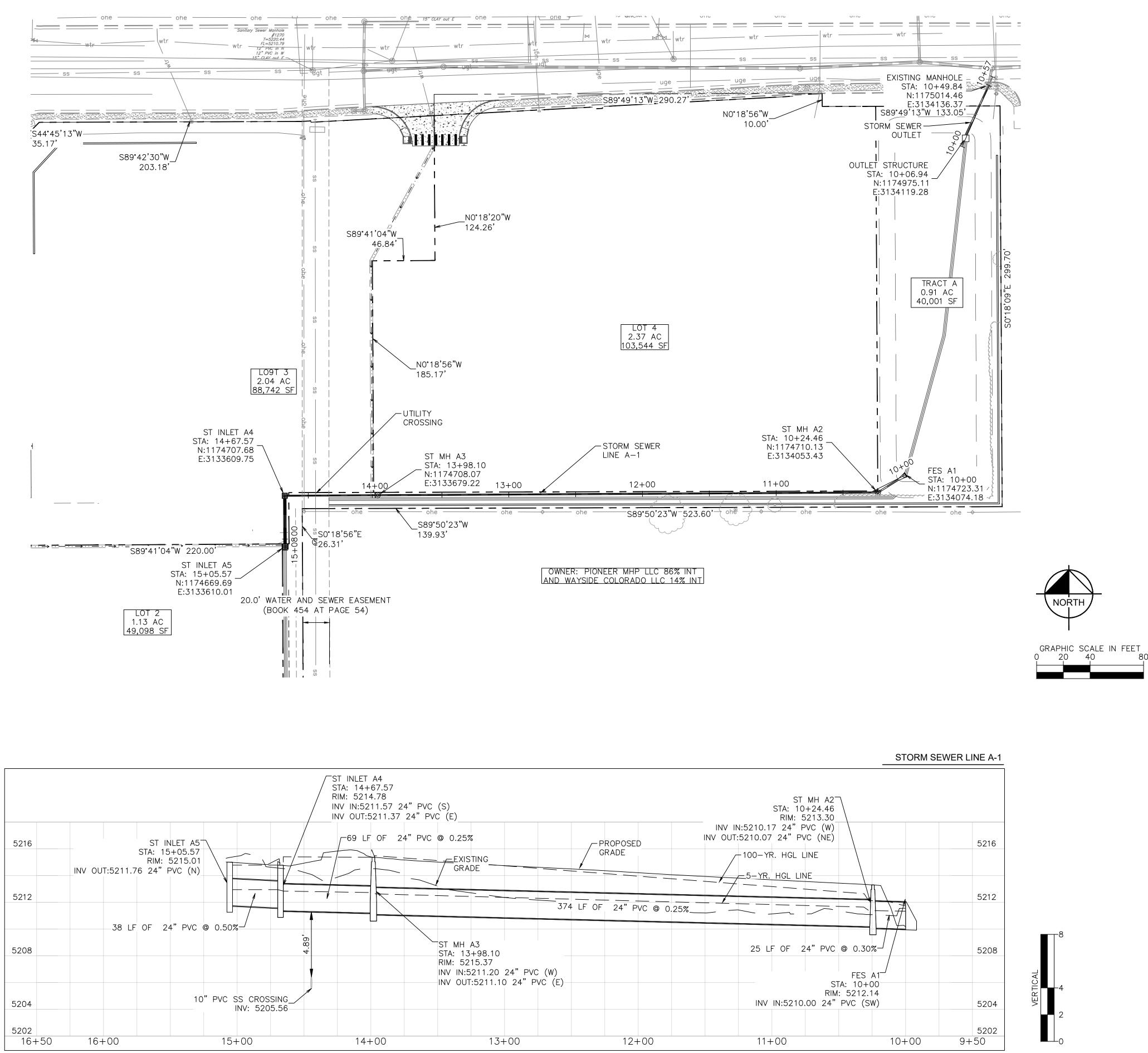
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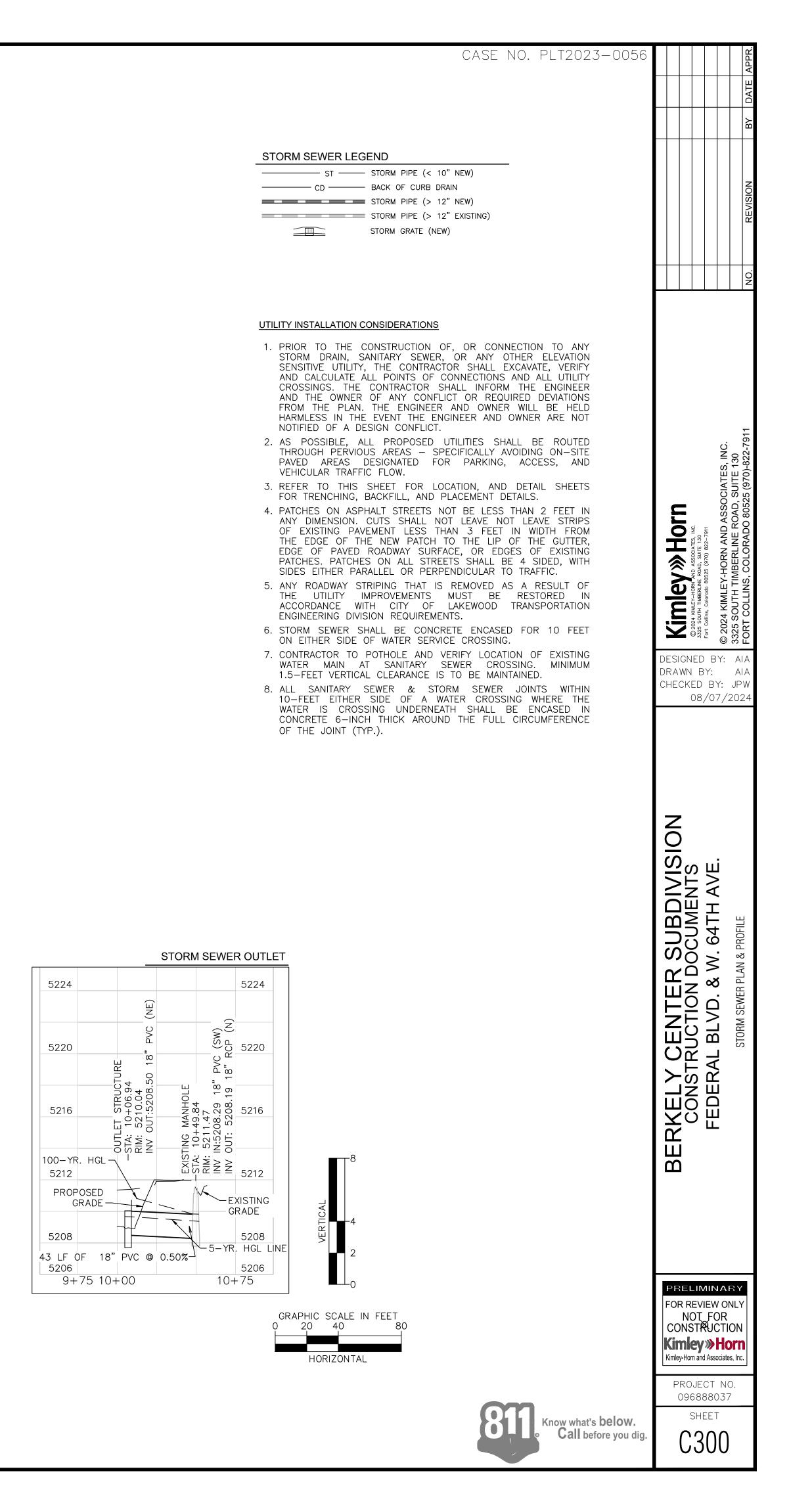
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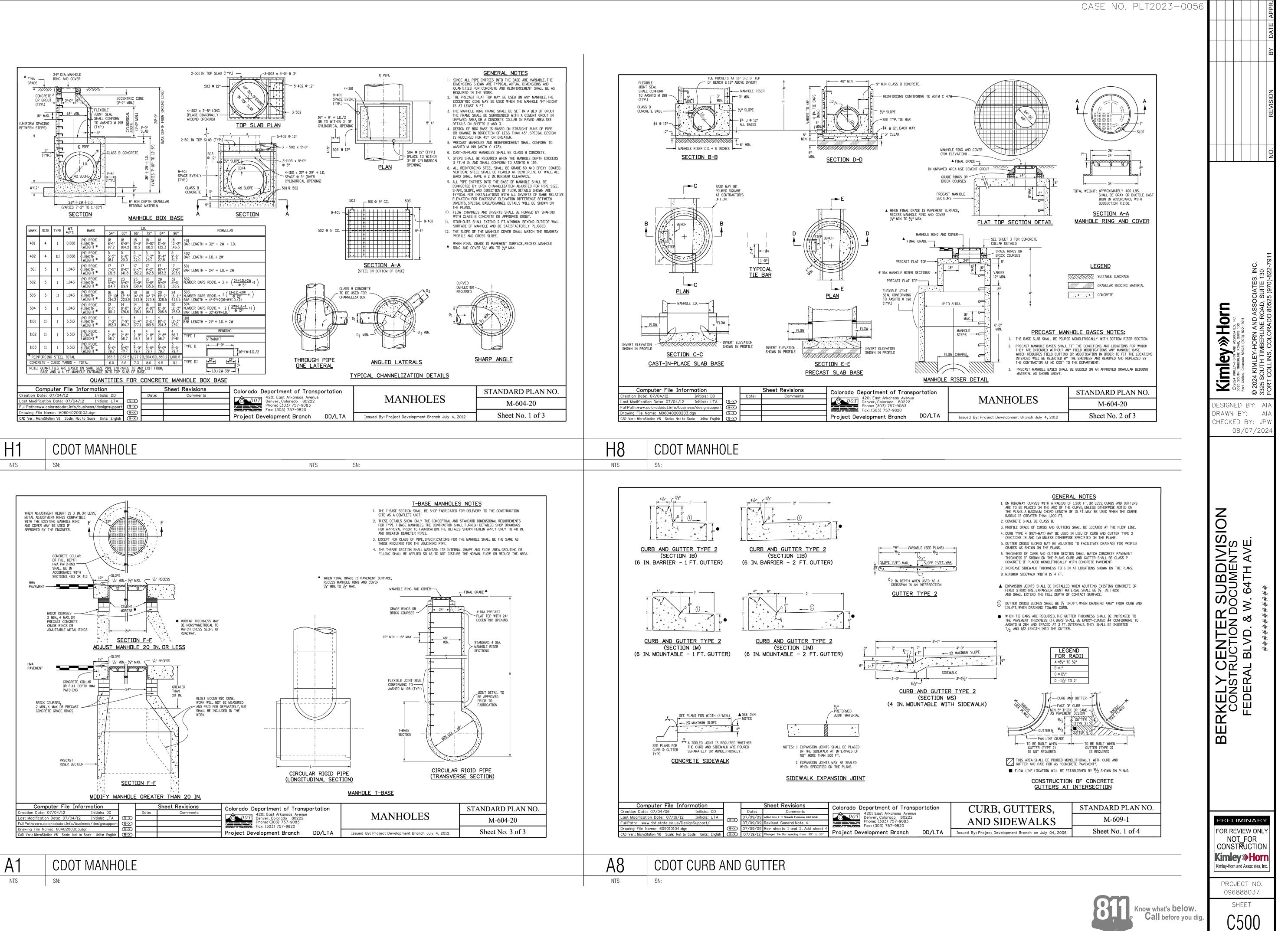
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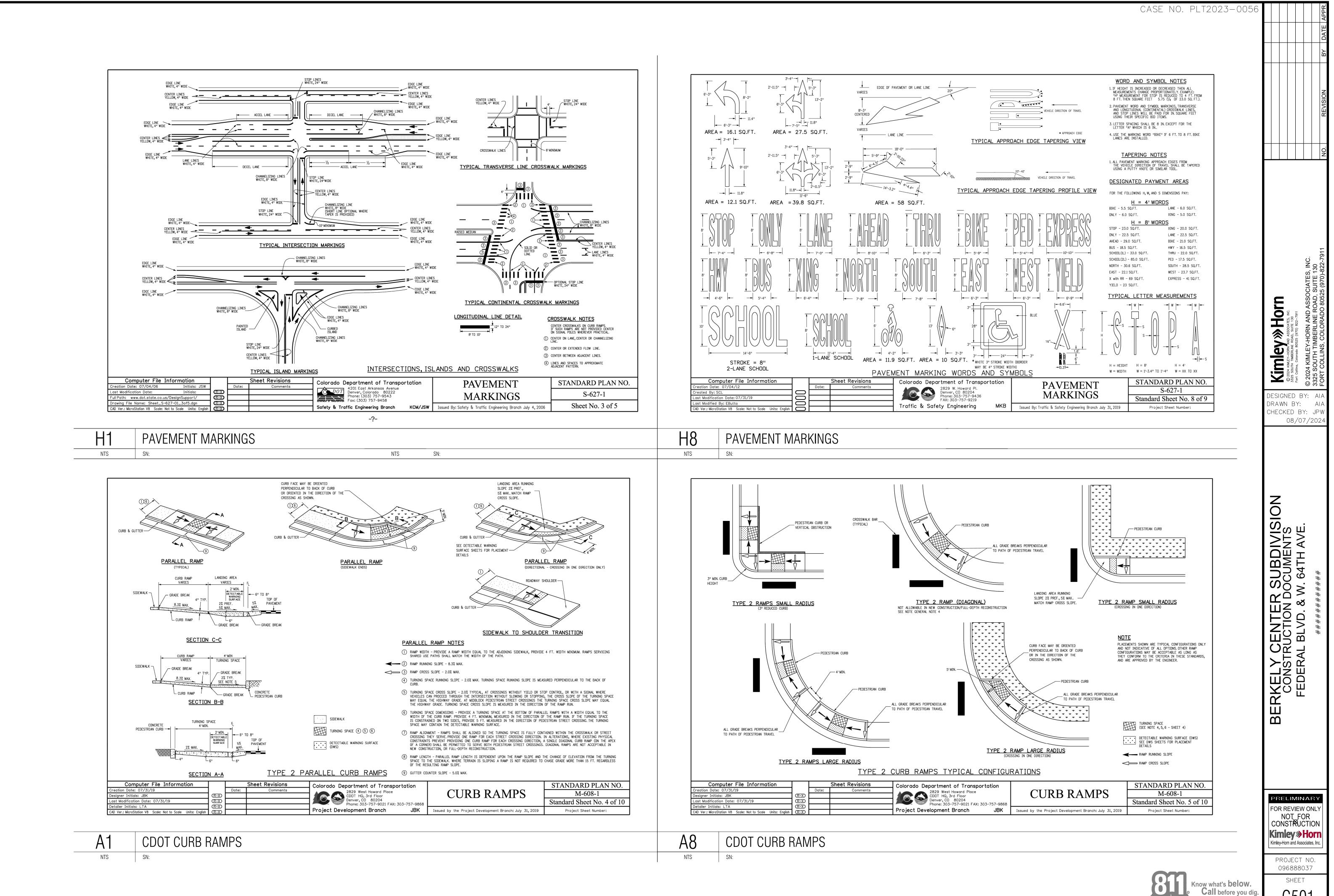




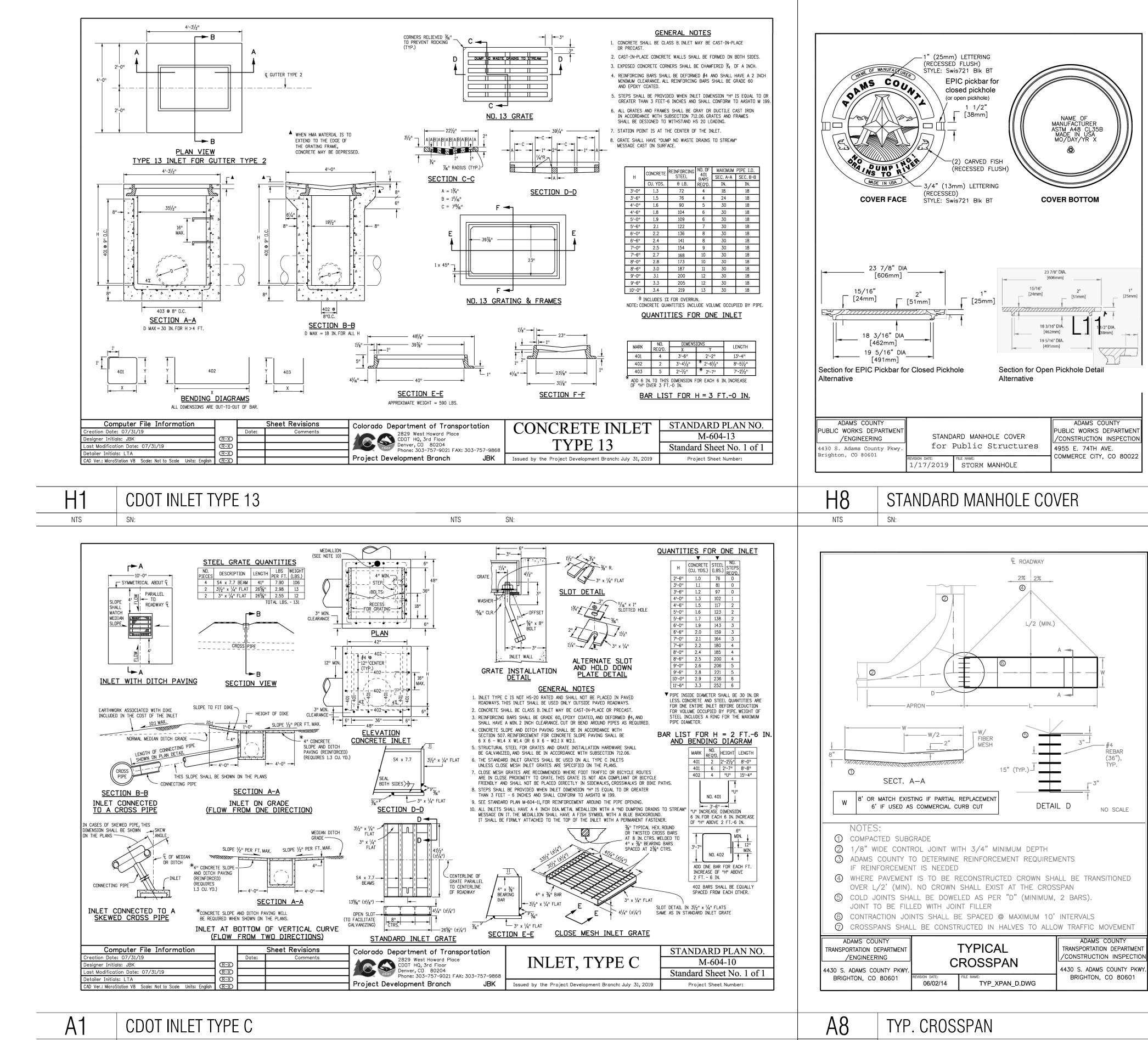


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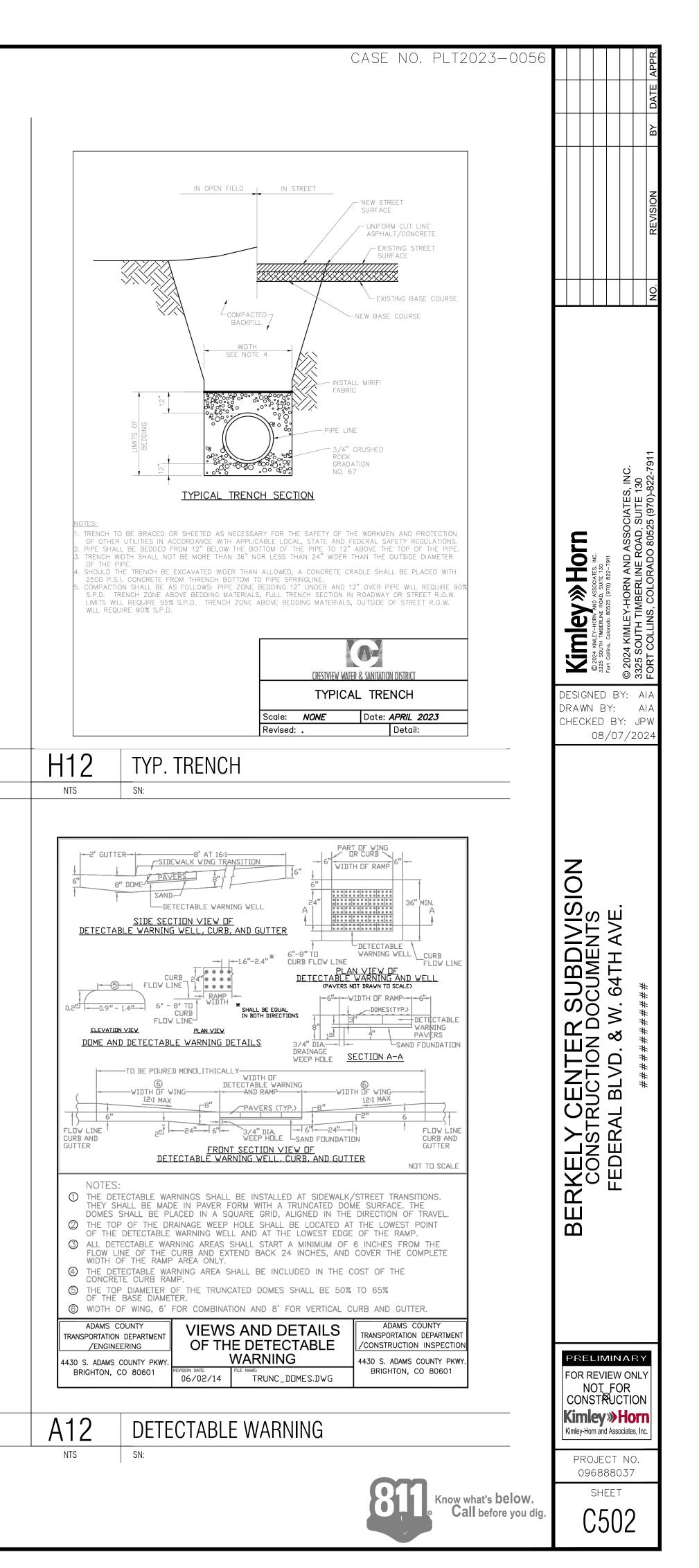
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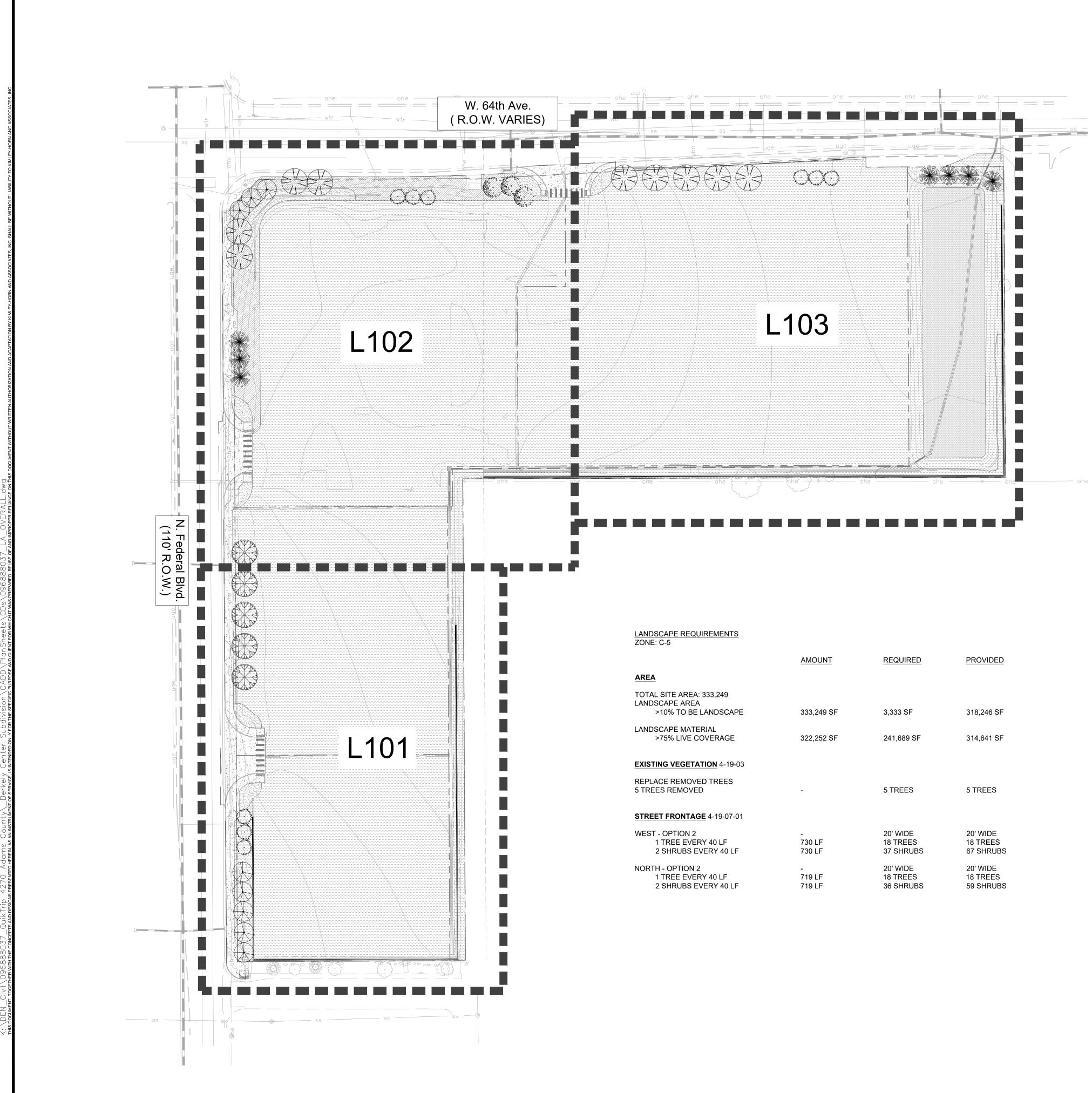


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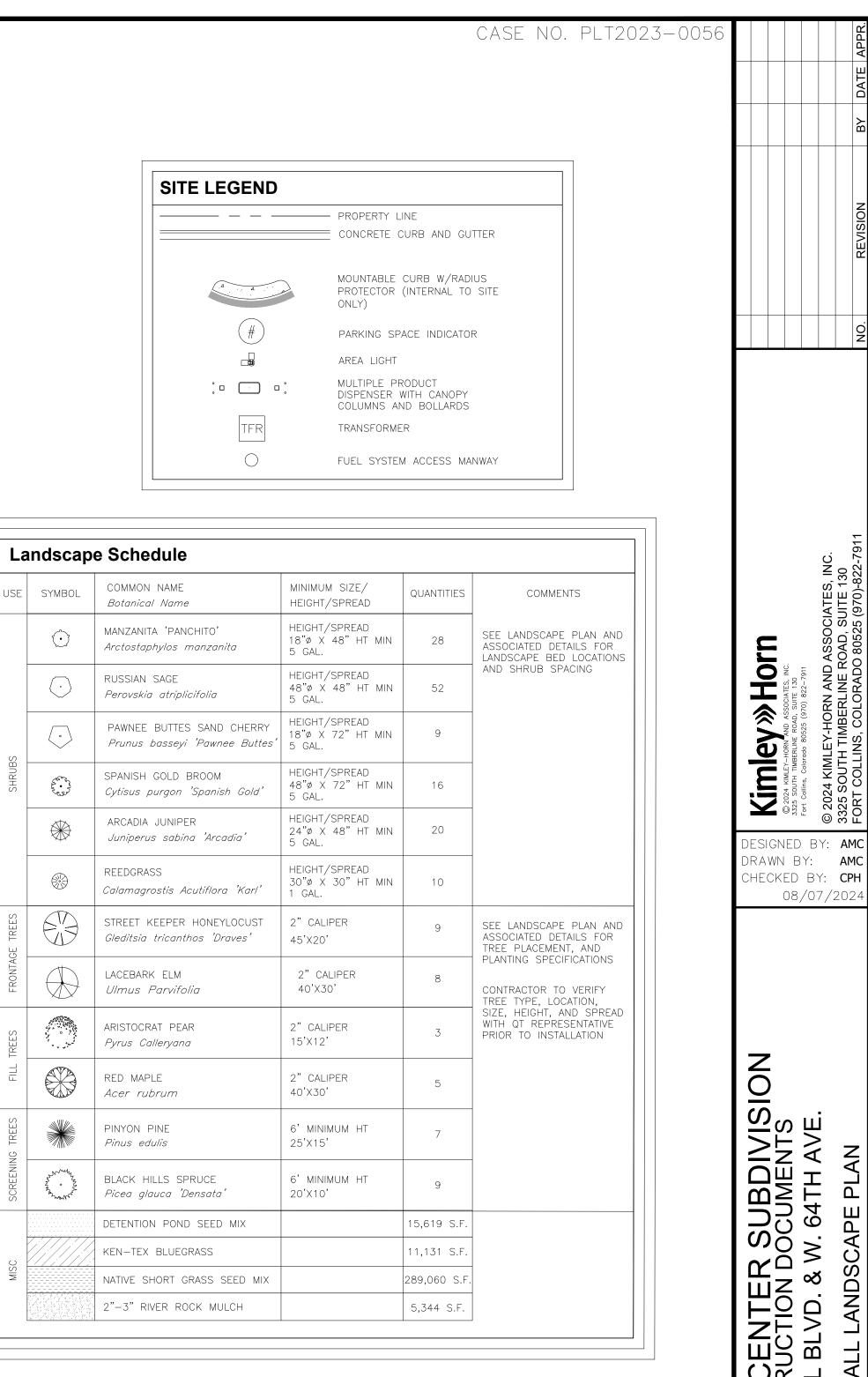




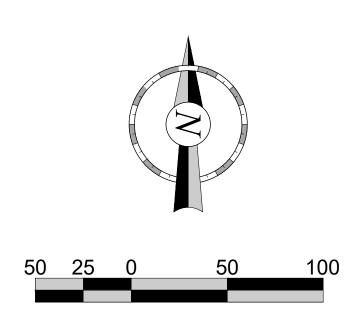
| LANDSCAPE REQUIREMENTS |
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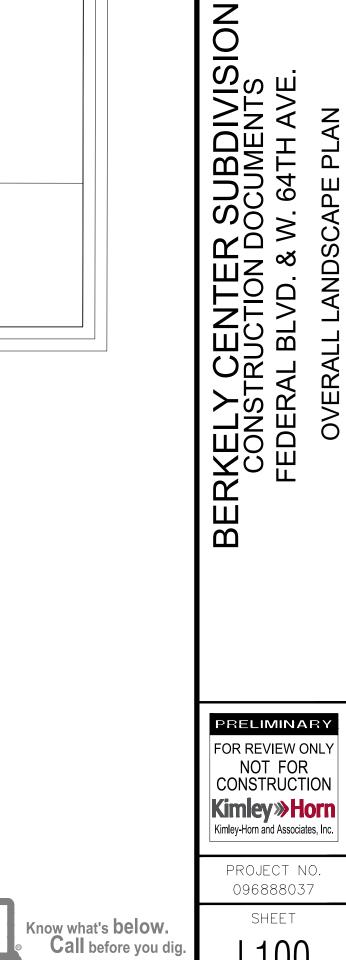
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| | | AMOUNT | REQUIRED | PROVIDED |
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| | OTAL SITE AREA: 333,249 ANDSCAPE AREA >10% TO BE LANDSCAPE | 333,249 SF | 3,333 SF | 318,246 SF |
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| E | XISTING VEGETATION 4-19-03 | | | |
| | EPLACE REMOVED TREES TREES REMOVED | - | 5 TREES | 5 TREES |
| S | TREET FRONTAGE 4-19-07-01 | | | |
| W | VEST - OPTION 2 1 TREE EVERY 40 LF 2 SHRUBS EVERY 40 LF | - 730 LF 730 LF | 20' WIDE 18 TREES 37 SHRUBS | 20' WIDE 18 TREES 67 SHRUBS |
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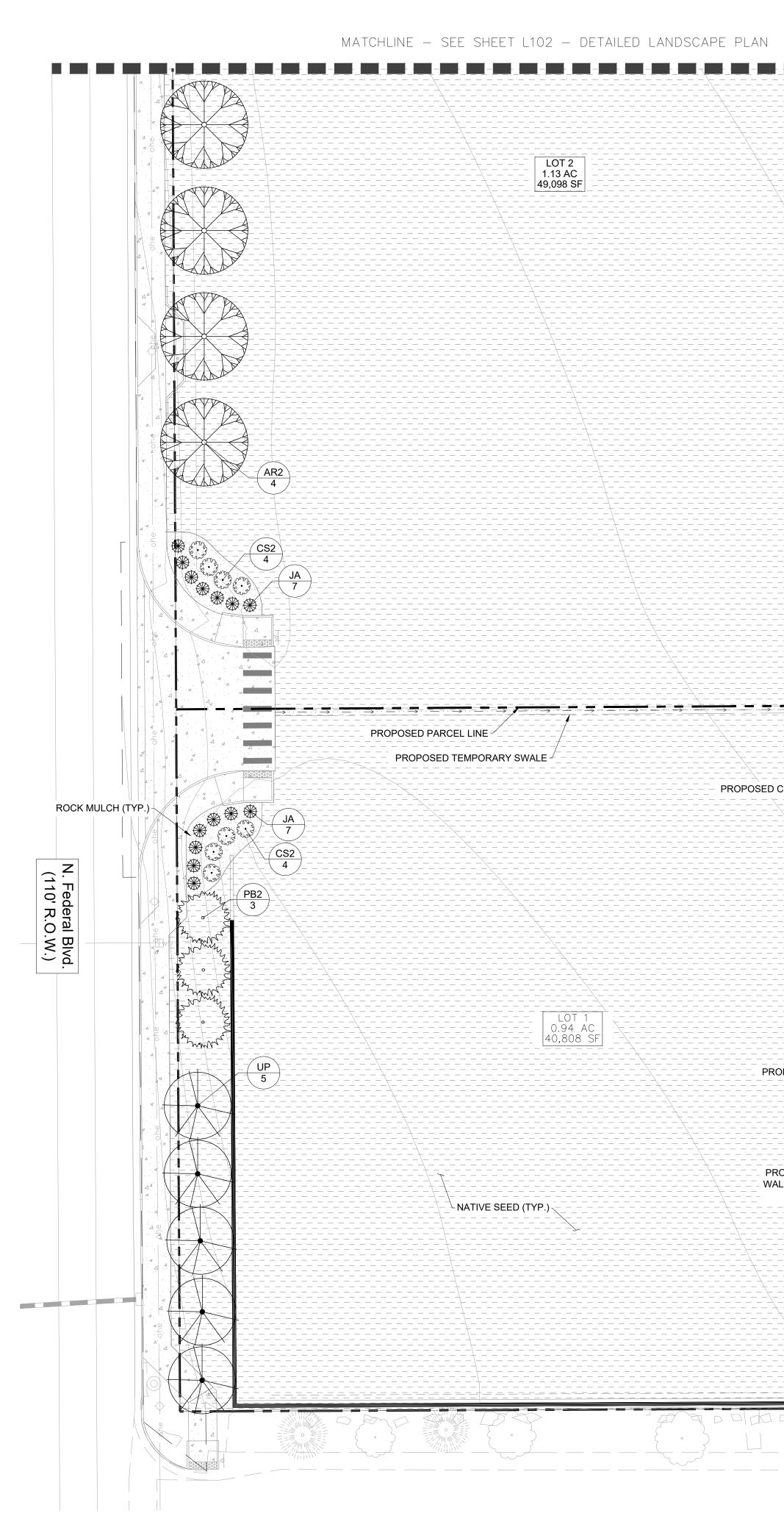


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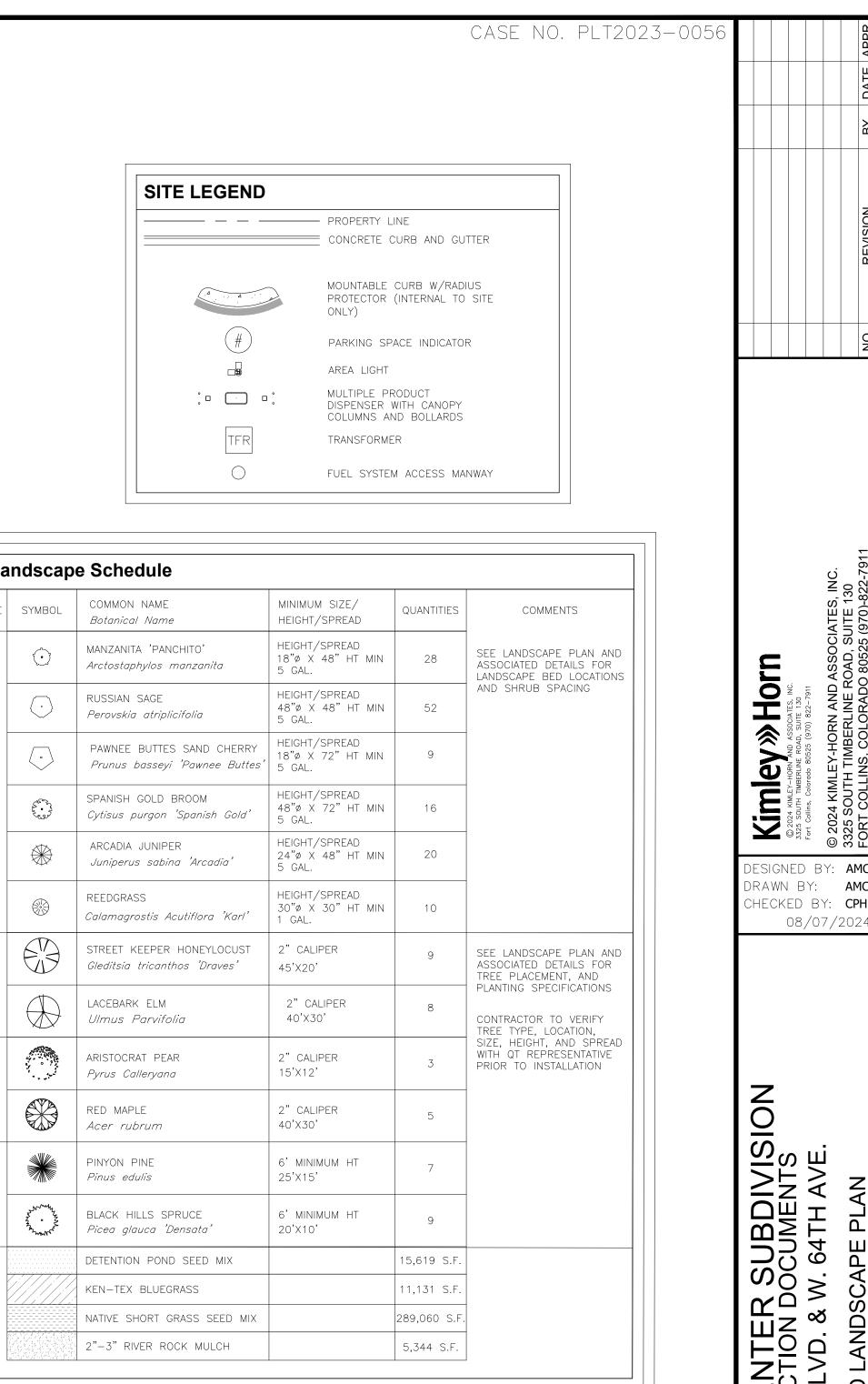


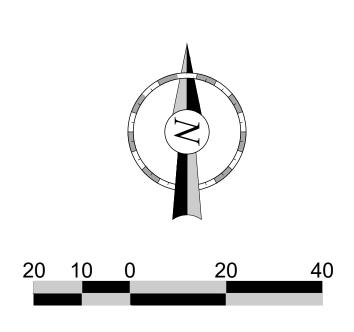
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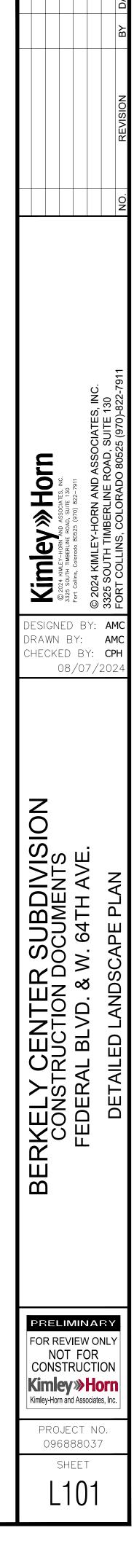


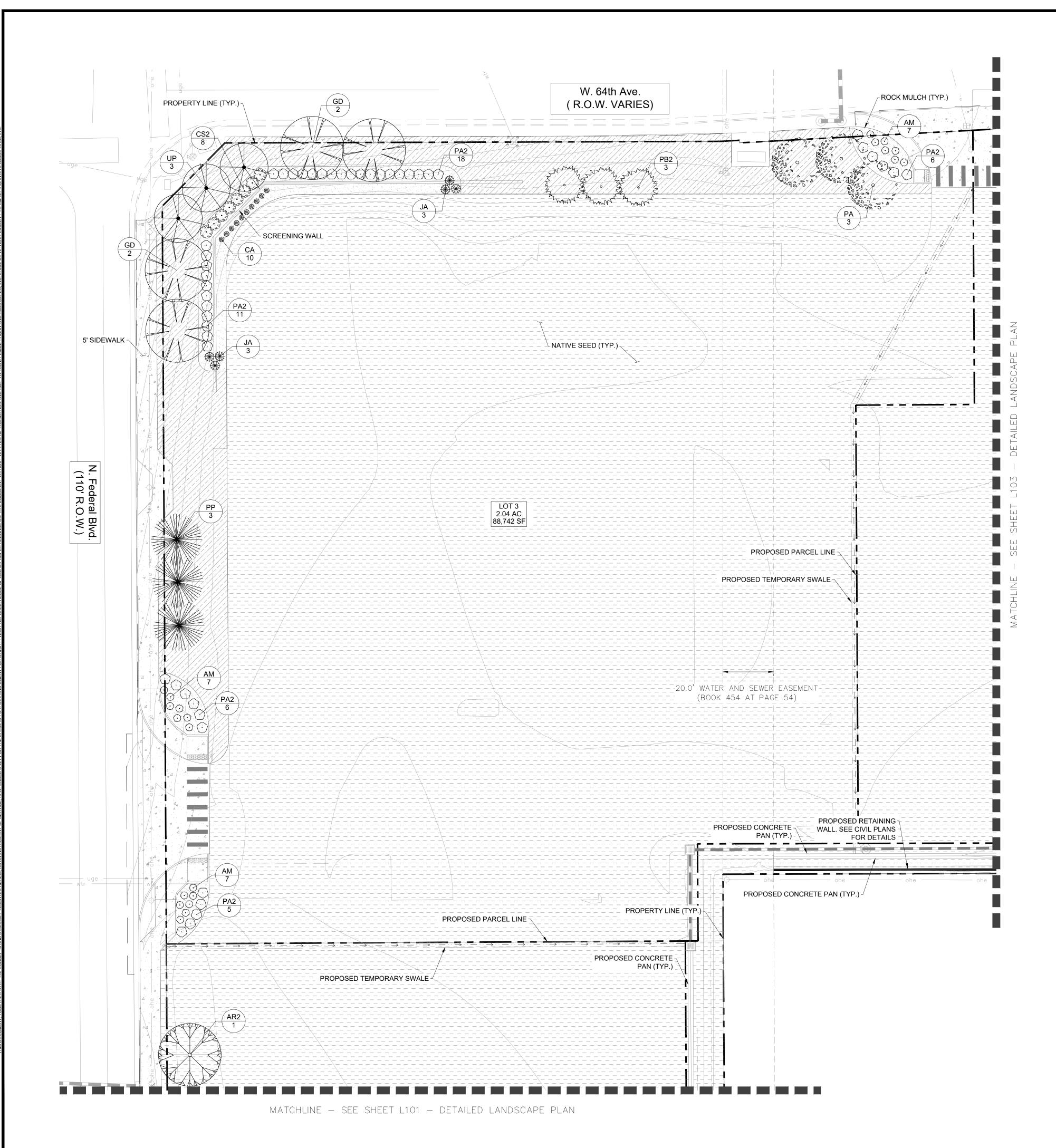
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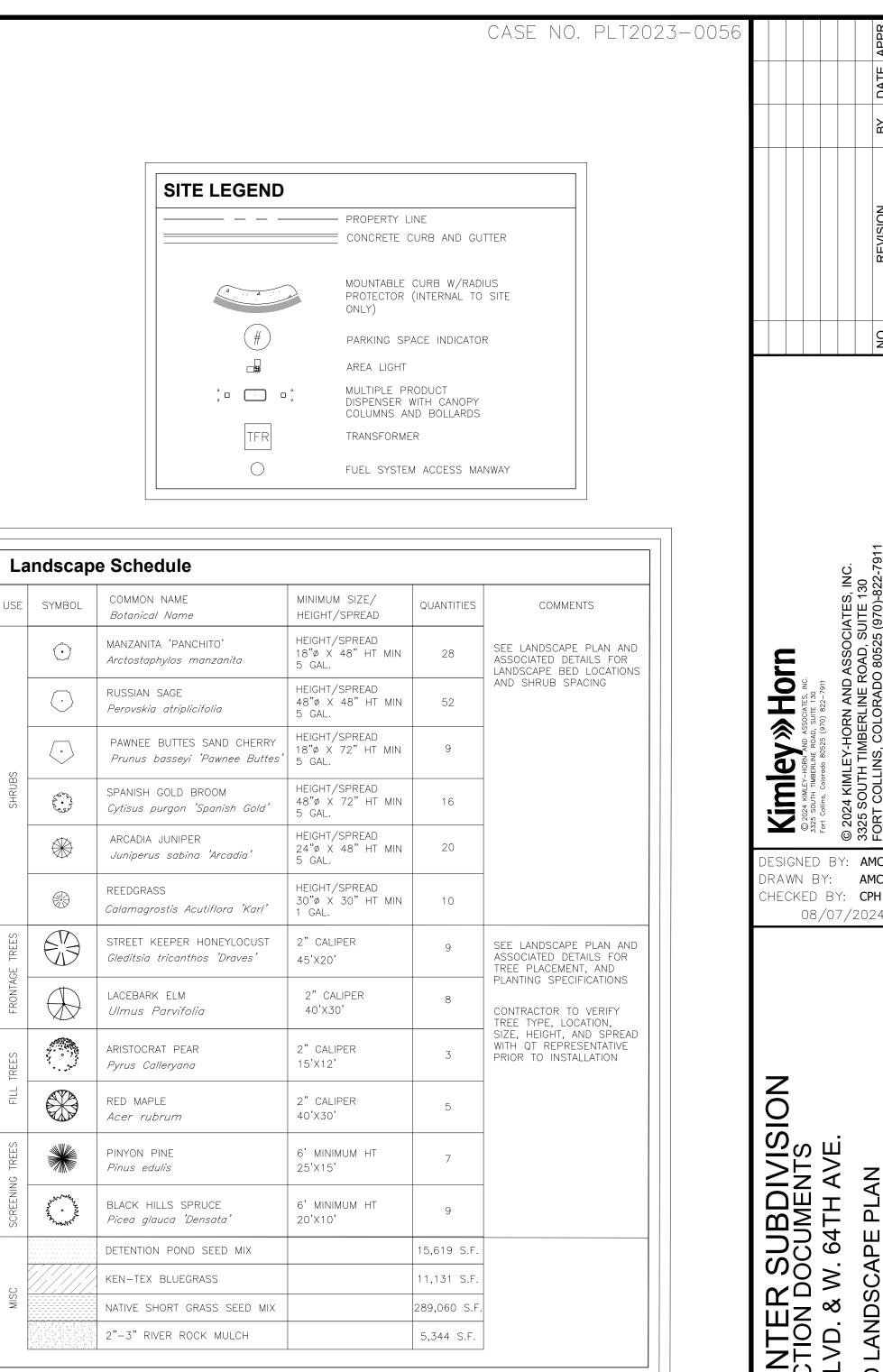


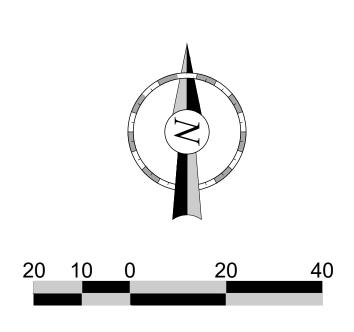


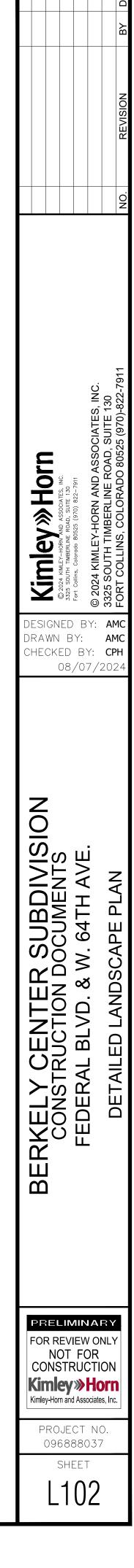


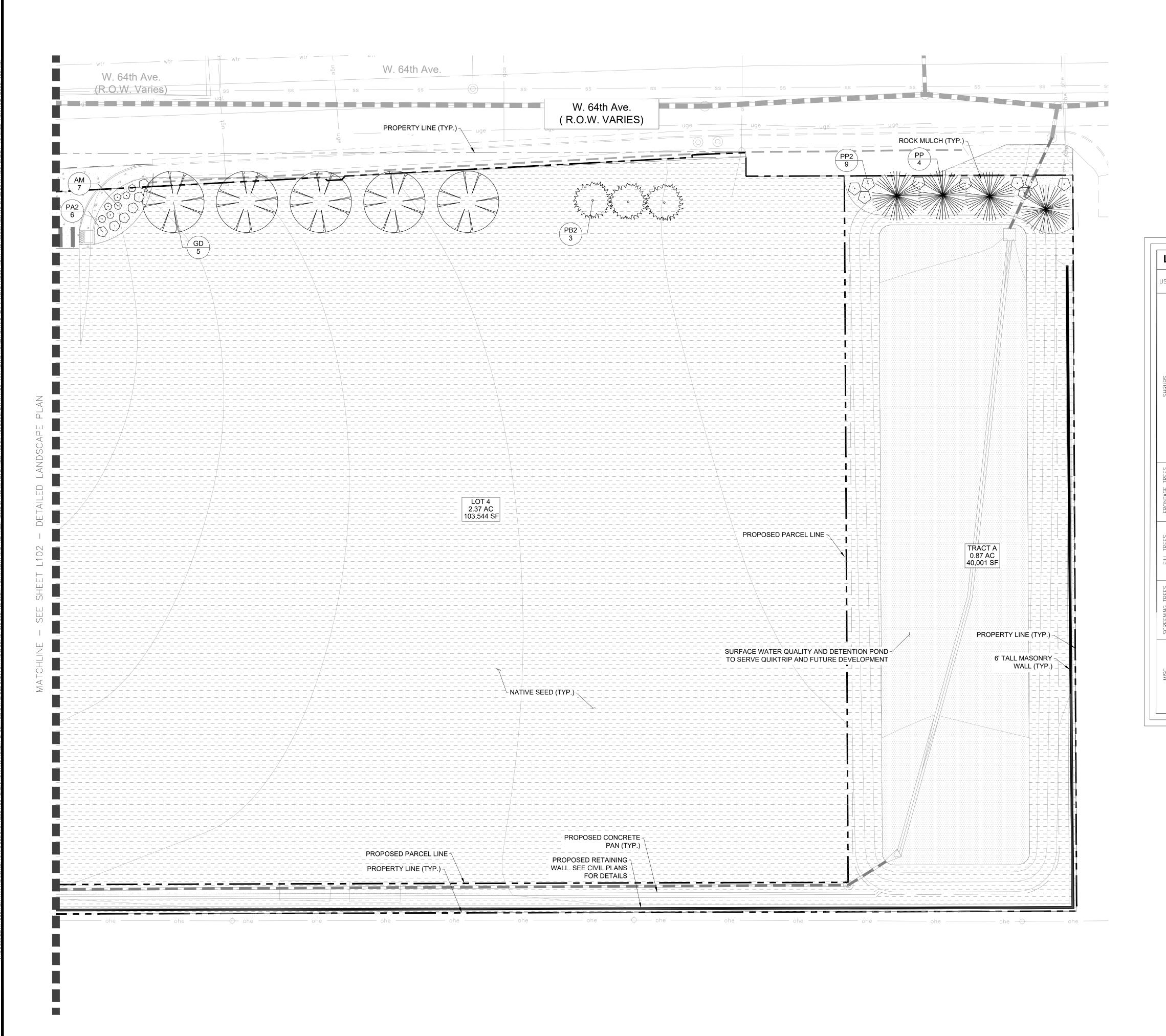


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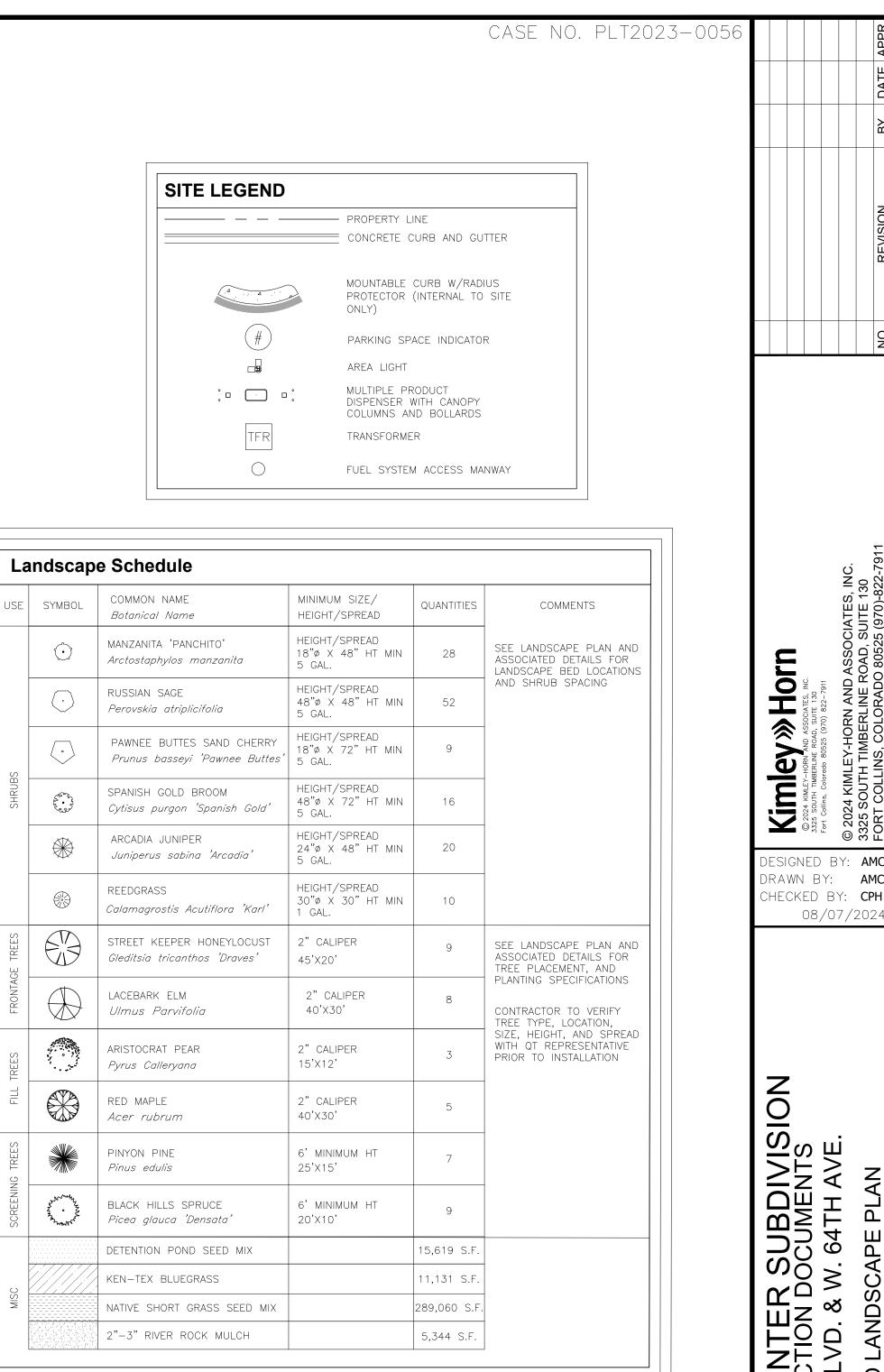


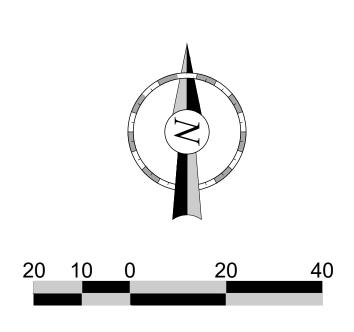


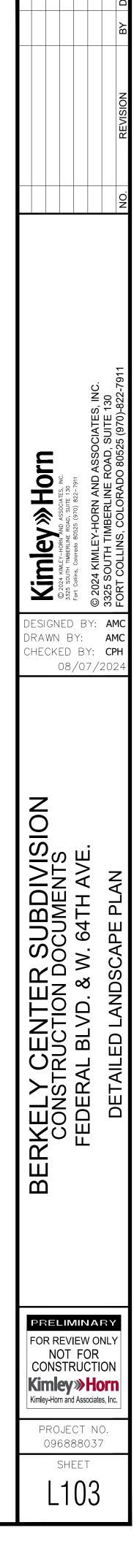












GENERAL LANDSCAPE SPECIFICATIONS

A. SCOPE OF WORK

- THE WORK CONSISTS OF: FURNISHING ALL LABOR, MATERIALS, EQUIPMENT, TOOLS, TRANSPORTATION, AND ANY OTHER APPURTENANCES NECESSARY FOR THE COMPLETION OF THIS PROJECT AS SHOWN ON THE DRAWINGS AND AS SPECIFIED HEREIN
- WORK SHALL INCLUDE MAINTENANCE AND WATERING OF ALL CONTRACT PLANTING AREAS UNTIL CERTIFICATION OF ACCEPTANCE BY THE OWNER.
- PROTECTION OF EXISTING STRUCTURES
- ALL EXISTING BUILDINGS, WALKS, WALLS, PAVING, PIPING, OTHER SITE CONSTRUCTION ITEMS, AND PLANTING ALREADY COMPLETED OR ESTABLISHED AND DESIGNATED TO REMAIN SHALL BE PROTECTED FROM DAMAGE BY THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. ALL DAMAGE RESULTING FROM NEGLIGENCE SHALL BE REPAIRED OR REPLACED TO THE SATISFACTION OF THE OWNER, AT NO COST TO THE OWNER.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING ALL NECESSARY BEST MANAGEMENT PRACTICES (BMP) DEVICES ACCORDING TO ALL REGULATORY AGENCY'S STANDARDS THROUGH THE DURATION OF ALL CONSTRUCTION ACTIVITIES.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY MAINTENANCE OF TRAFFIC (MOT) THAT MAY BE REQUIRED FOR THE PROJECT.
- 4. THE CONTRACTOR SHALL BE RESPONSIBLE FOR LOCATING ALL UTILITIES, WHETHER PUBLIC OR PRIVATE, PRIOR TO EXCAVATION. THE OWNER AND DESIGN PROFESSIONAL SHALL NOT BE RESPONSIBLE FOR THE ACCURACY AND COMPLETENESS OF ANY SUCH INFORMATION OR DATA. THE CONTRACTOR SHALL HAVE FULL RESPONSIBILITY FOR; REVIEWING AND CHECKING ALL SUCH INFORMATION AND DATA; LOCATING ALL UNDERGROUND FACILITIES DURING CONSTRUCTION; THE SAFETY AND PROTECTION THEREOF; REPAIRING ANY DAMAGE THERETO RESULTING FROM THE WORK. THE COST OF ALL WILL BE CONSIDERED AS HAVING BEEN INCLUDED IN THE CONTRACT PRICE. THE CONTRACTOR

C. PROTECTION OF EXISTING PLANT MATERIALS

CONSTRUCTION.

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL UNAUTHORIZED CUTTING OR DAMAGE TO TREES AND SHRUBS EXISTING OR OTHERWISE, CAUSED BY CARELESS EQUIPMENT OPERATION, MATERIAL STOCKPILING, ETC... THIS SHALL INCLUDE COMPACTION BY DRIVING OR PARKING INSIDE THE DRIP-LINE AND SPILLING OIL GASOLINE OR OTHER DELETERIOUS MATERIALS WITHIN THE DRIP-LINE. NO MATERIALS SHALL BE BURNED ON SITE. EXISTING TREES KILLED OR DAMAGED SO THAT THEY ARE MISSHAPEN AND/OR UNSIGHTLY SHALL BE REPLACED AT THE COST TO THE CONTRACTOR OF FOUR HUNDRED DOLLARS (\$400) PER CALIPER INCH ON AN ESCALATING SCALE WHICH ADDS AN ADDITIONAL TWENTY (20) PERCENT PER INCH OVER FOUR (4) INCHES CALIPER AS FIXED AND AGREED LIQUIDATED DAMAGES. CALIPER SHALL BE MEASURED SIX (6) INCHES ABOVE GROUND LEVEL FOR TREES UP TO AND INCLUDING FOUR (4) INCHES IN CALIPER AND TWELVE (12) INCHES ABOVE GROUND LEVEL FOR TREES OVER FOUR (4) INCHES IN CALIPER.

SHALL NOTIFY ANY AFFECTED UTILITY COMPANIES OR AGENCIES IN WRITING AT LEAST 48 HOURS PRIOR TO BEGINNING

SEE TREE MITIGATION PLAN AND NOTES, IF APPLICABLE

MATERIALS

MATER

GENERAL

MATERIAL SAMPLES LISTED BELOW SHALL BE SUBMITTED FOR APPROVAL, ON SITE OR AS DETERMINED BY THE OWNER. UPON APPROVAL, DELIVERY OF MATERIALS MAY COMMENCE.

| MATERIAL | SAMPLE SIZE |
|-------------|--|
| MULCH | ONE (1) CUBIC FOOT |
| TOPSOIL MIX | ONE (1) CUBIC FOOT |
| PLANTS | ONE (1) OF EACH VARIETY (OR TAGGED IN NURSERY) |

2. PLANT MATERIALS

- a. FURNISH NURSERY-GROWN PLANTS TRUE TO GENUS, SPECIES, VARIETY, CULTIVAR, STEM FORM, SHEARING, AND OTHER FEATURES INDICATED IN PLANT SCHEDULE SHOWN ON DRAWINGS AND COMPLYING WITH ANSI Z60.1 AND THE COLORADO NURSERY ACT; AND WITH HEALTHY ROOT SYSTEMS DEVELOPED BY TRANSPLANTING OR ROOT PRUNING. PROVIDE WELL-SHAPED. FULLY BRANCHED. HEALTHY. VIGOROUS STOCK, DENSELY FOLIATED WHEN IN LEAF AND FREE OF DISEASE, PESTS, EGGS, LARVAE, AND DEFECTS SUCH AS KNOTS, SUN SCALD, INJURIES, ABRASIONS, AND DISFIGUREMENT.
- b. TREES FOR PLANTING IN ROWS SHALL BE UNIFORM IN SIZE AND SHAPE.
- c. NO SUBSTITUTIONS SHALL BE MADE WITHOUT WRITTEN PERMISSION FROM THE PROJECT LANDSCAPE ARCHITECT. ANY ROW TREES MUST BE APPROVED BY OFFICE OF THE CITY FORESTER.
- d. PROVIDE PLANTS OF SIZES, GRADES, AND BALL OR CONTAINER SIZES COMPLYING WITH ANSI Z60.1 AND COLORADO NURSERY ACT FOR TYPES AND FORM OF PLANTS REQUIRED. PLANTS OF A LARGER SIZE MAY BE USED IF ACCEPTABLE TO PROJECT LANDSCAPE ARCHITECT WITH A PROPORTIONATE INCREASE IN SIZE OF ROOTS OR BALLS.
- e. PLANTS SHALL BE SUBJECT TO INSPECTION AND APPROVAL AT THE PLACE OF GROWTH, OR UPON DELIVERY TO THE SITE AS DETERMINED BY THE OWNER, FOR QUALITY, SIZE, AND VARIETY. SUCH APPROVAL SHALL NOT IMPAIR THE RIGHT OF INSPECTION AND REJECTION AT THE SITE DURING PROGRESS OF THE WORK OR AFTER COMPLETION FOR SIZE AND CONDITION OF ROOT BALLS OR ROOTS, LATENT DEFECTS OR INJURIES. REJECTED PLANTS SHALL BE REMOVED IMMEDIATELY FROM THE SITE. NOTICE REQUESTING INSPECTION SHALL BE SUBMITTED IN WRITING BY THE CONTRACTOR AT LEAST ONE (1) WEEK PRIOR TO ANTICIPATED DATE.
- f. TREES WITH DAMAGED, CROOKED, OR MULTIPLE LEADERS; TIGHT VERTICAL BRANCHES WHERE BARK IS SQUEEZED BETWEEN TWO BRANCHES OR BETWEEN BRANCH AND TRUNK ("INCLUDED BARK"); CROSSING TRUNKS; CUT-OFF LIMBS MORE THAN ³/₄ INCH (19 MM) IN DIAMETER; OR WITH STEM GIRDLING ROOTS WILL BE REJECTED.
- g. FURNISH TREES AND SHRUBS WITH ROOTS BALLS MEASURED FROM TOP OF ROOT BALL, WHICH SHALL BEGIN AT ROOT FLARE ACCORDING TO ANSI Z60.1 AND COLORADO NURSERY ACT. ROOT FLARE SHALL BE VISIBLE BEFORE PLANTING.
- h. LABEL AT LEAST ONE PLANT OF EACH VARIETY, SIZE, AND CALIPER WITH A SECURELY ATTACHED, WATERPROOF TAG BEARING LEGIBLE DESIGNATION OF COMMON NAME AND FULL SCIENTIFIC NAME, INCLUDING GENUS AND SPECIES. INCLUDE 11. EXCAVATION OF TREE OPENINGS SHALL BE PERFORMED USING EXTREME CARE TO AVOID DAMAGE TO SURFACE AND NOMENCLATURE FOR HYBRID, VARIETY, OR CULTIVAR, IF APPLICABLE FOR THE PLANT AS SHOWN ON DRAWINGS.
- i. IF FORMAL ARRANGEMENTS OR CONSECUTIVE ORDER OF PLANTS IS SHOWN ON DRAWINGS, SELECT STOCK FOR UNIFORM HEIGHT AND SPREAD, AND NUMBER THE LABELS TO ASSURE SYMMETRY IN PLANTING.

E. SOIL MIXTURE

- CONTRACTOR SHALL TEST EXISTING SOIL AND AMEND AS NECESSARY IN ACCORDANCE WITH THE GUIDELINES BELOW:
- SOIL MIXTURE SHALL CONSIST OF TWO PARTS OF TOPSOIL AND ONE PART SAND, AS DESCRIBED BELOW. CONTRACTOR TO SUBMIT SAMPLES AND PH TESTING RESULTS OF SOIL MIXTURE FOR OWNER'S REPRESENTATIVE APPROVAL PRIOR TO PLANT INSTALLATION OPERATIONS COMMENCE.
- a. TOPSOIL FOR USE IN PREPARING SOIL MIXTURE FOR BACKFILLING PLANT OPENINGS SHALL BE FERTILE, FRIABLE, AND OF A LOAMY CHARACTER; REASONABLY FREE OF SUBSOIL, CLAY LUMPS, BRUSH WEEDS AND OTHER LITTER; FREE OF ROOTS, STUMPS, STONES LARGER THAN 2" IN ANY DIRECTION, AND OTHER EXTRANEOUS OR TOXIC MATTER HARMFUL TO PLANT GROWTH. IT SHALL CONTAIN THREE (3) TO FIVE (5) PERCENT DECOMPOSED ORGANIC MATTER, HAVE A PH BETWEEN 5.5 AND 8.0, AND SOLUBLE SALTS LESS THAN 3.0 MMHOS/CM. SUBMIT SOIL SAMPLE AND PH TESTING RESULTS FOR APPROVAL.
- b. SAND SHALL BE COARSE, CLEAN, WELL-DRAINING, NATIVE SAND.
- TREES SHALL BE PLANTED IN THE EXISTING NATIVE SOIL ON SITE, UNLESS DETERMINED TO BE UNSUITABLE AT WHICH POINT THE CONTRACTOR SHALL CONTACT THE PROJECT LANDSCAPE ARCHITECT TO DISCUSS ALTERNATE RECOMMENDATION PRIOR TO PLANTING.

WATER

- WATER NECESSARY FOR PLANTING AND MAINTENANCE SHALL BE OF SATISFACTORY QUALITY TO SUSTAIN ADEQUATE PLANT GROWTH AND SHALL NOT CONTAIN HARMFUL, NATURAL OR MAN-MADE ELEMENTS DETRIMENTAL TO PLANTS. WATER MEETING THE ABOVE STANDARD SHALL BE OBTAINED ON THE SITE FROM THE OWNER, IF AVAILABLE, AND THE CONTRACTOR SHALL BE RESPONSIBLE TO MAKE ARRANGEMENTS FOR ITS USE BY HIS TANKS. HOSES. SPRINKLERS. ETC... IF SUCH WATER IS NOT AVAILABLE AT THE SITE, THE CONTRACTOR SHALL PROVIDE SATISFACTORY WATER FROM SOURCES OFF THE SITE AT NO ADDITIONAL COST TO THE OWNER.
- * WATERING/IRRIGATION RESTRICTIONS MAY APPLY REFER TO PROPERTY'S JURISDICTIONAL AUTHORITY.

FERTILIZER

- CONTRACTOR SHALL PROVIDE FERTILIZER APPLICATION SCHEDULE TO OWNER, AS APPLICABLE TO SOIL TYPE, PLANT INSTALLATION TYPE, AND SITE'S PROPOSED USE. SUGGESTED FERTILIZER TYPES SHALL BE ORGANIC OR OTHERWISE NATURALLY-DERIVED.
- * FERTILIZER RESTRICTIONS MAY APPLY REFER TO PROPERTY'S JURISDICTIONAL AUTHORITY.

H. MULCH

- MULCH MATERIAL SHALL BE MOISTENED AT THE TIME OF APPLICATION TO PREVENT WIND DISPLACEMENT, AND APPLIED AT A DEPTH OF THREE (3) INCHES. CLEAR MULCH FROM EACH PLANT'S CROWN (BASE) OR AS SHOWN IN PLANTING DETAILS. UNLESS OTHERWISE NOTED ON PLANS. MULCH SHALL BE DOUBLE SHREDDED HARDWOOD MULCH DARK BROWN FINES BY MOUNTAIN HIGH SAVATREE OR APPROVED EQUAL. DYED MULCH IS NOT ACCEPTABLE. SUBMIT SAMPLES TO PROJECT LANDSCAPE ARCHITECT FOR APPROVAL. MULCH SHALL BE PROVIDED OVER THE ENTIRE AREA OF EACH SHRUB BED, GROUND COVER, VINE BED, AND TREE RING (6' MINIMUM) PLANTED UNDER THIS CONTRACT, AS WELL AS FOR ANY EXISTING LANDSCAPE AREAS AS SHOWN ON PLANS.
- DIGGING AND HANDLING
- ALL TREES SPECIFIED SHALL BE BALLED AND BURLAPPED (B&B) UNLESS OTHERWISE APPROVED BY PROJECT LANDSCAPE ARCHITECT

- TRANSPIRATIONAL WATER LOSS.
- B&B, AND FIELD GROWN (FG) PLANTS SHALL BE DUG WITH FIRM, NATURAL BALLS OF SOIL OF SUFFICIENT SIZE TO PLANTED IF THE BALL IS CRACKED OR BROKEN. PLANTS SHALL NOT BE HANDLED BY STEMS.
- CONTAINER GROWN STOCK
- HEALTHY GROWING CONDITION.
- NOT BE HANDLED BY THEIR STEMS.
- 3. ROOT BOUND PLANTS ARE NOT ACCEPTABLE AND WILL BE REJECTED. MATERIALS LIST

FINE GRADING

- HAVE BEEN DISTURBED DURING CONSTRUCTION. THE CONTRACTOR SHALL FINE GRADE THE LAWN AND PLANTING AREAS TO BRING THE ROUGH GRADE UP TO FINAL
- PLANS FOR FINAL GRADES, IF APPLICABLE.

M. PLANTING PROCEDURES

- CORRECTIVE MEASURES THE RESPONSIBILITY OF THE CONTRACTOR.
- CONSTRUCTION.
- PLANTING DETAIL.
- PLANT MATERIALS BEFORE PLANTS ARE DUG AT NURSERY OR GROWING SITE.
- WORK. UPON ARRIVAL AT THE SITE, PLANTS SHALL BE THOROUGHLY WATERED AND PROPERLY MAINTAINED UNTIL HORTICULTURAL PRACTICES AS USED IN THE TRADE SHALL BE EXERCISED.
- WORK SHALL BE COORDINATED WITH OTHER TRADES TO PREVENT CONFLICTS. COORDINATE PLANTING WITH IRRIGATION
- STANDARD FOR NURSERY STOCK.
- DRAINAGE CONDITION" PLANTING DETAIL
- AND UNDER THE SUPERVISION OF A QUALIFIED LANDSCAPE FOREMEN.
- ROTO-TILLED TO A DEPTH EQUAL TO THE DEPTH OF THE ROOT BALL.
- 12. BALL DEPTH PLUS 6"

- 15. SOIL MIXTURE SHALL BE AS SPECIFIED IN SECTION 'E'.

- 19. ALL BURLAP, ROPE, WIRES, BASKETS, ETC.., SHALL BE REMOVED FROM THE SIDES AND TOPS OF BALLS, BUT NO BURLAP SHALL BE PULLED FROM UNDERNEATH.
- CUT. ALL PRUNING TO BE PERFORMED BY CERTIFIED ARBORIST.
- PLANTS AFTER INSTALLATION.
- TREE GUYING AND BRACING SHALL BE INSTALLED BY THE CONTRACTOR IN ACCORDANCE WITH THE PLANS TO INSURE UNDER THIS CONTRACT FALL AND DAMAGE PERSON OR PROPERTY.
- ALLOWED BY JURISDICTIONAL AUTHORITY)

LAWN SODDING

OWNER.

PROTECT ROOTS OR ROOT BALLS OF PLANTS AT ALL TIMES FROM SUN, DRYING WINDS, WATER AND FREEZING, AS NECESSARY UNTIL PLANTING. PLANT MATERIALS SHALL BE ADEQUATELY PACKED TO PREVENT DAMAGE DURING TRANSIT TREES TRANSPORTED MORE THAN TEN (10) MILES OR WHICH ARE NOT PLANTED WITHIN THREE (3) DAYS OF DELIVERY TO THE SITE SHALL BE SPRAYED WITH AN ANTITRANSPIRANT PRODUCT ("WILTPRUF" OR EQUAL) TO MINIMIZE

ENCOMPASS THE FIBROUS AND FEEDING ROOTS OF THE PLANTS. NO PLANTS MOVED WITH A ROOT BALL SHALL BE

ALL CONTAINER GROWN MATERIAL SHALL BE HEALTHY, VIGOROUS, WELL-ROOTED PLANTS ESTABLISHED IN THE CONTAINER IN WHICH THEY ARE SOLD. THE PLANTS SHALL HAVE TOPS WHICH ARE OF GOOD QUALITY AND ARE IN A

AN ESTABLISHED CONTAINER GROWN PLANT SHALL BE TRANSPLANTED INTO A CONTAINER AND GROWN IN THAT CONTAINER SUFFICIENTLY LONG ENOUGH FOR THE NEW FIBROUS ROOTS TO HAVE DEVELOPED SO THAT THE ROOT MASS WILL RETAIN ITS SHAPE AND HOLD TOGETHER WHEN REMOVED FROM THE CONTAINER. CONTAINER GROWN STOCK SHALL

QUANTITIES NECESSARY TO COMPLETE THE WORK ON THE DRAWINGS SHALL BE FURNISHED BY THE CONTRACTOR QUANTITY ESTIMATES HAVE BEEN MADE CAREFULLY, BUT THE LANDSCAPE ARCHITECT OR OWNER ASSUMES NO LIABILITY FOR OMISSIONS OR ERRORS. SHOULD A DISCREPANCY OCCUR BETWEEN THE PLANS AND THE PLANT LIST QUANTITY, THE PLANS SHALL GOVERN. ALL DIMENSIONS AND/OR SIZES SPECIFIED SHALL BE THE MINIMUM ACCEPTABLE SIZE.

FINE GRADING UNDER THIS CONTRACT SHALL CONSIST OF FINAL FINISHED GRADING OF LAWN AND PLANTING AREAS THAT

FINISHED GRADE ALLOWING FOR THICKNESS OF SOD AND/OR MULCH DEPTH.

ALL PLANTING AREAS SHALL BE GRADED AND MAINTAINED FOR POSITIVE DRAINAGE TO SURFACE/SUBSURFACE STORM DRAIN SYSTEMS. AREAS ADJACENT TO BUILDINGS SHALL SLOPE AWAY FROM THE BUILDINGS. REFER TO CIVIL ENGINEER'S O

THE CONTRACTOR SHALL CLEAN WORK AND SURROUNDING AREAS OF ALL RUBBISH OR OBJECTIONABLE MATTER DAILY. ALL MORTAR, CEMENT, BUILDING MATERIALS, AND TOXIC MATERIAL SHALL BE COMPLETELY REMOVED FROM PLANTING AREAS. THESE MATERIALS SHALL NOT BE MIXED WITH THE SOIL. SHOULD THE CONTRACTOR FIND SUCH SOIL CONDITIONS IN PLANTING AREAS WHICH WILL ADVERSELY AFFECT THE PLANT GROWTH, THE CONTRACTOR SHALL IMMEDIATELY CALL IT TO THE ATTENTION OF THE OWNER'S REPRESENTATIVE. FAILURE TO DO SO BEFORE PLANTING SHALL MAKE THE

VERIFY LOCATIONS OF ALL UTILITIES, CONDUITS, SUPPLY LINES AND CABLES, INCLUDING BUT NOT LIMITED TO: ELECTRIC, GAS (LINES AND TANKS), WATER, SANITARY SEWER, STORMWATER SYSTEMS, CABLE, AND TELEPHONE. PROPERLY MAINTAIN AND PROTECT EXISTING UTILITIES. CALL COLORADO (811) TO LOCATE UTILITIES AT LEAST 48 HOURS PRIOR TO

CONTRACTOR IS RESPONSIBLE TO REMOVE ALL EXISTING AND IMPORTED LIMEROCK AND LIMEROCK SUB-BASE FROM ALL R. PLANTING AREAS TO A MINIMUM DEPTH OF 36" OR TO NATIVE SOIL. CONTRACTOR IS RESPONSIBLE TO BACKFILL THESE PLANTING AREAS TO ROUGH FINISHED GRADE WITH CLEAN TOPSOIL FROM AN ON-SITE SOURCE OR AN IMPORTED SOURCE. IF LIMEROCK OR OTHER ADVERSE CONDITIONS OCCUR IN PLANTED AREAS AFTER 36" DEEP EXCAVATION BY THE CONTRACTOR, AND POSITIVE DRAINAGE CAN NOT BE ACHIEVED, CONTRACTOR SHALL UTILIZE POOR DRAINAGE CONDITION

4. FURNISH NURSERY'S CERTIFICATE OF COMPLIANCE WITH ALL REQUIREMENTS AS SPECIFIED HEREIN. INSPECT AND SELECT S. COMPLY WITH APPLICABLE FEDERAL, STATE, COUNTY, AND LOCAL REGULATIONS GOVERNING LANDSCAPE MATERIALS AND

PLANTED. PLANTS STORED ONSITE SHALL NOT REMAIN UNPLANTED OR APPROPRIATELY HEALED IN FOR A PERIOD EXCEEDING TWENTY-FOUR (24) HOURS. AT ALL TIMES WORKMANLIKE METHODS CUSTOMARY IN ACCEPTED

WORK TO ASSURE AVAILABILITY OF WATER AND PROPER LOCATION OF IRRIGATION APPURTENANCES AND PLANTS. ALL PLANTING OPENINGS SHALL BE EXCAVATED TO SIZE AND DEPTH IN ACCORDANCE WITH ANSI Z60.1-2014 AMERICAN

TEST ALL TREE OPENINGS WITH WATER BEFORE PLANTING TO ASSURE PROPER DRAINAGE PERCOLATION IS AVAILABLE. NO ALLOWANCE WILL BE MADE FOR LOST PLANTS DUE TO IMPROPER DRAINAGE. IF POOR DRAINAGE EXISTS, UTILIZE "POOR

TREES SHALL BE SET PLUMB AND HELD IN POSITION UNTIL THE PLANTING MIXTURE HAS BEEN FLUSHED INTO PLACE WITH A SLOW, FULL HOSE STREAM. ALL PLANTING SHALL BE PERFORMED BY PERSONNEL FAMILIAR WITH PLANTING PROCEDURES

10. PRIOR TO EXCAVATION OF TREE OPENINGS, AN AREA EQUAL TO TWO TIMES THE DIAMETER OF THE ROOT BALL SHALL BE

SUBSURFACE ELEMENTS SUCH AS UTILITIES OR HARDSCAPE ELEMENTS, FOOTERS AND PREPARED SUB-BASES.

IN CONTINUOUS SHRUB AND GROUND COVER BEDS, THE ROTO-TILLED PERIMETER SHOULD EXTEND TO A DISTANCE OF ONE FOOT BEYOND THE DIAMETER OF A SINGLE ROOT BALL. THE BED SHALL BE TILLED TO A DEPTH EQUAL TO THE ROOT

13. TREE OPENINGS FOR WELL DRAINED SOILS SHALL BE DUG SO THAT THE BOTTOM OF THE ROOT BALL WILL REST ON UNDISTURBED SOIL AND THE TOP OF THE ROOT BALL WILL BE FLUSH WITH FINISH GRADE. IN POORLY DRAINED SOILS THE TREE OPENING SHALL BE DUG SO THAT THE ROOT BALL RESTS ON UNDISTURBED SOIL AND THE TOP OF THE ROOT BALL IS 1" ABOVE FINISH GRADE. PLANT PIT WALLS SHALL BE SCARIFIED PRIOR TO PLANT INSTALLATION.

14. TAKE ALL NECESSARY PRECAUTIONS TO AVOID DAMAGE TO BUILDINGS AND BUILDING STRUCTURES WHILE INSTALLING

TREES AND SHRUBS SHALL BE SET STRAIGHT AT AN ELEVATION THAT, AFTER SETTLEMENT, THE PLANT CROWN WILL STAND ONE (1) TO TWO (2) INCHES ABOVE GRADE. EACH PLANT SHALL BE SET IN THE CENTER OF THE PIT. SOIL MIXTURE SHALL BE BACK FILLED, THOROUGHLY TAMPED AROUND THE BALL, AND SETTLED BY WATER (AFTER TAMPING).

17. AMEND PINE AND OAK PLANT OPENINGS WITH ECTOMYCORRHIZAL SOIL APPLICATION PER MANUFACTURER'S RECOMMENDATION. ALL OTHER PLANT OPENINGS SHALL BE AMENDED WITH ENDOMYCORRHIZAL SOIL APPLICATION PER MANUFACTURER'S RECOMMENDATION. PROVIDE PRODUCT INFORMATION SUBMITTAL PRIOR TO INOCULATION.

18. FILL HOLE WITH SOIL MIXTURE, MAKING CERTAIN ALL SOIL IS SATURATED. TO DO THIS, FILL HOLE WITH WATER AND ALLOW TO SOAK MINIMUM TWENTY (20) MINUTES, STIRRING IF NECESSARY TO GET SOIL THOROUGHLY WET. PACK LIGHTLY WITH FEET, ADD MORE WET SOIL MIXTURE. DO NOT COVER TOP OF BALL WITH SOIL MIXTURE.

TREES SHALL BE PRUNED, IN ACCORDANCE WITH ANSI A-300, TO PRESERVE THE NATURAL CHARACTER OF THE PLANT. ALL SOFT WOOD OR SUCKER GROWTH AND ALL BROKEN OR BADLY DAMAGED BRANCHES SHALL BE REMOVED WITH A CLEAN

21. SHRUBS AND GROUND COVER PLANTS SHALL BE EVENLY SPACED IN ACCORDANCE WITH THE DRAWINGS AND AS INDICATED ON THE PLANT LIST. MATERIALS INSTALLED SHALL MEET MINIMUM SPECIMEN REQUIREMENTS OR QUANTITIES

SHOWN ON PLANS, WHICHEVER IS GREATER. CULTIVATE ALL PLANTING AREAS TO A MINIMUM DEPTH OF 6", REMOVE AND DISPOSE ALL DEBRIS. MIX TOP 4" THE PLANTING SOIL MIXTURE AS SPECIFIED IN SECTION E. THOROUGHLY WATER ALL

STABILITY AND MAINTAIN TREES IN AN UPRIGHT POSITION. IF THE CONTRACTOR AND OWNER DECIDE TO WAIVE THE TREE GUYING AND BRACING. THE OWNER SHALL NOTIFY THE PROJECT LANDSCAPE ARCHITECT IN WRITING AND AGREE TO INDEMNIFY AND HOLD HARMLESS THE PROJECT LANDSCAPE ARCHITECT IN THE EVENT UNSUPPORTED TREES PLANTED

23. ALL PLANT BEDS SHALL BE KEPT FREE OF NOXIOUS WEEDS UNTIL FINAL ACCEPTANCE OF WORK. IF DIRECTED BY THE OWNER, "ROUND-UP" SHALL BE APPLIED FOR WEED CONTROL BY QUALIFIED PERSONNEL TO ALL PLANTING AREAS IN SPOT APPLICATIONS PER MANUFACTURER'S RECOMMENDATIONS. PRIOR TO FINAL INSPECTION, TREAT ALL PLANTING BEDS WITH AN APPROVED PRE-EMERGENT HERBICIDE AT AN APPLICATION RATE RECOMMENDED BY THE MANUFACTURER. (AS

THE WORK CONSISTS OF LAWN BED PREPARATION, SOIL PREPARATION, AND SODDING COMPLETE, IN STRICT ACCORDANCE WITH THE SPECIFICATIONS AND THE APPLICABLE DRAWINGS TO PRODUCE A TURF GRASS LAWN ACCEPTABLE TO THE

- ALL AREAS THAT ARE TO BE SODDED SHALL BE CLEARED OF ANY ROUGH GRASS, WEEDS, AND DEBRIS BY MEANS OF A SOD CUTTER TO A DEPTH OF THREE (3) INCHES, AND THE GROUND BROUGHT TO AN EVEN GRADE. THE ENTIRE SURFACE SHALL BE ROLLED WITH A ROLLER WEIGHING NOT MORE THAN ONE-HUNDRED (100) POUNDS PER FOOT OF WIDTH. DURING THE ROLLING, ALL DEPRESSIONS CAUSED BY SETTLEMENT SHALL BE FILLED WITH ADDITIONAL SOIL, AND THE SURFACE SHALL BE REGRADED AND ROLLED UNTIL PRESENTING A SMOOTH AND EVEN FINISH TO THE REQUIRED GRADE.
- PREPARE LOOSE BED FOUR (4) INCHES DEEP. HAND RAKE UNTIL ALL BUMPS AND DEPRESSIONS ARE REMOVED. WET PREPARED AREA THOROUGHLY.
- 4. SODDING
- a. THE CONTRACTOR SHALL SOD ALL AREAS THAT ARE NOT PAVED OR PLANTED AS DESIGNATED ON THE DRAWINGS WITHIN THE CONTRACT LIMITS, UNLESS SPECIFICALLY NOTED OTHERWISE.
- b. SOD PANELS SHALL BE LAID TIGHTLY TOGETHER SO AS TO MAKE A SOLID SODDED LAWN AREA. SOD SHALL BE LAID UNIFORMLY AGAINST THE EDGES OF ALL CURBS AND OTHER HARDSCAPE ELEMENTS, PAVED AND PLANTED AREAS. ADJACENT TO BUILDINGS, A 24 INCH STONE MULCH STRIP SHALL BE PROVIDED. IMMEDIATELY FOLLOWING SOD LAYING, THE LAWN AREAS SHALL BE ROLLED WITH A LAWN ROLLER CUSTOMARILY USED FOR SUCH PURPOSES, AND THEN THOROUGHLY IRRIGATED. IF. IN THE OPINION OF THE OWNER. TOP-DRESSING IS NECESSARY AFTER ROLLING TO FILL THE VOIDS BETWEEN THE SOD PANELS AND TO EVEN OUT INCONSISTENCIES IN THE SOD, CLEAN SAND, AS APPROVED BY THE OWNER'S REPRESENTATIVE, SHALL BE UNIFORMLY SPREAD OVER THE ENTIRE SURFACE OF THE SOD AND THOROUGHLY WATERED IN. FERTILIZE INSTALLED SOD AS ALLOWED BY PROPERTY'S JURISDICTIONAL AUTHORITY.
- DURING DELIVERY, PRIOR TO, AND DURING THE PLANTING OF THE LAWN AREAS, THE SOD PANELS SHALL AT ALL TIMES BE PROTECTED FROM EXCESSIVE DRYING AND UNNECESSARY EXPOSURE OF THE ROOTS TO THE SUN. ALL SOD SHALL BE STACKED SO AS NOT TO BE DAMAGED BY SWEATING OR EXCESSIVE HEAT AND MOISTURE.
- LAWN MAINTENANCE
- a. WITHIN THE CONTRACT LIMITS, THE CONTRACTOR SHALL PRODUCE A DENSE, WELL ESTABLISHED LAWN. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPAIR AND RE-SODDING OF ALL ERODED. SUNKEN OR BARE SPOTS (LARGER THAN 12"X12") UNTIL CERTIFICATION OF ACCEPTANCE BY THE OWNER'S REPRESENTATIVE. REPAIRED SODDING SHALL BE ACCOMPLISHED AS IN THE ORIGINAL WORK, INCLUDING REGRADING IF NECESSARY
- b. CONTRACTOR SHALL BE RESPONSIBLE FOR ESTABLISHING AND MAINTAINING SOD/LAWN UNTIL ACCEPTANCE BY THE OWNER'S REPRESENTATIVE. PRIOR TO AND UPON ACCEPTANCE, CONTRACTOR TO PROVIDE WATERING/IRRIGATION SCHEDULE TO OWNER, OBSERVE ALL APPLICABLE WATERING RESTRICTIONS AS SET FORTH BY THE PROPERTY'S JURISDICTIONAL AUTHORITY.

FDGING

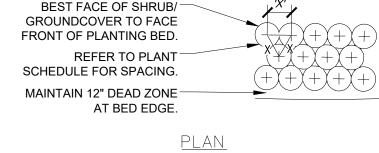
- a. CONTRACTOR SHALL INSTALL 4"X $_8^1$ " ROLLED TOP STEEL EDGING BETWEEN ALL SOD/SEED AREAS AND PLANTING BEDS. CLEANUF
- UPON COMPLETION OF ALL PLANTING WORK AND BEFORE FINAL ACCEPTANCE, THE CONTRACTOR SHALL REMOVE ALL MATERIAL. EQUIPMENT, AND DEBRIS RESULTING FROM CONTRACTORS WORK. ALL PAVED AREAS SHALL BE CLEANED AND THE SITE LEFT IN A NEAT AND ACCEPTABLE CONDITION AS APPROVED BY THE OWNER'S REPRESENTATIVE.

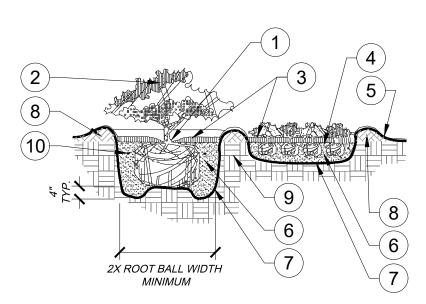
PLANT MATERIAL MAINTENANCE

ALL PLANTS AND PLANTING INCLUDED UNDER THIS CONTRACT SHALL BE MAINTAINED BY WATERING, CULTIVATING, SPRAYING, PRUNING, AND ALL OTHER OPERATIONS (SUCH AS RE-STAKING OR REPAIRING GUY SUPPORTS) NECESSARY TO INSURE A HEALTHY PLANT CONDITION BY THE CONTRACTOR UNTIL CERTIFICATION OF ACCEPTANCE BY THE OWNER'S REPRESENTATIVE.

FINAL INSPECTION AND ACCEPTANCE OF WORK

- FINAL INSPECTION AT THE END OF THE WARRANTY PERIOD SHALL BE ON PLANTING, CONSTRUCTION AND ALL OTHER INCIDENTAL WORK PERTAINING TO THIS CONTRACT. ANY REPLACEMENT AT THIS TIME SHALL BE SUBJECT TO THE SAME ONE (1) YEAR WARRANTY (OR AS SPECIFIED BY THE LANDSCAPE ARCHITECT OR OWNER IN WRITING) BEGINNING WITH THE TIME OF REPLACEMENT AND ENDING WITH THE SAME INSPECTION AND ACCEPTANCE HEREIN DESCRIBED. WARRANT
- THE LIFE AND SATISFACTORY CONDITION OF ALL PLANT MATERIAL INSTALLED (INCLUDING SOD) BY THE LANDSCAPE CONTRACTOR SHALL BE WARRANTED BY THE CONTRACTOR FOR A MINIMUM OF ONE (1) CALENDAR YEAR COMMENCING AT THE TIME OF CERTIFICATION OF ACCEPTANCE BY THE OWNER'S REPRESENTATIVE.
- ANY PLANT NOT FOUND IN A HEALTHY GROWING CONDITION AT THE END OF THE WARRANTY PERIOD SHALL BE REMOVED FROM THE SITE AND REPLACED AS SOON AS WEATHER CONDITIONS PERMIT. ALL REPLACEMENTS SHALL BE PLANTS OF THE SAME KIND AND SIZE AS SPECIFIED IN THE PLANT LIST. THEY SHALL BE FURNISHED PLANTED AND MULCHED AS SPECIFIED AT NO ADDITIONAL COST TO THE OWNER.
- IN THE EVENT THE OWNER DOES NOT CONTRACT WITH THE CONTRACTOR FOR LANDSCAPE AND IRRIGATION MAINTENANCE, THE CONTRACTOR SHOULD VISIT THE PROJECT SITE PERIODICALLY DURING THE ONE (1) YEAR WARRANTY PERIOD TO EVALUATE MAINTENANCE PROCEDURES BEING PERFORMED BY THE OWNER. CONTRACTOR SHALL NOTIFY THE OWNER IN WRITING OF MAINTENANCE PROCEDURES OR CONDITIONS WHICH THREATEN VIGOROUS AND HEALTHY PLANT GROWTH.





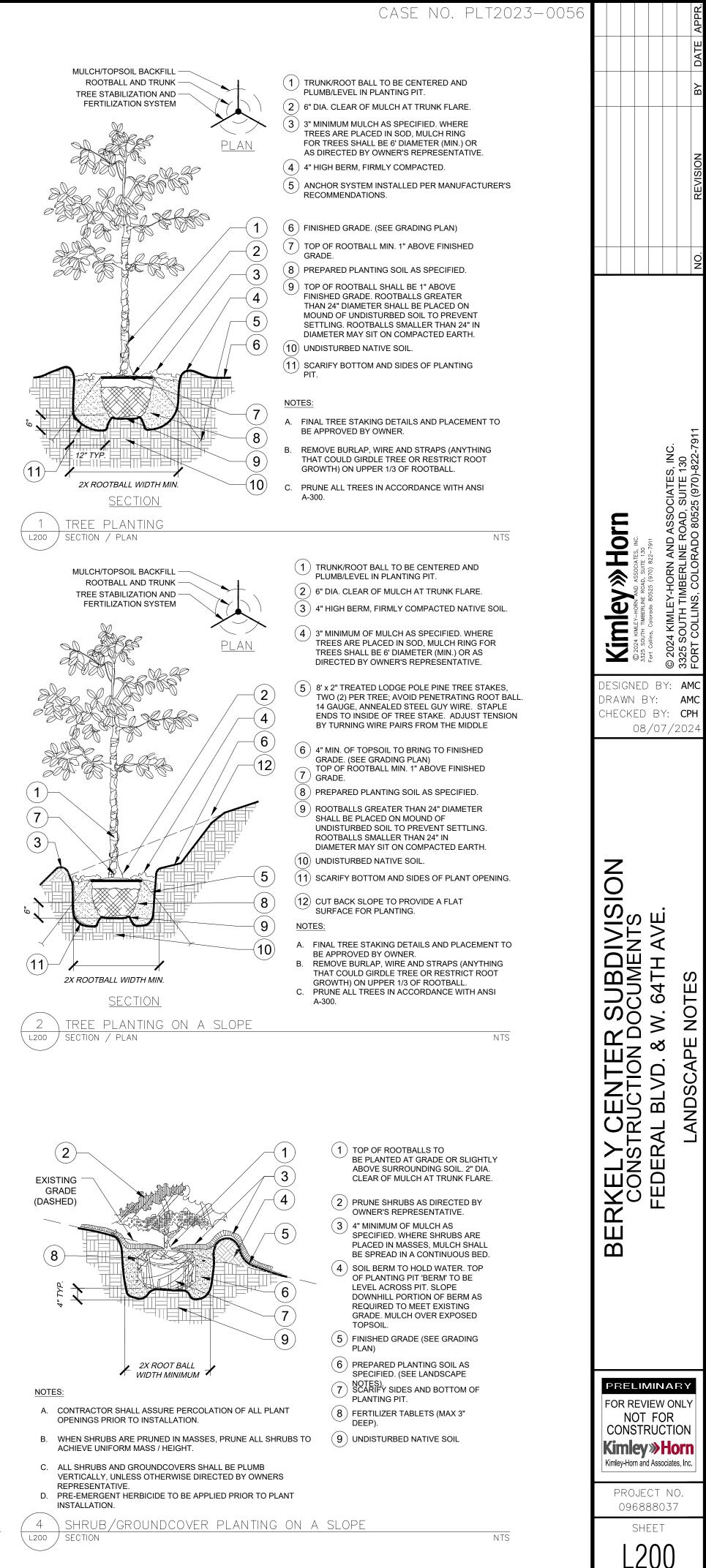
NOTES

- A. CONTRACTOR SHALL ASSURE PERCOLATION OF ALL PLANTING AREAS PRIOR TO INSTALLATION
- B. WHEN SHRUBS ARE PRUNED IN MASSES, PRUNE ALL SHRUBS TO ACHIEVE UNIFORM MASS / HEIGHT
- C. ALL SHRUBS AND GROUNDCOVERS SHALL BE PLUMB VERTICALLY, UNLESS OTHERWISE DIRECTED BY PROJECT LANDSCAPE ARCHITECT.
- SHRUB/GROUNDCOVER PLANTING SECTION / PLAN

D. PRE-EMERGENT HERBICIDE TO BE APPLIED PRIOR TO PLANT INSTALLATION.

SECTION

- 1) TOP OF ROOTBALLS TO BE PLANTED AT GRADE OR SLIGHTLY ABOVE SURROUNDING SOIL. 2" DIA. CLEAR OF MULCH AT TRUNK FLARE.
- 2) PRUNE ALL SHRUBS TO ACHIEVE A UNIFORM
- MASS/HEIGHT. 3) 4" MULCH LAYER AS
- SPECIFIED. (4) EXCAVATE ENTIRE BED
- SPECIFIED FOR GROUNDCOVER (5) FOR CONDITIONS WITH FINISHED
- GRADE OF 4:1 MAX SLOPE ON ALL SIDES (SEE GRADING PLAN).
- 6) PREPARED PLANTING SOIL AS SPECIFIED. (SEE LANDSCAPE NOTES) NOTE: WHEN GROUND COVERS AND SHRUBS USED IN MASSES. ENTIRE BED TO BE AMENDED WITH PLANTING SOIL
- MIX AS SPECIFIED. 7) SCARIFY PLANT OPENING
- SIDES AND BOTTOM. 8) 4" HIGH BERM FIRMLY
- COMPACTED.
- 9 UNDISTURBED NATIVE SOIL.
- 10) FERTILIZER TABLETS (MAX 3" DEEP)
- NTS



EROSION CONTROL DOCUMENTS FOR BERKLEY CENTER SUBDIVISION

SHEET LIST TABLE

SHEET NUMBER SHEET TITLE COVER SHEET EC001 EC002 GENERAL NOTES EC140 **EROSION CONTROL PLAN - INITIAL** EC141 **EROSION CONTROL PLAN - INTERIM** EC142 **EROSION CONTROL PLAN - FINAL** EC550 **EROSION CONTROL DETAILS** EC551 **EROSION CONTROL DETAILS** EC552 **EROSION CONTROL DETAILS**

LEGAL DESCRIPTION:

EC553

PARCEL A: LOT 1. BLOCK 1. ELLETT SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THE NORTH 10 FEET THEREOF CONVEYED TO THE COUNTY OF ADAMS DESCRIBED IN RESOLUTION AND DEED RECORDED NOVEMBER 25, 1969 IN BOOK 1561 AT PAGE 44.

PARCEL B: LOT 1, BLOCK 1, LEXI PAPPAGEORGE SUBDIVISION, COUNTY OF ADAMS, STATE OF COLORADO.

EROSION CONTROL DETAILS

PARCEL C: A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8 AND 320.00 FEET WEST OF THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE THENCE S 90°00'00" W ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 270.38 FEET TO A POINT, SAID POINT BEING 75.00 FEET EAST OF 20.00 FEET SOUTH OF THI N1/4 CORNER OF SECTION 8: THENCE S 44°58'15" W A DISTANCE OF 28.28 FEET TO A POINT OF THE EAST RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, SAID POINT BEING 55.00 FEET EAST AND 40.00 FEET SOUTH OF THE N1/4 CORNER OF SECTION 8: THENCE S 0°03'30" E ALONG THE EAS RIGHT-OF-WAY LINE OF FEDERAL BOULEVARD, A DISTANCE OF 289.80 FEET TO THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE N 90°00'00" E ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8, A DISTANCE OF 141.89 FEET; THENCE N 0°31'25" W A DISTANCE OF 166.68 FEET; THENCE N 89°28'25" E DISTANCE OF 149.85 FEET THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO A POINT ON THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, AND 20.00 FEET SOUTH OF THE POINT OF BEGINNING, COUNTY OF ADAMS STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE BOARD OF COUNTY COMMISSIONERS OF THE COUNTY OF ADAMS, STATE OF COLORADO, AS DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 6, 1907 IN BOOK 33 AT PAGE 220.

AND EXCEPT THAT PORTION TAKEN IN RULE AND ORDER RECORDED OCTOBER 15, 1971 IN BOOK 1745 AT PAGE 484.

ALSO EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE STATE DEPARTMENT OF HIGHWAYS. DIVISION OF HIGHWAYS. STATE OF COLORADO DESCRIBED IN DEED RECORDED DECEMBER 11. 1984 IN BOOK 2945 AT PAGE 579.

AND FURTHER EXCEPTING THEREFROM THAT PORTION CONVEYED TO THE COUNTY OF ADAMS. STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7. 2005 AT RECEPTION NO. 20051107001229480.

PARCEL D:

A PARCEL OF LAND LOCATED IN THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT THE NORTH LINE OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, SAID POINT BEING 345.38 FEET EAST OF THE N1/4 CORNER OF SECTION 8, AND 320.00 FEET WEST OF THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8; THENCE S 0°03'30" E DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE AND THE POINT OF BEGINNING; THENCE S 90°00'00" E A DISTANCE OF 30.00 FEET; THENCE S 0°03'30" W A DISTANCE OF 309.80 FEET TO A POINT ON THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8; THENCE S 90°00'00" W ALONG THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4, OF SECTION 8, A DISTANCE OF 178.49 FEET; THENCE N 0°31'25" W A DISTANCE OF 166.68 FEET; THENCE N 89°28'25" E A DISTANCE OF 149.85 FEET; THENCE N 0°03'30" W A DISTANCE OF 141.76 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVE., AND THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

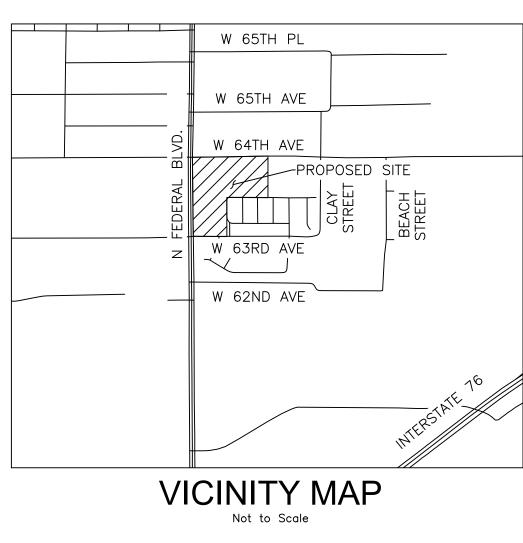
EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

PARCEL E: A PARCEL OF LAND BEING A PORTION OF THE EAST 290.00 FEET OF THE N1/2, NW1/4, NE1/4 OF SECTION 8, TOWNSHIP 3 SOUTH, RANGE 68 WEST, OF THE 6TH P.M., MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT THE NORTHEAST CORNER OF THE N1/2, NW1/4, NW1/4, NE1/4 OF SECTION 8, THENCE SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 20.00 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, WHICH IS THE TRUE POINT OF BEGINNING: THENCE CONTINUING SOUTH ALONG THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH LINE OF THE N1/2, NW1/4, NW1/4, NE1/4; THENCE WEST ALONG THE SOUTH LINE A DISTANCE OF 290.00 FEET; THENCE NORTH AND PARALLEL TO THE EAST LINE OF THE N1/2, NW1/4, NW1/4, NE1/4 A DISTANCE OF 309.80 FEET TO THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE: THENCE EAST ALONG THE SOUTH RIGHT-OF-WAY LINE OF 64TH AVENUE, A DISTANCE OF 290.00 FEET TO THE TRUE POINT OF BEGINNING, COUNTY OF ADAMS, STATE OF COLORADO.

EXCEPT THAT PORTION CONVEYED TO THE COUNTY OF ADAMS, STATE OF COLORADO DESCRIBED IN WARRANTY DEED RECORDED NOVEMBER 7, 2005 AT RECEPTION NO. 20051107001229480.

ADAMS COUNTY, CO FEDERAL BLVD. & 64TH AVE.



MUNICIPAL CONTACT LIST:

ADAMS COUNTY

<u>PLANNING DIVISION</u> 4430 SOUTH ADAMS COUNTY PARKWAY, 1ST FLOOR, SUITE W2000A BRIGHTON, CO 80601 TEL: 720-523-6847 CONTACT: DAVID DEBOSKEY

FIRE DEPARTMENT ADAMS COUNTY FIRE PROTECTION DISTRICT 8055 NORTH WASHINGTON ST. DENVER, CO 80229 TEL: 303-539-6800

WATER UTILITIES CRESTVIEW WATER AND SANITATION DISTRICT TEL: 303-429-1881

STORM/SANITARY UTILITIES CRESTVIEW WATER AND SANITATION DISTRICT TEL: 303-429-1881

ELECTRIC COMPANY XCEL ENERGY

TEL: (800) 895-4999

GAS COMPANY XCEL ENERGY TEL: (800) 895-4999

TELEPHONE COMPANY CENTURY LINK TEL: (866) 449-1979

PROJECT CONTACT LIST:

SURVEYOR OF RECORD ALTURA LAND CONSULTANTS 6950 S TUCSON WAY, UNIT C CENTENNIAL, CO 80112 TEL: (303) 902-7791 CONTACT: JESSE LUGO, PLS

ENGINEER OF RECORD KIMLEY-HORN AND ASSOCIATES, INC. 3801 AUTOMATION WAY, SUITE 210 FORT COLLINS, CO 80525 TEL: (970) 822 7911 CONTACT: JAMES WALLER, PE

QT REAL ESTATE PROJECT MANAGER QUIKTRIP CORPORATION 12000 WASHINGTON ST, STE 175 THORNTON, CO 80241 (303) 248-0436 CONTACT: BRITTANY SIKORSKI

QT CIVIL PROJECT MANAGER QUIKTRIP CORPORATION 4705 SOUTH 129TH EAST AVE TULSA, OK 74134 (918) 615-7685 CONTACT: JOSH POTTER, PE

ARCHITECT: LICKEL ARCHITECTURE 14 W 3RD ST #100 KANSAS CITY, MO 64105 TEL: (913) 389-7866 CONTACT: AMANDA SPITZER

LANDSCAPE ARCHITECT KIMLEY-HORN AND ASSOCIATES, INC. 6200 SOUTH SYRACUSE WAY, SUITE 300 GREENWOOD VILLAGE, CO 80111 TEL: (303) 228–2319 CONTACT: CHRIS HEPLER, PLA

GENERAL NOTES:

1. IN ACCORDANCE WITH GENERALLY ACCEPTED CONSTRUCTION PRACTICES, THE CONTRACTOR SHALL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE, INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND NOT BE LIMITED TO NORMAL WORKING HOURS. ANY CONSTRUCTION OBSERVATION BY THE ENGINEER OF THE CONTRACTOR'S PERFORMANCE IS NOT INTENDED TO INCLUDE REVIEW OF THE ADEQUACY OF THE CONTRACTOR'S SAFETY MEASURES, IN, ON OR NEAR THE CONSTRUCTION SITE.

2. THE CONTRACTOR IS RESPONSIBLE FOR ENSURING THAT ALL NECESSARY PERMITS HAVE BEEN OBTAINED FROM THE GOVERNING AGENCIES AND COORDINATING ALL GOVERNING AGENCY INSPECTIONS REQUIRED THROUGHOUT THE DURATION OF THE PROJECT.

3. CONTRACTOR SHALL BE RESPONSIBLE FOR RAZING AND REMOVAL OF THE EXISTING STRUCTURES RELATED UTILITIES, PAVING, AND ANY OTHER EXISTING IMPROVEMENTS AS NOTED. REFERENCE SITE WORK SPECIFICATIONS.

4. CONTRACTOR IS TO REMOVE AND DISPOSE OF ALL DEBRIS, RUBBISH AND OTHER MATERIALS RESULTING FROM PREVIOUS AND CURRENT DEMOLITION OPERATIONS. DISPOSAL WILL BE IN ACCORDANCE WITH ALL LOCAL, STATE AND/OR FEDERAL REGULATIONS GOVERNING SUCH OPERATIONS.

5. THE CONTRACTOR WILL BE HELD SOLELY RESPONSIBLE FOR DAMAGE TO ADJACENT PROPERTIES AND NEW CONSTRUCTION IN PLACE DURING THE CONSTRUCTION PHASES OF THIS PROJECT. ANY DISTURBED IMPROVEMENTS SHALL BE REPLACED IN KIND AT THE CONTRACTORS EXPENSE.

6. ANY QUANTITIES PROVIDED ON THESE PLANS ARE FOR GENERAL REFERENCE PURPOSES ONLY. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING THE QUANTITIES REQUIRED FOR CONSTRUCTION.

7. THE EXISTING FEATURES SHOWN ON THESE PLANS ARE THOSE NOTED IN THE FIELD AND THOSE TAKEN FROM RECORD DRAWINGS. THERE IS NO GUARANTEE THAT ALL FEATURES (ABOVE OR BELOW GROUND) ARE SHOWN ON THE PLANS. IT IS THE CONTRACTOR'S RESPONSIBILITY TO VERIFY ALL EXISTING FEATURES PRIOR TO BIDDING THE PROJECT.

8. THE CONTRACTOR SHALL LOCATE ALL UTILITIES PRIOR TO BEGINNING CONSTRUCTION BY CONTACTING THE LOCAL UTILITY COMPANIES AND/OR UTILIZING THE LOCAL ONE-CALL SYSTEM. ANY DAMAGE DONE TO EXISTING UTILITIES (THAT ARE TO REMAIN IN PLACE) DURING CONSTRUCTION OPERATIONS WILL BE THE CONTRACTOR'S RESPONSIBILITY AND REPAIRED AT THE CONTRACTOR'S EXPENSE.

9. ALL SITE WORK FOR THIS PROJECT SHALL MEET OR EXCEED THE OWNERS CONTRACT DOCUMENTS AND SPECIFICATIONS. ALL WORK SHALL MEET OR EXCEED THE RELEVANT UTILITY COMPANIES AND REGULATORY AGENCIES, CONTRACT DOCUMENTS AND SPECIFICATIONS. ALL WORK WITHIN PUBLIC AND STATE RIGHT OF WAY SHALL BE IN ACCORDANCE WITH THE GOVERNING AGENCIES STANDARDS AND SPECIFICATIONS

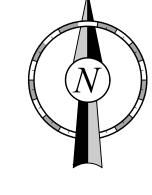
10. TRAFFIC CONTROL SHALL CONFORM TO THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES (MUTCD), CURRENT EDITION. IT IS THE CONTRACTOR'S RESPONSIBILITY TO ENSURE PROPER TRAFFIC CONTROL IS IN PLACE FOR EACH PHASE OF CONSTRUCTION. THE CONTRACTOR IS ALSO RESPONSIBLE FOR PROPERLY MAINTAINING TRAFFIC CONTROL DEVICES THROUGHOUT THE DURATION OF THE WORK. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING TRAFFIC CONTROL PLANS TO THE CITY AND DEPARTMENT OF TRANSPORTATION AS REQUIRED.

WARRANTY/DISCLAIMER:

NOTICE TO BIDDERS:

FLOOD CERTIFICATION:

VERTICAL RELIEF WAS MADE FROM AN ON THE GROUND SURVEY, CONTOURS SHOWN HERON ARE AT 1' INTERVALS USING THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAV 88), GEOID 12A. SITE VERTICAL WAS ESTABLISHED BY USING COUNTY OF DENVER BENCH MARK "156B" LOCATED AT THE SOUTHEAST CORNER OF 50TH AVENUE AND FEDERAL BOULEVARD.



CASE NO. PLT2023-005

WETLANDS NOTICE

ANY DEVELOPMENT, EXCAVATION, CONSTRUCTION, OR FILLING IN A U.S. CORPS OF ENGINEERS DESIGNATED WETLAND IS SUBJECT TO LOCAL, STATE AND FEDERAL APPROVALS. THE CONTRACTOR SHALL COMPLY WITH ALL PERMIT REQUIREMENTS AND/OR RESTRICTIONS AND ANY VIOLATION WILL BE SUBJECT TO FEDERAL PENALTY. THE CONTRACTOR SHALL HOLD THE OWNER/ DEVELOPER, THE ENGINEER AND THE LOCAL GOVERNING AGENCIES HARMLESS AGAINST SUCH VIOLATION

THE DESIGNS REPRESENTED IN THESE PLANS ARE IN ACCORDANCE WITH ESTABLISHED PRACTICES OF CIVIL ENGINEERING FOR THE DESIGN FUNCTIONS AND USES INTENDED BY THE OWNER AT THIS TIME. HOWEVER, NEITHER THE ENGINEER NOR ITS PERSONNEL CAN OR DO WARRANT THESE DESIGNS OR PLANS AS CONSTRUCTED EXCEPT IN THE SPECIFIC CASES WHERE THE ENGINEER INSPECTS AND CONTROLS THE PHYSICAL CONSTRUCTION ON A CONTEMPORARY BASIS AT THE SITE.

ALL QUESTIONS REGARDING THE PREPARATION OF THE GENERAL CONTRACTOR'S BID SHALL BE DIRECTED TO THE OWNER'S CONSTRUCTION REPRESENTATIVE. SUBCONTRACTORS MUST DIRECT THEIR QUESTIONS THROUGH THE GENERAL CONTRACTOR. THE CONSULTING ARCHITECT AND/OR THE CONSULTING ENGINEER SHALL NOT BE CONTACTED DIRECTLY WITHOUT PRIOR AUTHORIZATION FROM THE OWNER/DEVELOPER.

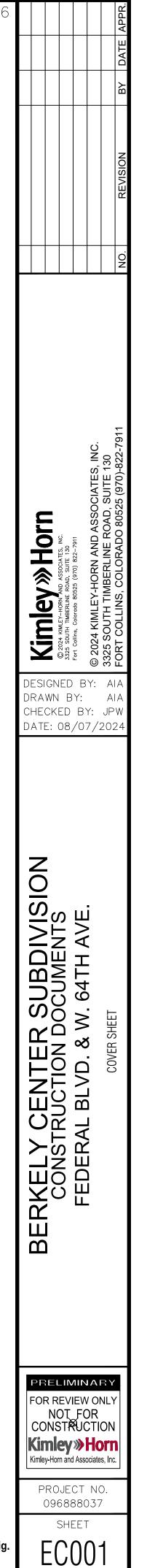
THE FEDERAL EMERGENCY MANAGEMENT AGENCY, FLOOD INSURANCE RATE MAPS NO. 08001C0584H AND NO.08001C0592H, EFFECTIVELY DATED 03/05/2007, INDICATES THIS PARCEL OF LAND TO BE LOCATED IN ZONE X (AREAS DETERMINED TO BE OUTSIDE THE 0.2% ANNUAL CHANCE FLOODPLAIN).

BENCHMARKS

ELEVATION = 5379.63 FEET (NAVD 1988)

BASIS OF BEARINGS

BEARINGS ARE BASED ON THE STATE PLANE COORDINATE SYSTEM ESTABLISHED FOR THE COLORADO NORTH ZONE 0502, NORTH AMERICAN DATUM (NAD) OF 1983. DISTANCES SHOWN HEREON ARE GROUND UNITS. BEING THE NORTH LINE OF THE NORTHEAST 1/4 OF SECTION 8, BEARING S89°49'13"W, BETWEEN MONUMENTS SHOWN HEREON.





Know what's **below**. Call before you dig ADAMS COUNTY EROSION CONTROL PLAN – GENERAL NOTES

- 1. ALL CONSTRUCTION PROJECTS, REGARDLESS OF THE SIZE, SHALL INSTALL, MAINTAIN AND REPAIR STORMWATER POLLUTION CONTROL MEASURES (CMS) TO EFFECTIVELY MINIMIZE EROSION, SEDIMENT TRANSPORT, AND THE RELEASE OF POLLUTANTS RELATED TO CONSTRUCTION ACTIVITY. CMS EXAMPLE INCLUDE: SEDIMENT CONTROL LOGS (SCL), SILT FENCE (SF), DIKES/SWALES, SEDIMENT TRAPS (ST), INLET PROTECTION (IP), OUTLET PROTECTION (OP), CHECK DAMS (CD), SEDIMENT BASINS (SB), TEMPORARY/PERMANENT SEEDING AND MULCHING (MU), SOIL ROUGHENING, MAINTAINING EXISTING VEGETATION AND PROTECTION OF TREES. CMS MUST BE SELECTED, DESIGNED, ADEQUATELY SIZED, INSTALLED AND MAINTAINED IN ACCORDANCE WITH GOOD ENGINEERING, HYDROLOGIC AND POLLUTION CONTROL PRACTICES. CMS/BMPS INSTALLATION AND MAINTENANCE DETAILS SHALL CONFORM TO URBAN DRAINAGE FLOOD CONTROL CRITERIA MANUAL VOLUME 3, OR THE COLORADO DEPARTMENT OF TRANSPORTATION (CDOT) ITEM CODE BOOK. CMS MUST FILTER, SETTLE, CONTAIN OR STRAIN POLLUTANTS FROM STORMWATER FLOWS IN ORDER TO PREVENT BYPASS OF FLOWS WITHOUT TREATMENT. CMS MUST BE APPROPRIATE TO TREAT THE RUNOFF FROM THE AMOUNT OF DISTURBED AREA, THE EXPECTED FLOW RATE, DURATION, AND FLOW CONDITIONS (I.E., SHEET OR CONCENTRATED FLOW). CMS/BMPS SHALL BE SPECIFIED IN THE SWMP (IF APPLICABLE), AND THE LOCATIONS SHOWN ON THE EC PLAN.
- 2. PRIOR TO CONSTRUCTION, PROJECTS DISTURBING 1 OR MORE ACRES OF LAND, OR ANY PROJECT BELONGING TO A COMMON PLAN OF DEVELOPMENT DISTURB 1 OR MORE ACRES, MUST OBTAIN:
- A GENERAL PERMIT FOR STORMWATER DISCHARGES ASSOCIATED WITH CONSTRUCTION ACTIVITIES, FROM THE COLORADO DEPARTMENT OF PUBLIC HEALTH AND ENVIRONMENT, AND
 AN ADAMS COUNTY STORMWATER QUALITY PERMIT WITHIN THE UNINCORPORATED ADAMS COUNTY MS4 AREA.
- 3. PERMITTED PROJECTS SHALL DEVELOP A STORMWATER MANAGEMENT PLAN (SWMP), AKA EROSION AND SEDIMENT CONTROL PLAN (ESCP), IN COMPLIANCE WITH CDPHE MINIMUM REQUIREMENTS. THE APPROVED SWMP, INCLUDING EROSION CONTROL (EC) PLAN (SITE MAP), SHALL BE KEPT ON SITE AND UPDATED AT ALL TIMES. THE QUALIFIED STORMWATER MANAGER IS RESPONSIBLE FOR IMPLEMENTING THE SWMP AND CMS (AKA BMPS) DURING CONSTRUCTION.
- 4. PERMITTED PROJECTS SHALL PERFORM REGULAR STORMWATER INSPECTIONS EVERY 7 CALENDAR DAYS; OR EVERY CALENDAR DAYS AND WITHIN 24 HOURS AFTER ANY PRECIPITATION OR SNOWMELT EVENT THAT CAUSES SURFACE EROSION. INSPECTION FREQUENCY CAN BE REDUCED FOR POST STORM EVENT INSPECTIONS AT TEMPORARILY IDLE SITES AND ALSO FOR STORMWATER INSPECTIONS AT COMPLETED SITES WAITING FOR FINAL STABILIZATION. INSPECTION REPORTS MUST IDENTIFY ANY INCIDENTS OF NON COMPLIANCE.
- 5. TRACKING OF DIRT ONTO PAVED PUBLIC OR PRIVATE PAVED ROADS IS NOT ALLOWED. THE USE OF DIRT RAMPS TO ENTER/EXIT FROM AN UNPAVED INTO A PAVED AREA IS PROHIBITED. VEHICLE TRACKING CONTROLS SHALL BE IMPLEMENTED, OTHERWISE ENTRANCE AREA MUST DRAIN THRU A CM TOWARDS THE PRIVATE SITE.
- 6. TRUCK LOADS OF FILL MATERIAL IMPORTED TO OR CUT MATERIAL EXPORTED FROM THE SITE SHALL BE PROPERLY COVERED TO PREVENT LOSS OF THE MATERIAL DURING TRANSPORTATION ON PUBLIC ROW. HAUL ROUTES MUST BE PERMITTED BY THE COUNTY. NO MATERIAL SHALL BE TRANSPORTED TO ANOTHER SITE WITHOUT APPLICABLE PERMITS.
- 7. CONTROL MEASURES DESIGNED FOR CONCRETE WASHOUT WASTE MUST BE IMPLEMENTED. THIS INCLUDES WASHOUT WASTE DISCHARGED TO THE GROUND AND WASHOUT WASTE FROM CONCRETE TRUCKS AND MASONRY OPERATIONS.
- 8. TEMPORARY CMS/BMPS SHALL BE REMOVED AFTER THE SITE HAS REACHED FINAL STABILIZATION.
- 9. DEWATERING OPERATIONS DISCHARGING OFF SITE INTO ANY WATERS CONVEYANCE SYSTEMS INCLUDING WETLANDS, IRRIGATION DITCHES, CANALS, RIVERS, STREAMS OR STORM SEWER SYSTEMS, REQUIRE A STATE CONSTRUCTION DEWATERING PERMIT.
- 10. PERMITTED PROJECTS SHALL KEEP THE CDPHE'S STORMWATER DISCHARGE PERMIT, STORMWATER MANAGEMENT PLAN (SWMP) AND INSPECTION LOGS AVAILABLE ON SITE THROUGHOUT THE DURATION OF THE PROJECT, AND FOR AN ADDITIONAL 3 YEARS AFTER PERMIT CLOSE OUT.
- 11. PERMITTED LANDOWNER AND/OR CONTRACTOR SHALL CLOSE THE STATE AND CITY/COUNTY PERMIT ONCE FINAL STABILIZATION IS REACHED. STORMWATER INSPECTIONS SHALL CONTINUE UNTIL INACTIVATION NOTICE IS FILED WITH CDPHE.

MAINTENANCE STANDARD NOTES:

- 1. MAINTAIN AND REPAIR CMS ACCORDING TO APPROVED EROSION CONTROL PLAN (CIVIL DRAWING) TO ASSURE THEY CONTINUE PERFORMING AS ORIGINALLY INTENDED.
- 2. CMS/BMPS REQUIRING MAINTENANCE OR ADJUSTMENT SHALL BE REPAIRED IMMEDIATELY AFTER OBSERVATION OF THE FAILING BMP.
- 3. CMS SHALL BE CLEANED WHEN SEDIMENT LEVELS ACCUMULATE TO HALF THE DESIGN UNLESS OTHERWISE SPECIFIED.
- 4. SWMP AND EC PLAN SHALL BE CONTINUOUSLY UPDATED TO REFLECT NEW OR REVISED CMS/BMPS DUE TO CHANGES IN DESIGN, CONSTRUCTION, OPERATION, OR MAINTENANCE, TO ACCURATELY REFLECT THE ACTUAL FIELD CONDITIONS. A NOTATION SHALL BE MADE IN THE SWMP, INCLUDING DATE OF CHANGES IN THE FIELD, IDENTIFICATION OF THE CMS REMOVED, MODIFIED OR ADDED, AND THE LOCATIONS OF THOSE CMS. UPDATES MUST BE MADE WITHIN 72 HOURS FOLLOWING THE CHANGE.
- 5. MAINTAIN VEHICLE TRACKING CONTROL (VTC), IF SEDIMENT TRACKING OCCURS, CLEAN UP IMMEDIATELY. SWEEP BY HAND OR THE USE STREET SWEEPERS (WITH VACUUM SYSTEM). FLUSHING OFF PAVED SURFACES WITH WATER IS PROHIBITED.
- 6. CWA MUST BE CLEANED ONCE WASTE ACCUMULATION REACHES % OF THE WET STORAGE CAPACITY OF THE STRUCTURE. LEGALLY DISPOSED OF CONCRETE WASTE. DO NOT BURY ON-SITE.
- 7. CLEAN-UP SPILLS IMMEDIATELY AFTER DISCOVERY, OR CONTAIN UNTIL APPROPRIATE CLEANUP METHODS CAN BE EMPLOYED.FOLLOW MANUFACTURER'S RECOMMENDED METHODS FOR SPILL CLEANUP, ALONG WITH PROPER DISPOSAL METHODS. RECORDS OF SPILLS, LEAKS, OR OVERFLOWS THAT RESULT IN DISCHARGE OF POLLUTANTS MUST BE DOCUMENTED AND MAINTAINED.
- 8. REMOVE SEDIMENT FROM STORM SEWER INFRASTRUCTURE (PONDS, STORM PIPES, OUTLETS, INLETS, ROADSIDE DITCHES, ETC.), AND RESTORE VOLUME CAPACITY UPON COMPLETION OF PROJECT OR PRIOR TO INITIAL ACCEPTANCE OF PUBLIC IMPROVEMENTS (IF APPLICABLE). DO NOT FLUSH SEDIMENT OFFSITE, CAPTURE ON-SITE AND DISPOSED OF AT AN APPROVED LOCATION.

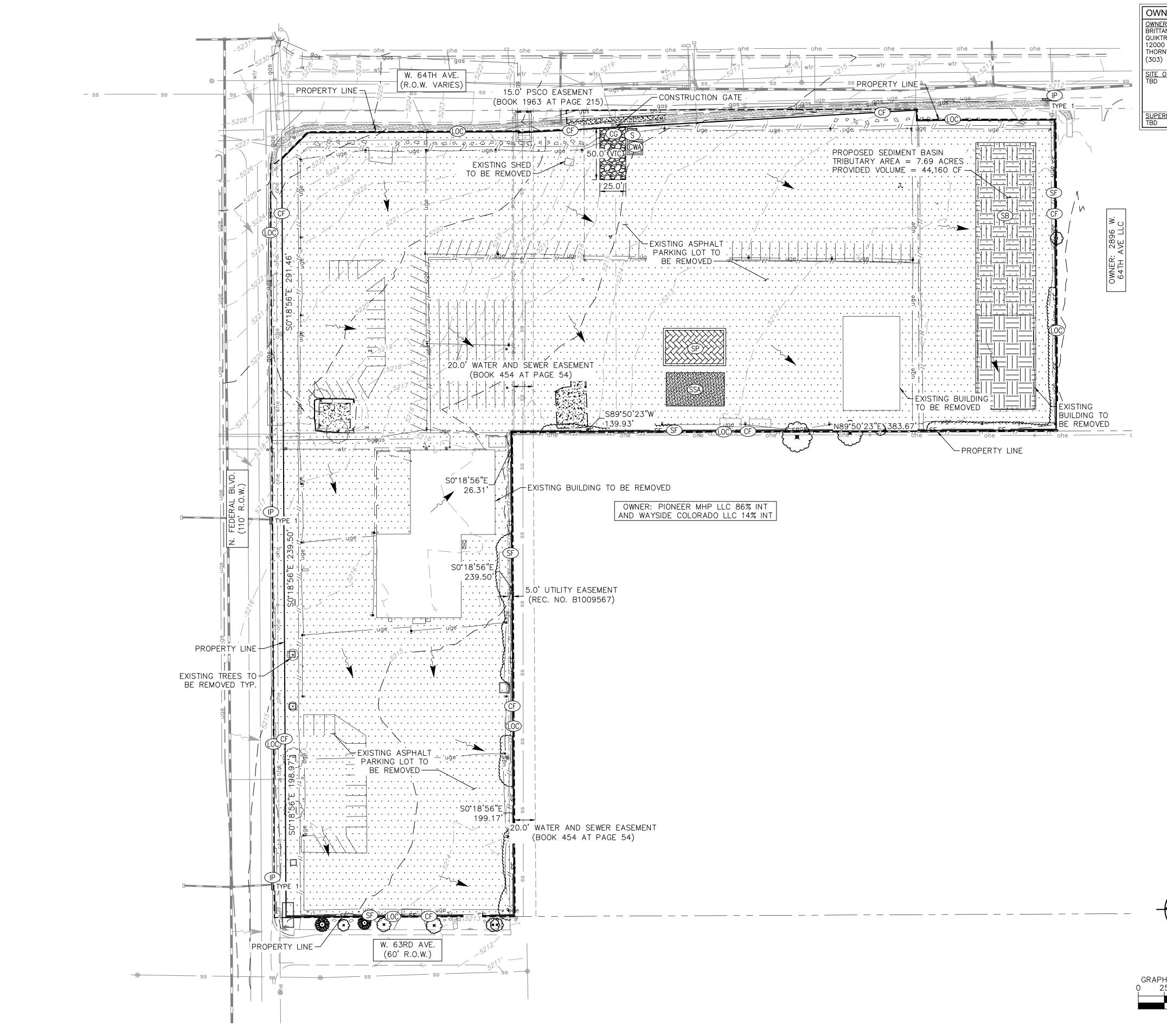
PERFORMANCE STANDARD NOTES:

- 1. STORMWATER RUNOFF FROM DISTURBED AREAS MUST FLOW TO AT LEAST ONE (1) CM TO MINIMIZE SEDIMENT IN THE DISCHARGE. DO NOT ALLOW SEDIMENT TO LEAVE THE SITE. THE BEST WAY TO PREVENT SEDIMENT OR POLLUTANTS FROM ENTERING THE STORM SEWER SYSTEM IS TO STABILIZE THE SITE AS QUICKLY AS POSSIBLE, PREVENTING EROSION AND STOPPING SEDIMENT RUN OFF AT ITS SOURCE.
- 2. PHASE CONSTRUCTION TO MINIMIZE DISTURBED AREAS, INCLUDING DISTURBANCE OF STEEP SLOPES. (I.E. THE ENTIRE PROJECT SITE SHOULD NOT BE DISTURBED IF CONSTRUCTION WILL ONLY BE OCCURRING IN ONE PARTICULAR SECTION OF THE SITE).LIMIT SOIL EXPOSURE TO THE SHORTEST POSSIBLE PERIOD OF TIME. PROTECT NATURAL FEATURES AND EXISTING VEGETATION WHENEVER POSSIBLE. REMOVAL OF EXISTING VEGETATION SHALL BE LIMITED TO THE AREA REQUIRED FOR IMMEDIATE CONSTRUCTION OPERATIONS. MAINTAIN PRE-EXISTING VEGETATION (OR EQUIVALENT CMS) FOR AREAS WITHIN 50 HORIZONTAL FT OF RECEIVING WATERS.
- 3. SOIL COMPACTION MUST BE MINIMIZED FOR AREAS WHERE INFILTRATION CMS WILL OCCUR OR WHERE FINAL STABILIZATION WILL BE ACHIEVED THROUGH VEGETATIVE COVER.
- 4. ALL SOIL IMPORTED TO OR EXPORTED FROM THE SITE SHALL BE PROPERLY COVERED TO PREVENT THE LOSS OF MATERIAL DURING TRANSPORT.
- 5. DUST EMISSIONS RESULTING FROM GRADING ACTIVITIES OR WIND SHALL BE CONTROLLED.
- 6. INSTALL CONSTRUCTION FENCE (ORANGE) TO PROTECT WETLANDS AND OTHER SENSITIVE AREAS AND TO PREVENT ACCESS, AND TO DELINEATE THE LIMITS OF CONSTRUCTION. DO NOT USE SILT FENCE TO PROTECT WETLANDS SINCE TRENCHING MAY IMPACT THESE AREAS.
- 7. CMS INTENDED TO CAPTURE OVERLAND, LOW VELOCITY SHEET FLOW AT A FAIRLY LEVEL GRADE SHALL ONLY BE INSTALLED ALONG CONTOURS.
- 8. INSTALL CMS, SUCH AS CHECK DAMS, PERPENDICULAR TO THE CONCENTRATED FLOWS TO REDUCE FLOW VELOCITY.
- 9. STORM DRAIN INLETS WITHIN AND ADJACENT TO THE CONSTRUCTION SITE MUST BE PROTECTED. ANY PONDING OF STORMWATER AROUND INLET PROTECTION MUST NOT CAUSE EXCESSIVE FLOODING OR DAMAGE ADJACENT AREAS OR STRUCTURES.
- 10. INSTALL VEHICLE TRACKING CONTROL (VTC) TO ENTER/EXIT UNPAVED AREA. DO NOT USE RECYCLED CRUSHED CONCRETE OR ASPHALT MILLINGS FOR VEHICLE TRACKING PADS.
- 11. STRAW BALES SHALL NOT BE USED FOR PRIMARY EROSION OR SEDIMENT CONTROL (I.E. STRAW BALES MAY BE USED FOR REINFORCEMENT BEHIND ANOTHER BMP SUCH AS SILT FENCE).
- 12. OUTLETS SYSTEMS (SUCH AS SKIMMER OR PERFORATED RISER PIPE) SHALL BE INSTALLED TO WITHDRAW WATER FROM OR NEAR THE SURFACE LEVEL WHEN DISCHARGING FROM BASINS. WATER CANNOT DRAIN FROM THE BOTTOM OF THE POND.
- 13. TEMPORARY STABILIZATION MUST BE IMPLEMENTED FOR EARTH DISTURBING ACTIVITIES ON ANY PORTION OF THE SITE WHERE LAND DISTURBING ACTIVITIES HAVE PERMANENTLY OR TEMPORARILY CEASED (FOR MORE THAN 14 CALENDAR DAYS). TEMPORARY STABILIZATION METHODS EXAMPLES: TARPS, SOIL TACKIFIER, AND HYDROSEED. TEMPORARY STABILIZATION REQUIREMENT MAY EXCEED THE 14-DAY SCHEDULE WHEN EITHER THE FUNCTION OF THE SPECIFIC AREA REQUIRES IT TO REMAIN DISTURBED, OR, PHYSICAL CHARACTERISTICS OF THE TERRAIN AND CLIMATE PREVENT STABILIZATION AS LONG AS THE CONSTRAINTS AND ALTERNATIVE SCHEDULE IS DOCUMENTED ON THE SWMP, AND LOCATIONS ARE IDENTIFIED ON THE EC PLAN (SITE MAP).
- 14. RUNOFF FROM STOCKPILE AREA MUST BE CONTROLLED. SOILS THAT WILL BE STOCKPILED FOR MORE THAN 30 DAYS SHALL BE PROTECTED FROM WIND AND WATER EROSION WITHIN 14 DAYS OF STOCKPILE CONSTRUCTION INSTALL CMS/BMPS 5 FT AWAY FROM THE TOE OF THE STOCKPILE'S SLOPE.
- 15. WATER USE TO CLEAN CONCRETE TRUCKS SHALL BE DISCHARGED INTO A CONCRETE WASHOUT AREA (CWA). THE PREDEFINED CONTAINMENT AREA MUST BE IDENTIFIED WITH A SIGN, AND SHALL ALLOW THE LIQUIDS TO EVAPORATE OR DRY OUT. CWA DISCHARGES THAT MAY REACH GROUNDWATER MUST FLOW THROUGH SOIL THAT HAS BUFFERING CAPACITY PRIOR TO REACHING GROUNDWATER. THE CONCRETE WASHOUT LOCATION SHALL BE NOT BE LOCATED IN AN AREA WHERE SHALLOW GROUNDWATER MAY BE PRESENT AND WOULD RESULT IN BUFFERING CAPACITY NOT BEING ADEQUATE, SUCH AS NEAR NATURAL DRAINAGES, SPRINGS, OR WETLANDS. IN THIS CASE, A LINER UNDERNEATH IS NEEDED FOR AREAS WITH HIGH GROUNDWATER LEVELS. CWA SHALL NOT BE PLACED IN LOW AREAS, DITCHES OR ADJACENT TO STATE WATERS. PLACE CWA 50 FT AWAY FROM STATE WATERS.
- 16. WASTE, SUCH AS BUILDING MATERIALS, WORKERS TRASH AND CONSTRUCTION DEBRIS, MUST BE PROPERLY MANAGED TO PREVENT STORMWATER POLLUTION.
- 17. INSTALL STABILIZED STAGING AREA (SSA) TO STORE MATERIALS, CONSTRUCTION TRAILER, ETC.
- 18. IF CONDITIONS IN THE FIELD WARRANT ADDITIONAL CMS/BMPS TO THE ONES ORIGINALLY APPROVED ON THE SWMP OR EC PLAN (CIVIL DRAWING), THE LANDOWNER OR CONTRACTOR SHALL IMPLEMENT MEASURES DETERMINED NECESSARY, AS DIRECTED BY THE COUNTY.
- 19. PERMANENT CMS/BMPS FOR SLOPES, CHANNELS, DITCHES, OR DISTURBED LAND AREA SHALL BE PERFORMED IMMEDIATELY AFTER FINAL GRADING. CONSIDER THE USE EROSION CONTROL BLANKETS ON SLOPES 3:1 OR STEEPER AND AREAS WITH CONCENTRATED FLOWS SUCH AS SWALES, LONG CHANNELS AND ROADSIDE DITCHES.
- 20. THE DISCHARGE OF SANITARY WASTE INTO THE STORM SEWER SYSTEM IS PROHIBITED. PORTABLE TOILETS MUST BE PROVIDED, SECURED AND PLACED ON PERMEABLE SURFACES, AWAY FROM THE CURBSIDE, STORM INLETS AND/OR DRAINAGE WAYS.
- 21. REMOVE TEMPORARY CMS/BMPS ONCE FINAL STABILIZATION IS REACHED, UNLESS OTHERWISE AUTHORIZED.
- 22. FINAL STABILIZATION MUST BE IMPLEMENTED. FINAL STABILIZATION IS REACHED WHEN ALL SOIL DISTURBING ACTIVITIES HAVE BEEN COMPLETED, AND EITHER A UNIFORM VEGETATIVE COVER HAS BEEN ESTABLISHED WITH AN INDIVIDUAL PLANT DENSITY OF AT LEAST 70% OF PRE-DISTURBANCE LEVELS, OR EQUIVALENT PERMANENT ALTERNATIVE METHOD HAS BEEN IMPLEMENTED.
- 23. PROVIDE SPILL PREVENTION AND CONTAINMENT MEASURES FOR CONSTRUCTION MATERIALS, WASTE AND FUEL STORAGE AREAS. BULK STORAGE (55 GALLONS OR GREATER) OF PETROLEUM PRODUCTS AND LIQUID CHEMICALS MUST HAVE SECONDARY CONTAINMENT, OR EQUIVALENT PROTECTION, IN ORDER TO CONTAIN SPILLS AND TO PREVENT SPILLED MATERIAL FROM ENTERING STATE WATERS.
- 24. REPORT SPILLS OR RELEASES OF CHEMICAL, OIL, PETROLEUM PRODUCT, SEWAGE, ETC., WHICH MAY REACH THE STORM SEWER OR ENTER STATE WATERS WITHIN 24-HOURS FROM TIME OF DISCOVERY. GUIDANCE AVAILABLE AT WWW.CDPHE.STATE.CO.US/EMP/SPILLSANDRELEASED.HTM. STATE OF COLORADO SPILL-LINE: 1-877-518-5608. ADAMS COUNTY STORMWATER HOTLINE: 720-523-6400; PUBLIC WORKS 303-453-8787 AND THE TRI-COUNTY HEALTH DEPARTMENT AT 303-220-9200.

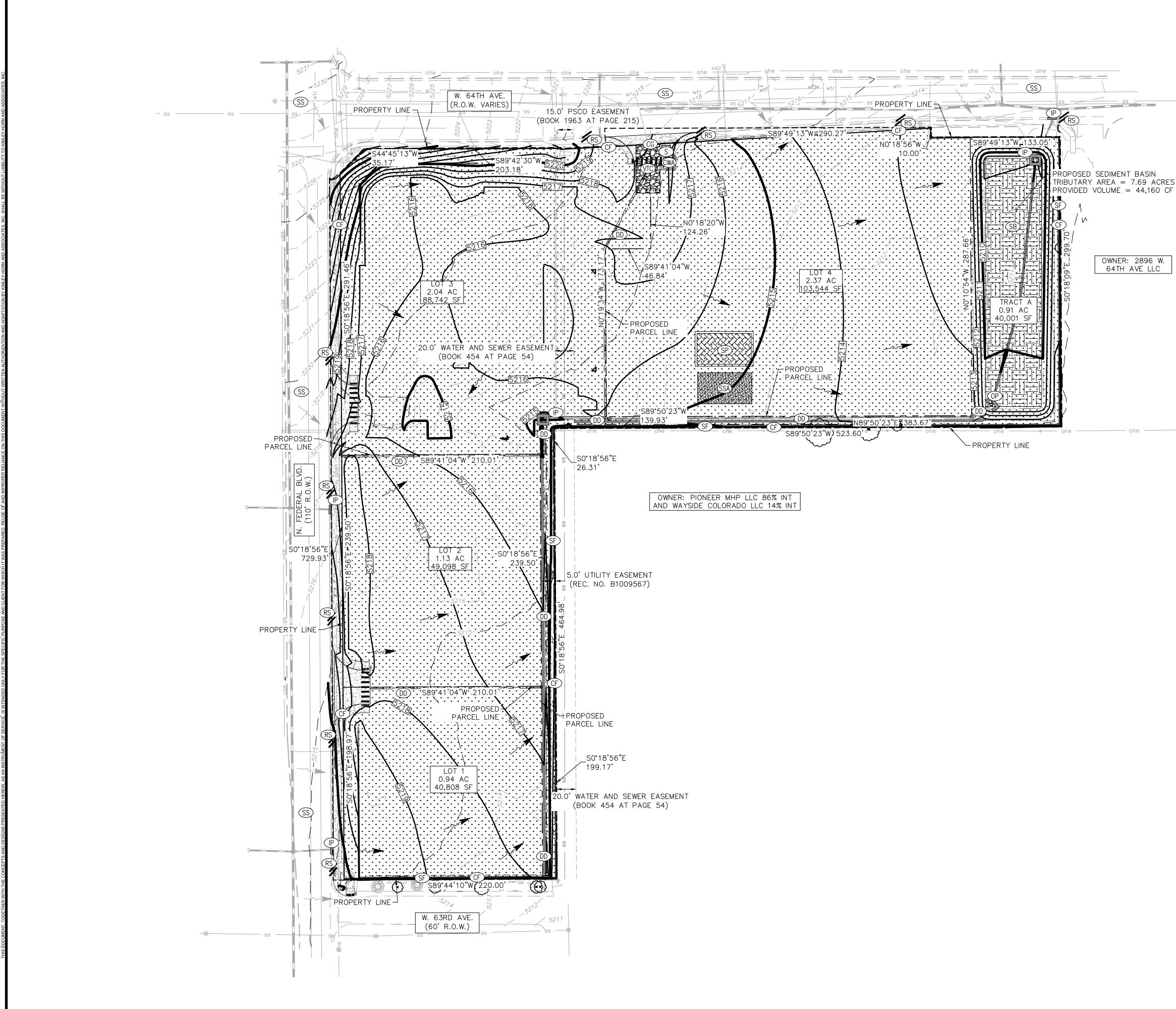
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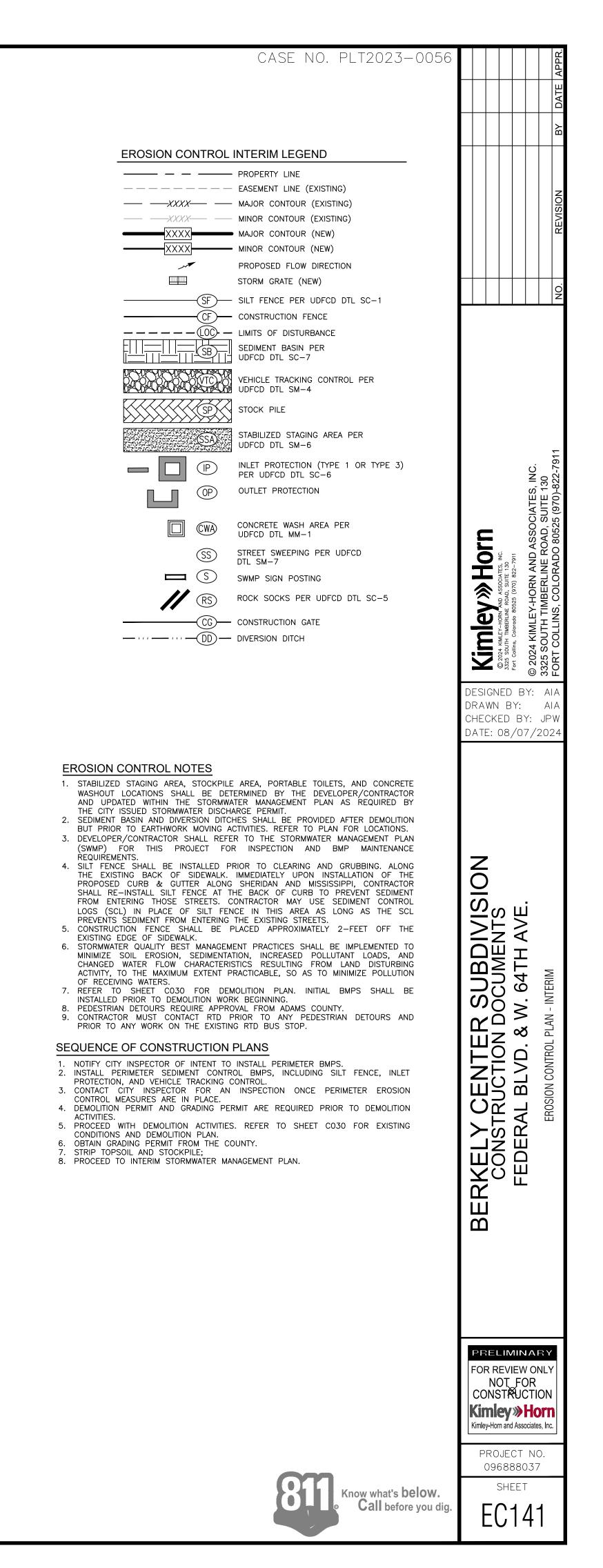
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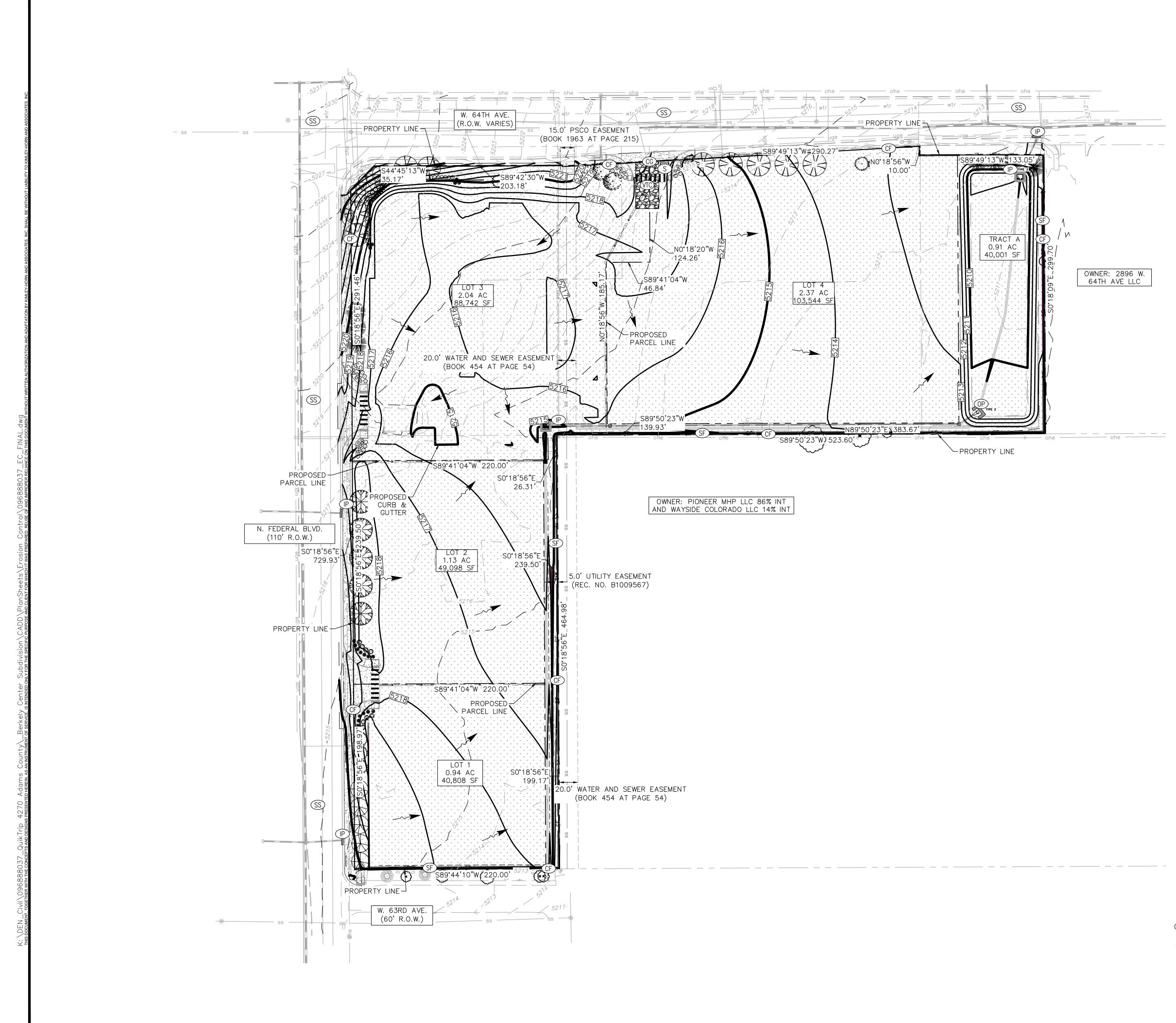
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| VNERSHIP / CONTRACTOR SUMMARY | EROSION CONTROL INITIAL LEGEND | |
| NER/DEVELOPER: TANY SIKORSKI (TRIP CORPORATION 00 WASHINGTON ST, STE 175 IRNTON, CO 80241 3) 248–0436 | | REVISION |
| OPERATOR/GENERAL_CONTRACTOR: | | |
| | E I | |
| IMPERVIOUS AREA±7.59 ACRESLANDSCAPE AREA±0.07 ACRESTOTAL DISTURBED±7.66 ACRES | STOCK PILE STOCK PILE STABILIZED STAGING AREA PER | |
| | UDFCD DTL SM-6 | |
| | CONCRETE WASH AREA PER UDFCD DTL MM-1 | |
| | SS STREET SWEEPING PER UDFCD DTL SM-7 | IC. |
| | IP INLET PROTECTION, TYPE 1 | TES, INC TE 130 70)-822-7 |
| | CG CONSTRUCTION GATE EXISTING FLOW DIRECTION | DTD M.C. |
| | | HOLT MES. INC. 22-7911 AND AS: INE ROA RADO 80 |
| 1. STABILIZED WASHOUT AND UPDA THE CITY 2. SEDIMENT BUT PRIOF 3. DEVELOPEF (SWMP) REQUIREME 4. SILT FENC THE EXIST PROPOSED SHALL RE- FROM ENT LOGS (SC PREVENTS 5. CONSTRUC EXISTING E 6. STORMWATI MINIMIZE CHANGED ACTIVITY, T OF RECEIV 7. REFER TO INSTALLED | STAGING AREA, STOCKPILE AREA, PORTABLE TOILETS, AND CONCRETE LOCATIONS SHALL BE DETERMINED BY THE DEVELOPER/CONTRACTOR TED WITHIN THE STORMWATER MANAGEMENT PLAN AS REQUIRED BY SSUED STORMWATER DISCHARGE PERMIT. BASIN AND DIVERSION DITCHES SHALL BE PROVIDED AFTER DEMOLITION TO EARTHWORK MOVING ACTIVITIES. REFER TO PLAN FOR LOCATIONS. P/CONTRACTOR SHALL REFER TO THE STORMWATER MANAGEMENT PLAN TO EARTHWORK MOVING ACTIVITIES. REFER TO PLAN FOR LOCATIONS. P/CONTRACTOR SHALL REFER TO THE STORMWATER MANAGEMENT PLAN FOR THIS PROJECT FOR INSPECTION AND BMP MAINTENANCE TOT. S. E SHALL BE INSTALLED PRIOR TO CLEARING AND GRUBBING. ALONG ING BACK OF SIDEWALK. IMMEDIATELY UPON INSTALLATION OF THE CURB & GUTTER ALONG SHERIDAN AND MISSISSIPPI, CONTRACTOR -INSTALL SILT FENCE AT THE BACK OF CURB TO PREVENT SEDIMENT ERING THOSE STREETS. CONTRACTOR MAY USE SEDIMENT CONTROL .) IN PLACE OF SILT FENCE IN THIS AREA AS LONG AS THE SCL SEDIMENT FROM ENTERING THE EXISTING STREETS. TION FENCE SHALL BE PLACED APPROXIMATELY 2-FEET OFF THE DGE OF SIDEWALK. ER QUALITY BEST MANAGEMENT PRACTICES SHALL BE IMPLEMENTED TO SOIL EROSION, SEDIMENTATION, INCREASED POLLUTANT LOADS, AND WATER FLOW CHARACTERISTICS RESULTING FROM LAND DISTURBING O THE MAXIMUM EXTENT PRACTICABLE, SO AS TO MINIMIZE POLLUTION ING WATERS. SHEET CO30 FOR DEMOLITION PLAN. INITIAL BMPS SHALL BE PRIOR TO DEMOLITION WORK BEGINNING. N DETOURS REQUIRE APPROVAL FROM THE CITY OF LAKEWOOD | ACCOLOR ACC |
| TRANSPOR 9. CONTRACTO PRIOR TO SEQUENCE 1. NOTIFY CIT 2. INSTALL P PROTECTIO 3. CONTACT CONTROL 4. DEMOLITION ACTIVITIES. 5. PROCEED CONDITION: 6. OBTAIN GR 7. STRIP TOP | A DEIGNOS INCLUENCE INFORME THOME THE OUT OF DEACHOOD ANY WORK ON THE EXISTING RTD BUS STOP. OF CONSTRUCTION PLANS INSPECTOR OF INTENT TO INSTALL PERIMETER BMPS. ENMETER SEDIMENT CONTROL BMPS, INCLUDING SILT FENCE, INLET N, AND VEHICLE TRACKING CONTROL. (ITY INSPECTOR FOR AN INSPECTION ONCE PERIMETER EROSION MEASURES ARE IN PLACE. I PERMIT AND GRADING PERMIT ARE REQUIRED PRIOR TO DEMOLITION WITH DEMOLITION ACTIVITIES. REFER TO SHEET CO30 FOR EXISTING SAND DEMOLITION ACTIVITIES. REFER TO SHEET CO30 FOR EXISTING SOL AND STOCKPILE; TO INTERIM STORMWATER MANAGEMENT PLAN. | BERKELY CENTER SUBDIVISION CONSTRUCTION DOCUMENTS FEDERAL BLVD. & W. 64TH AVE. ROSION CONTROL PLAN - INITIAL |
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| PHIC SCALE IN FEET 25 50 100 | | NOT_FOR CONSTRUCTION Kimley >>> Horn Kimley-Horn and Associates, Inc. |
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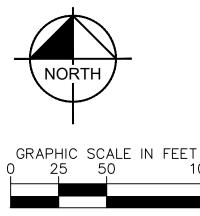


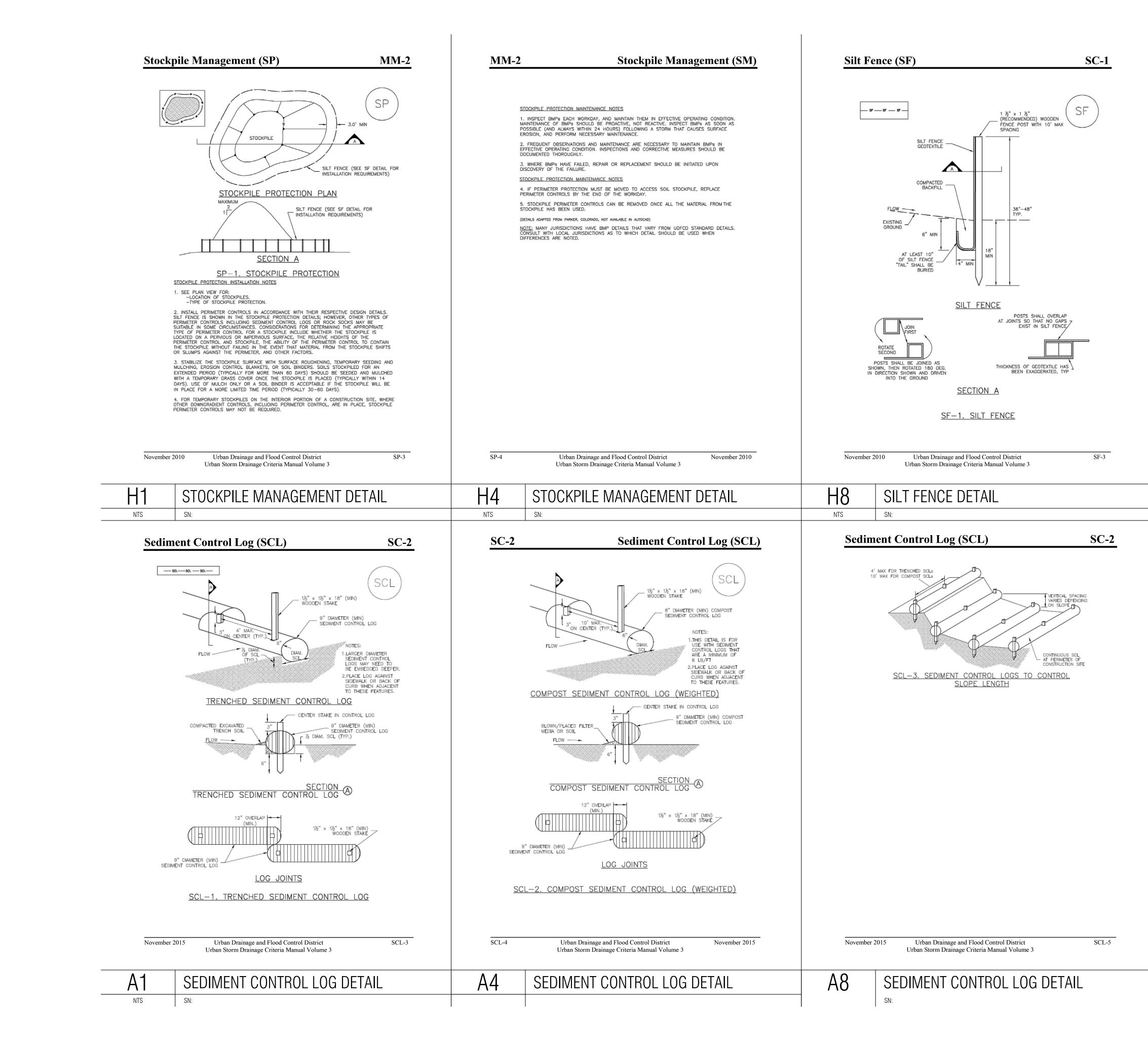




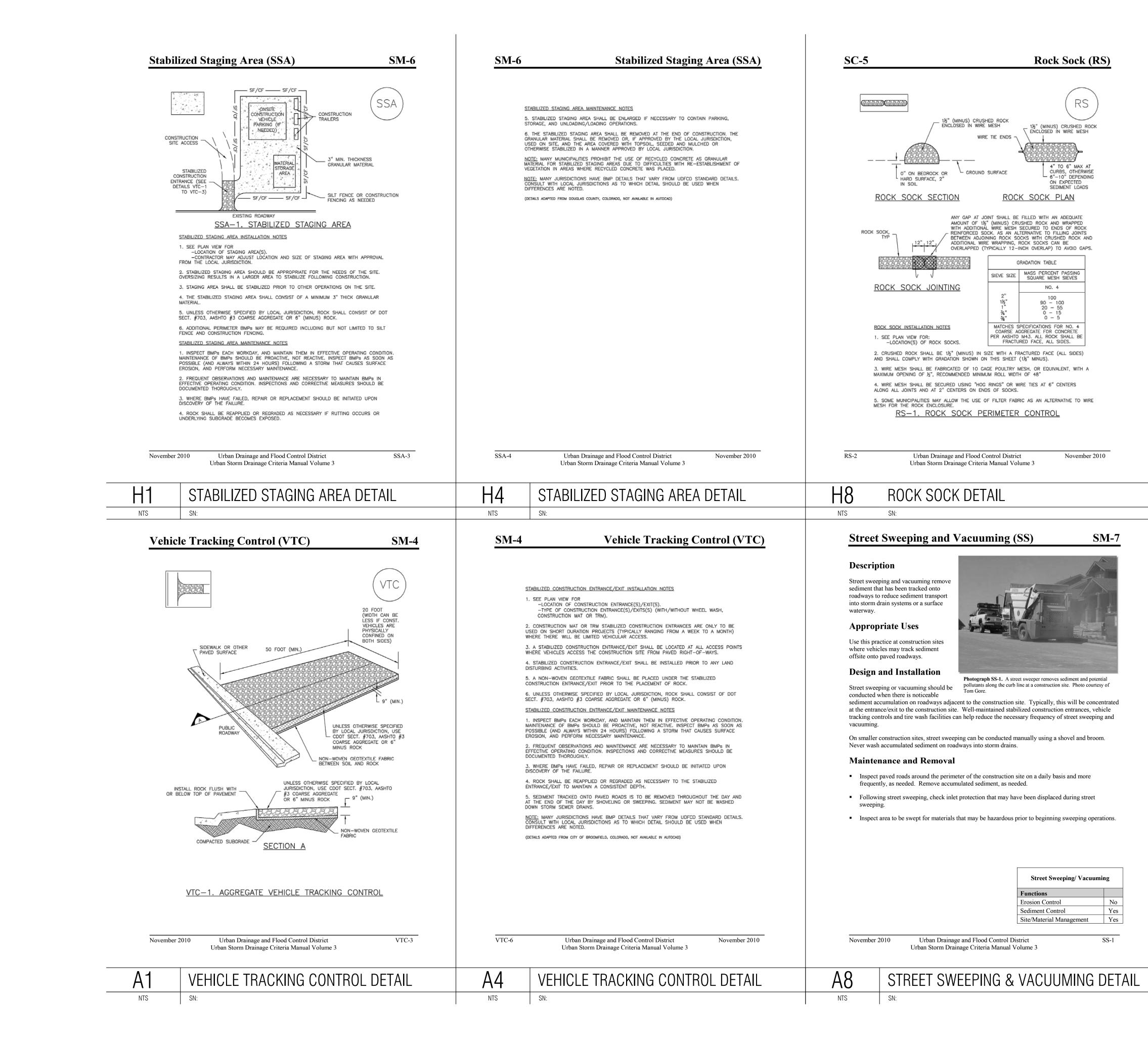
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| EROSION CONTROL NOTES STABILIZED STAGING AREA, STOCKPILE AREA, PORTABLE TOILETS, AND CONCRETE WASHOUT LOCATIONS SHALL BE DETERMINED BY THE DEVELOPER/CONTRACTOR AND UPDATED WITHIN THE STORMWATER MANAGEMENT PLAN AS REQUIRED BY THE CITY ISSUED STORMWATER DISCHARGE PERMIT. SEDIMENT BASIN AND DIVERSION DITCHES SHALL BE PROVIDED AFTER DEMOLITION BUT PRIOR TO EARTHWORK MOVING ACTIVITIES. REFER TO PLAN FOR LOCATIONS. DEVELOPER/CONTRACTOR SHALL REFER TO THE STORMWATER MANAGEMENT PLAN (SWMP) FOR THIS PROJECT FOR INSPECTION AND BMP MAINTENANCE REQUIREMENTS. SILT FENCE SHALL BE INSTALLED PRIOR TO CLEARING AND GRUBBING. ALONG THE EXISTING BACK OF SIDEWALK. IMMEDIATELY UPON INSTALLATION OF THE PROPOSED CURB & GUTTER ALONG SHERIDAN AND MISSISSIPPI, CONTRACTOR SHALL RE-INSTALL SILT FENCE IN THE BACK OF CURB TO PREVENT SEDIMENT FROM ENTERING THE EXISTING STREETS. CONTRACTOR MAY USE SEDIMENT CONTROL LOGS (SCL) IN PLACE OF SILT FENCE IN THIS AREA AS LONG AS THE SCL PREVENTS SEDIMENT FROM ENTERING THE EXISTING STREETS. CONSTRUCTION FENCE SHALL BE PLACED APPROXIMATELY 2-FEET OFF THE EXISTING EDGE OF SIDEWALK. STORMWATER QUALTY BEST MANAGEMENT PRACTICES SHALL BE IMPLEMENTED TO MINIMIZE SOLL EROSION, SEDIMENTATION, INCREASED POLULTANT LOADS, AND CHANGED GOT SIDEWALK. STORMWATER QUALTY BEST MANAGEMENT PRACTICES SHALL BE IMPLEMENTED TO MINIMIZE SOLL EROSION, SEDIMENTATION, INCREASED POLULTANT LOADS, AND CHANGED WATER FLOW CHARACTERISTICS RESULTING FROM LAND DISTURBING ACTIVITY, TO THE MAXIMUM EXTENT PRACTICABLE, SO AS TO MINIMIZE POLUTION OF RECEIVING WATERS. REFER TO SHEATS. REFER TO SHEATS. REFER TO SHEATS. REFER TO DEMOLITION WORK BEGINNING. PEDESTRIAN DETOURS REQUIRE APPROVAL FROM THE CITY OF LAKEWOOD TRANSPORTATION ENGINEERING DAVIDAN DETOURS REQUIRE APPROVAL FROM THE CITY OF LAKEWOOD TRANSPORTATION ENGING. | ACCOLLINS, COLORADO 80525 (970)-822 FORT COLLINS, COLORADO 80525 (970)-822 FORT COLLINS, COLORADO 80525 (970)-822 FORT COLLINS, COLORADO 80525 (970)-822 |
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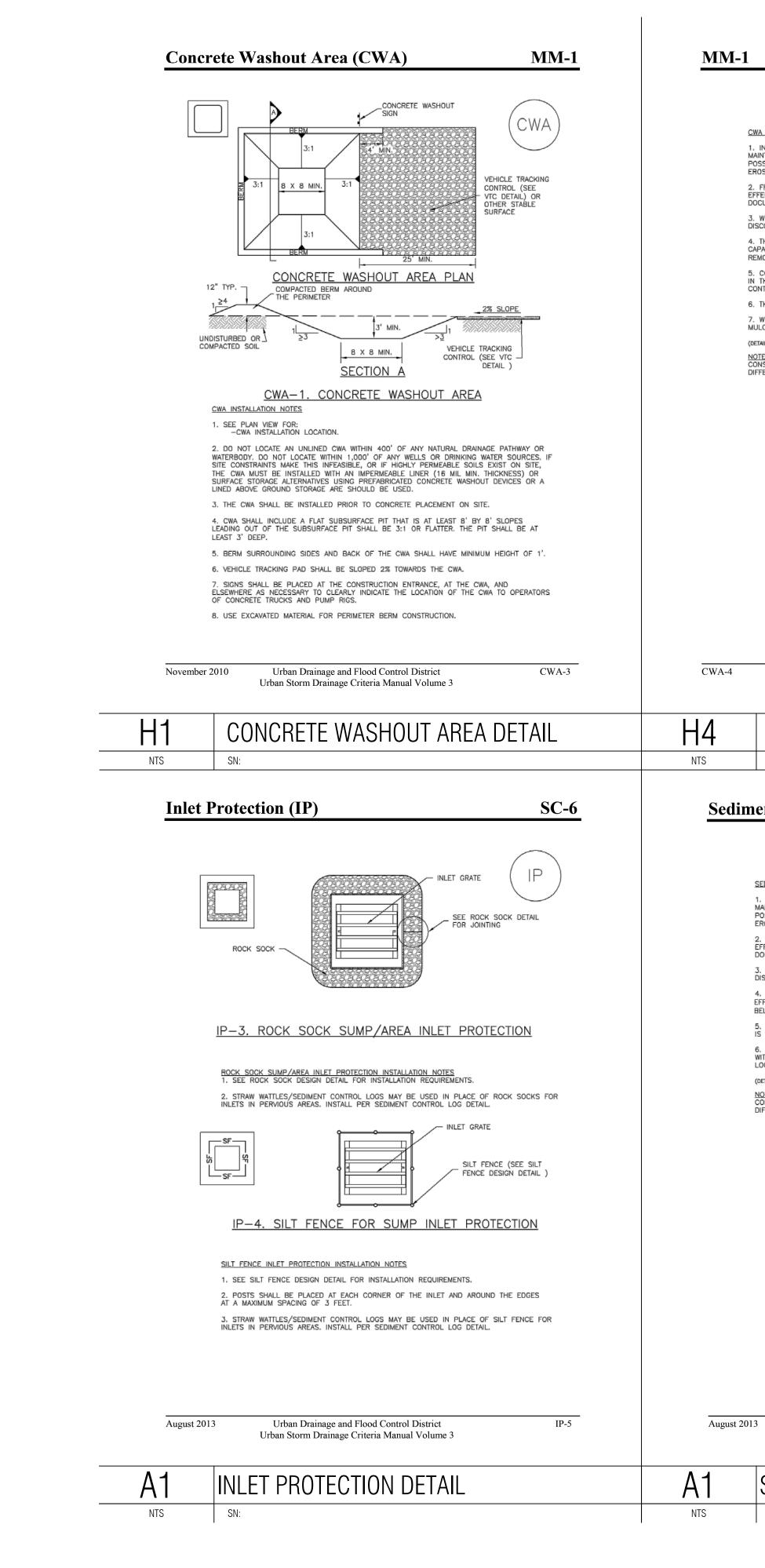




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| | SILT FENCE INSTALLATION NOTES 1. SILT FENCE MUST BE PLACED AWAY FROM THE TOE OF THE SLOPE TO ALLOW FOR WATER PONDING. SILT FENCE AT THE TOE OF A SLOPE SHOULD BE INSTALLED IN A FLAT LOCATION AT LEAST SEVERAL FEET (2-5 FT) FROM THE TOE OF THE SLOPE TO ALLOW ROOM FOR PONDING AND DEPOSITION. 2. A UNIFORM 6" X 4" ANCHOR TRENCH SHALL BE EXCAVATED USING TRENCHER OR SILT FENCE INSTALLATION DEVICE. NO ROAD GRADERS, BACKHOES, OR SIMILAR EQUIPMENT SHALL BE USED. | NO. RE |
| | 3. COMPACT ANCHOR TRENCH BY HAND WITH A "JUMPING JACK" OR BY WHEEL ROLLING. COMPACTION SHALL BE SUCH THAT SILT FENCE RESISTS BEING PULLED OUT OF ANCHOR TRENCH BY HAND. 4. SILT FENCE SHALL BE PULLED TIGHT AS IT IS ANCHORED TO THE STAKES. THERE SHOULD BE NO NOTICEABLE SAG BETWEEN STAKES AFTER IT HAS BEEN ANCHORED TO THE STAKES. 5. SILT FENCE FABRIC SHALL BE ANCHORED TO THE STAKES USING 1" HEAVY DUTY STAPLES OR NAILS WITH 1" HEADS. STAPLES AND NAILS SHOULD BE PLACED 3" ALONG THE FABRIC DOWN THE STAKE. 6. AT THE END OF A RUN OF SILT FENCE ALONG A CONTOUR, THE SILT FENCE SHOULD BE TURNED PERPENDICULAR TO THE CONTOUR TO CREATE A "J-HOOK." THE "J-HOOK" EXTENDING PERPENDICULAR TO THE CONTOUR SHOULD BE OF SUFFICIENT LENGTH TO KEEP RUNOFF FROM FLOWING AROUND THE END OF THE SILT FENCE (TYPICALLY 10' - 20'). | |
| | 7. SILT FENCE SHALL BE INSTALLED PRIOR TO ANY LAND DISTURBING ACTIVITIES. <u>SILT FENCE MAINTENANCE NOTES</u> 1. INSPECT BMPs EACH WORKDAY, AND MAINTAIN THEM IN EFFECTIVE OPERATING CONDITION. MAINTENANCE OF BMPs SHOULD BE PROACTIVE, NOT REACTIVE. INSPECT BMPs AS SOON AS POSSIBLE (AND ALWAYS WITHIN 24 HOURS) FOLLOWING A STORM THAT CAUSES SURFACE EROSION, AND PERFORM NECESSARY MAINTENANCE. 2. FREQUENT OBSERVATIONS AND MAINTENANCE ARE NECESSARY TO MAINTAIN BMPs IN EFFECTIVE OPERATING CONDITION. INSPECTIONS AND CORRECTIVE MEASURES SHOULD BE DOCUMENTED THOROUGHLY. 3. WHERE BMPs HAVE FAILED, REPAIR OR REPLACEMENT SHOULD BE INITIATED UPON DISCOVERY OF THE FAILURE. 4. SEDIMENT ACCUMULATED UPSTREAM OF THE SILT FENCE SHALL BE REMOVED AS NEEDED | JTN 46. 10. 10. 10. 10. 10. 10. 10. 10 |
| | TO MAINTAIN THE FUNCTIONALITY OF THE BMP, TYPICALLY WHEN DEPTH OF ACCUMULATED SEDIMENTS IS APPROXIMATELY 6". 5. REPAIR OR REPLACE SILT FENCE WHEN THERE ARE SIGNS OF WEAR, SUCH AS SAGGING, TEARING, OR COLLAPSE. 6. SILT FENCE IS TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS STABILIZED AND APPROVED BY THE LOCAL JURISDICTION, OR IS REPLACED BY AN EQUIVALENT PERIMETER SEDIMENT CONTROL BMP. 7. WHEN SILT FENCE IS REMOVED, ALL DISTURBED AREAS SHALL BE COVERED WITH TOPSOIL, SEEDED AND MULCHED OR OTHERWISE STABILIZED AS APPROVED BY LOCAL JURISDICTION. (DETAIL ADAPTED FROM TOWN OF PARKER, COLORADO AND CITY OF AURORA, NOT AVAILABLE IN AUTOCAD) NOTE: MANY JURISDICTIONS HAVE BMP DETAILS THAT VARY FROM UDFCD STANDARD DETAILS. CONSULT WITH LOCAL JURISDICTIONS AS TO WHICH DETAIL SHOULD BE USED WHEN | Contraction (Contraction) (Con |
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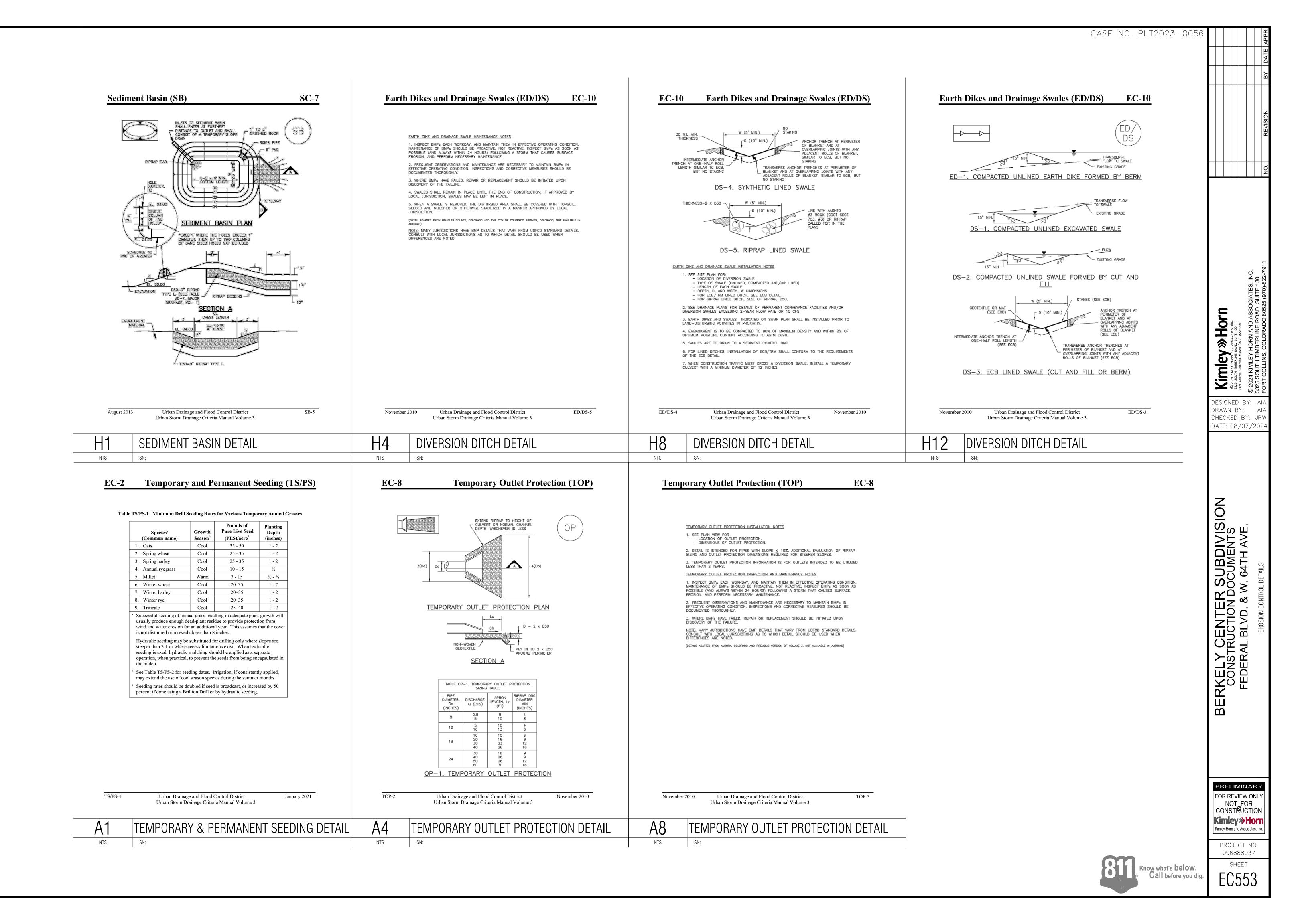


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| -LOCATION OF INLET PROTECTION. -TYPE OF INLET PROTECTION (IP.1, IP.2, IP.3, IP.4, IP.5, IP.6) INLET PROTECTION SHALL BE INSTALLED PROMPTLY AFTER INLET CONSTRUCTION OR PAVING IS COMPLETE (TYPICALLY WITHIN 48 HOURS). IF A RAINFALL/RUNOFF EVENT IS FORECAST, INSTALL INLET PROTECTION PRIOR TO ONSET OF EVENT. | , , , , , , , , , , , , , , , , , , , |
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| 4. SEDIMENT ACCUMULATED UPSTREAM OF INLET PROTECTION SHALL BE REMOVED AS NECESSARY TO MAINTAIN BMP EFFECTIVENESS, TYPICALLY WHEN STORAGE VOLUME REACHES 50% OF CAPACITY, A DEPTH OF 6" WHEN SILT FENCE IS USED, OR ¼ OF THE HEIGHT FOR STRAW BALES. 5. INLET PROTECTION IS TO REMAIN IN PLACE UNTIL THE UPSTREAM DISTURBED AREA IS PERMANENTLY STABILIZED, UNLESS THE LOCAL JURISDICTION APPROVES EARLIER REMOVAL OF | -7911 |
| INLET PROTECTION IN STREETS. 6. WHEN INLET PROTECTION AT AREA INLETS IS REMOVED, THE DISTURBED AREA SHALL BE COVERED WITH TOP SOIL, SEEDED AND MULCHED, OR OTHERWISE STABILIZED IN A MANNER APPROVED BY THE LOCAL JURISDICTION. | ATES, INC JITE 130 (970)-822- |
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| IN THE MANUFACTURER'S DETAILS. <u>NOTE:</u> SOME MUNICIPALITIES DISCOURAGE OR PROHIBIT THE USE OF STRAW BALES FOR INLET PROTECTION. CHECK WITH LOCAL JURISDICTION TO DETERMINE IF STRAW BALE INLET PROTECTION IS ACCEPTABLE. | MIEY-HORN AND H TIMBERUNE RO 4. COLOTOGO 80525 KIMLEY-H DUTH TIMI |
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Berkely Center Subdivision (64th & Federal) Adams County, Colorado

Prepared for:

QuikTrip Corporation 4705 South 129th East Ave Tulsa, OK 74134-7008 (918) 615-7685

Prepared by:

Kimley-Horn and Associates, Inc. 3325 South Timberline Road, Suite 130, CO 80525 (970) 822-7911

Project #: 096888037







Level 3 Storm Drainage Study – Berkely Center Subdivision

CERTIFICATION

ENGINEER'S STATEMENT

"I hereby certify that this report for the drainage design of Berkely Center Subdivision was prepared by me or under my direct supervision in accordance with the provisions of Adams County Storm Drainage Design and Technical Criteria for the owners thereof. I understand that Adams County does not and will not assume liability for drainage facilities designed by others."

James Waller , P.E. Colorado Registered PE #60876 Date



OWNER STATEMENT

"QuikTrip Corporation hereby certifies that the drainage facilities for Berkley Center Subdivision shall be constructed according to the design presented in this report. I understand that Adams County does not and will not assume liability for the drainage facilities designed and/ or certified by my engineer. I understand that Adams County reviews drainage plans pursuant to Colorado Revised Statues Title 30, Article 28; but cannot, on behalf of Berkley Center Subdivision, guarantee that final drainage design review will absolve QuikTrip Corporation and/ or their successors and/ or assigns the future liability for improper design. I further understand that approval of the Final Plat and/ or Final Development Plan does not imply approval of my engineer's drainage design."

(Property Owner Signature)

Date

Name:QuikTrip CorporationAddress:12000 Washington Street, Suite 175
Thornton, CO 80241Phone:(303) 248-0436Contact:Brittany Sikorski



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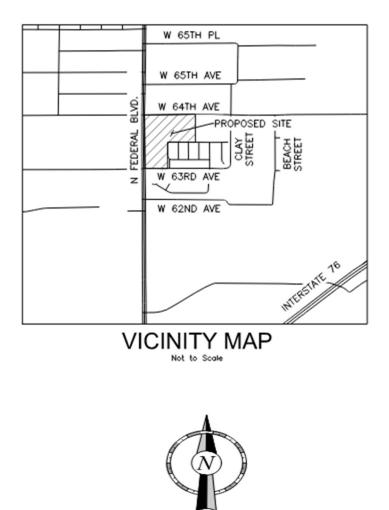
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Kinley Horn Level 3 Storm Drainage Study – Berkely Center Subdivision

GENERAL LOCATION AND PROJECT DESCRIPTION

LOCATION

The Site is located at the at Southeast corner of Federal Boulevard and West 64th Avenue in Adams County, Colorado. The Site totals approximately 7.41 acres. The site is bounded by Federal Boulevard to the west, West 64th Avenue to the north, commercial development to the east, West 63rd Avenue to the south, and mobile residential community to the southeast. A vicinity map has been included below for reference.





PROJECT DESCRIPTION

The existing site is planned to be subdivided into five (5) lots totaling 7.41 acres, with a total disturbed area of 7.68 acres. The lot on the corner of Federal Blvd. and 64th Avenue will be a subdivision with five (5) proposed lots to be developed at a future date. The site is zoned Commercial-5 (C-5) and the proposed lots will include business suburban, and light industrial.

EXISTING CONDITIONS

The existing site is currently a vacant used car sales lot. The majority of the site is covered with asphalt pavement, ~90% of the total area. The remaining site area is classified as roofed area with minimal landscaping onsite. The existing drainage pattern generally sheet flows from the northwest to the southeast with slopes ranging from 1%-8%. Along the Project frontage, Federal Blvd slopes to the south at 1%-3% and 64th Ave slopes to the east around 1%-5%. There are no existing onsite detention or water quality facilities, and all drainage patterns flow offsite. The historic runoff pattern within the adjacent rights-of-way will be maintained and will not be negatively the proposed Project.

FLOOD STUDIES

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) Panel 08001C0584H (effective March 5, 2007) and C0592H, the Site is entirely located in "Zone X", which is considered an area of minimal flood hazard, outside of the regulatory floodplain. The FEMA FIRM associated with the Site is included in **Appendix A**. A portion of the offsite area south of the site is located within zone AE and no construction is proposed within this area.

SOIL REPORT

An NRCS soil study for the project was obtained to determine the soil characteristics of the site. The result of this study shows that the majority of the site is Wet alluvial land at approximately 78%, 22% Loamy alluvial land which are classified as hydraulic soil groups D, C respectively. The NRCS soil report can be found in **Appendix B** of this report.

MAJOR DRAINAGE BASIN DESCRIPTION

According to the Mile High Flood District (MHFD), this project is located within the Clear Creek Watershed (Basin ID 4300). This basin is a tributary of First Creek. The overall drainage basin is generally undeveloped and drainage facilities immediately downstream of this site are in place.

EXISTING SUB-BASIN DESCRIPTION

For more detailed information on the sub-basins, please reference the *Existing Drainage Plan* in **Appendix E.** In addition, **Table 2** following this section provides additional detail for rational calculation summaries and outfalls. With no existing onsite detention and water quality, all basins in the existing sub-basins outfall offsite. Existing hydrologic calculations are included in **Appendix C**.

Sub-Basin EX-1

Sub-basin EX-1 is a 7.26-acre area that contains the majority of the existing site. This area is comprised of minimal to no vegetation and asphalt paving. There are three (3) existing buildings onsite providing 0.53 acres of roof coverage. Runoff from subbasin EX-1 sheet flows southeast across the site and outfalls into the residential community.



Sub-Basin EX-2

Sub-basin EX-2 is a 0.28-acre area that consists of asphalt paving along the western portion of the site. Runoff from Basin EX-2 sheet flows west offsite onto Federal Blvd. and is conveyed south along Federal Blvd. via curb and gutter to an existing Denver 13 Combination inlet (Design Point 1).

Sub-Basin EX-3

Sub-basin EX-3 is a 0.07-acre area that consists of asphalt paving along the northern portion of the site. Runoff from Basin EX-3 sheet flows North offsite onto 64th Ave. and is conveyed east along 64th Ave. via curb and gutter to an existing Denver 13 Combination inlet (Design Point 2).

Sub-Basin EX-4

Sub-basin EX-4 is a 0.05-acre area that consists of native vegetation along the northern portion of the site. Runoff from basin EX-3 sheet flows north offsite onto 64th Avenue and is conveyed east along 64th Avenue via curb and gutter to existing Denver 13 Combination inlet (Design Point 2).

| | | <u> </u> | , | | | |
|----------------|-------------------------------|--|------|------------------|-------|--|
| | RATIONAL CALCULATIONS SUMMARY | | | | | |
| DESIGN POINT | TRIBUTARY | RIBUTARY TRIBUTARY AREA IMPERVIOUSNESS | | PEAK FLOWS (CFS) | | |
| | BASINS | (AC) | % | Q5 | Q100 | |
| On-Site Basins | | | | | | |
| | EX-1 | 7.26 | 98% | 28.48 | 58.71 | |
| 1 | EX-2 | 0.28 | 100% | 1.12 | 2.30 | |
| 2 | EX-3 | 0.07 | 100% | 0.21 | 0.43 | |
| 2 | EX-4 | 0.05 | 2% | 0.00 | 0.15 | |

Table 2: Existing Rational Calcs Summary

DEVELOPED SITE DRAINAGE CONDITIONS

The proposed drainage design will incorporate the use of drainage swales and/or concrete pans to convey runoff to a local inlet. Once the flows have been captured by the inlet, the runoff will be routed via underground storm pipe to the proposed regional extended detention basin (EDB) for treatment.

The site has been divided into seven (7) onsite basins and three (3) offsite subbasins. All of the onsite subbasins will be captured and conveyed to the proposed EDB with the exception of subbasins OF-E1 and OF-AB1. After runoff is released from the EDB, runoff will outfall to the existing storm system in 64th Avenue. For more detailed information on the sub-basins, please reference the *Proposed Drainage Plan* in **Appendix A. Table 3** following this section provides additional detail for rational calculation summaries and outfalls. Proposed hydrologic calculations are included in **Appendix D.**



PROPOSED SUB-BASIN DESCRIPTION

<u>ONSITE</u>

Sub-Basin A-1

Sub-basin A-1 is a 0.89-acre area that is designed for future development consistent with allowed uses in applicable zoning. Subbasin A-1 has an assumed imperviousness of 75% based on **Table 6.3** in Adams County Stormwater Drainage Design and Stormwater Quality Control Regulations manual ("the Manual"). Runoff will be conveyed via overland flows into a concrete pan on the eastern side of the site and routed north through B-1 to design point C in Basin C-1. A temporary swale will be installed to convey all runoff from A-1 to the pan.

Sub-Basin B-1

Sub-basin B-1 is a 1.12-acre area that is designed for future development consistent with allowed uses in applicable zoning. Subbasin B-1 has an assumed imperviousness of 75% based on **Table 6.3** in The Manual. Runoff will be conveyed via overland flows into a concrete pan on the eastern side of the site and routed north through to design point C in Basin C-1. A temporary swale will be installed to convey all runoff from B-1 to the pan.

Sub-Basin C-1

Sub-basin C-1 is a 2.04-acre area that is designed for future development consistent with allowed uses in applicable zoning. Subbasin C-1 has an assumed imperviousness of 75% based on **Table 6.3** in the manual. Runoff will be conveyed via overland flows to design point C in Basin C-1. A temporary swale will be installed to convey all runoff from C-1 to the pan. During the 100-year event, inlet A-4 will overtop and follow drainage patterns east across basin D-1 into basin E-1.

Sub-Basin D-1

Sub-basin D-1 is a 2.37-acre area that is designed for future development consistent with allowed uses in applicable zoning. Subbasin D-1 has an assumed imperviousness of 80% based on **Table 6.3** in the Manual. The runoff will be conveyed via sheet flow to the proposed EDB at the east side of the site.

Sub-Basin OF-AB1

Sub-basin OF-AB1 is a 0.13-acre area that is comprised of landscaping and pavement along the western portion of the site. Flows on the surface will not be captured by proposed storm infrastructure and will be routed offsite to Federal Blvd. where it will be routed via curb and gutter to EX Design Point 1.

Sub-Basin E-1

Sub-basin E-1 is a 0.76-acre area that is comprised of the proposed EDB that will serve future development sites. Flows will be conveyed to the concrete pan in the previous basins and then into the proposed EDB and treated for water quality and detention (Design Point 1). Flows will then be released at historic flow rates to the existing storm system at Existing Design point 2.



Sub-Basin OF-E1

Sub-basin OF-E1 is a 0.10-acre area that is comprised of landscaping along the eastern portion of the site. Flows on the surface will not be captured by proposed storm infrastructure and will be routed offsite to the existing residential community following existing drainage patterns.

OFFSITE

Sub-Basin OS-C1

Sub-basin OS-C1 is a 0.10-acre offsite area that is comprised of landscaping and pavement along the west side of the site. Flows on the surface will be conveyed by overland flows into proposed Basin C-1 and follow the respective drainage patterns of each basin. See Basin C-1 for proposed drainage patterns.

Sub-Basin OF-AB2

Sub-basin OF-AB3 is a 0.10-acre offsite area that is comprised of landscaping and pavement along the eastern side of the site. Flows on the surface will not be captured by proposed storm infrastructure and will be routed offsite east to Federal Blvd. where they will be routed via curb and gutter to EX Design Point 1.

Sub-Basin OS-D1

Sub-basin OS-D1 is a 0.06-acre offsite area that is comprised of landscaping and pavement along the northern side of the site. Flows on the surface will be conveyed by overland flows into proposed Basin D-1 and follow the respective drainage patterns of the basin.

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| | TRIBUTARY | TRIBUTARY AREA | IMPERVIOUSNESS | PEAK FLOWS (CFS) | | | |
|-----------------|----------------|----------------|----------------|------------------|-------|--|--|
| DESIGN POINT | BASINS | (AC) | % | Q5 | Q100 | | |
| On-Site Basins | On-Site Basins | | | | | | |
| | A1 | 0.89 | 75% | 2.55 | 4.87 | | |
| | B1 | 1.12 | 75% | 3.10 | 5.92 | | |
| | C1 | 2.04 | 75% | 6.03 | 11.51 | | |
| | D1 | 2.37 | 80% | 8.07 | 15.40 | | |
| | El | 0.76 | 2% | 0.03 | 2.56 | | |
| | OF-E1 | 0.10 | 2% | 0.00 | 0.46 | | |
| | OF-AB1 | 0.12 | 24% | 0.12 | 0.65 | | |
| TOTAL 7.41 | | 67% | 19.90 | 41.37 | | | |
| Off-Site Basins | | | | | | | |
| OS-C1 | OS-C1 | 0.10 | 58% | 0.25 | 0.69 | | |
| OF-AB2 | OF-AB2 | 0.10 | 71% | 0.31 | 0.75 | | |
| OS-D1 | OS-D1 | 0.06 | 16% | 0.04 | 0.29 | | |
| TOTAL | <i>(</i> | 0.26 | 54% | 0.60 | 1.74 | | |

Table 3: Proposed Rational Calcs Summary Table

The total tributary area to the Pond is 7.34 acres. The total runoff to the Pond from these basins is 17.14 cfs in the 5-year storm event and 36.72 in the 100-year storm event.

Tributary Tributary Imperviousness Q₅ (cfs) Q₁₀₀ (cfs) Basins Area (ac) A-E1,OS-C1,OS-20.07 Tributary to 7.34 68% 41.24 D1 Pond Tributary OF-E1,OF-0.43 0.33 25% 1.86 AB1,OF-AB2 Offsite

Table 4: Pond Tributary Areas



DRAINAGE FACILITY DESIGN

GENERAL CONCEPT

Stormwater runoff will be conveyed in conformance with historic drainage patterns, flowing into the storm sewer systems on site, and ultimately into Clear Creek. Developed runoff will be collected via curb and gutter, concrete pans, and storm sewer inlets. The onsite storm system will convey to the EDB located at the eastern edge of the site for water quality and detention storage of the excess urban runoff volume (EURV) and 100-yr event.

OFFSITE FEDERAL BLVD.

In the existing condition, the tributary area outfalling to Design Point 1 along Federal Blvd. is 0.28 acres with a runoff of 1.12 cfs in the 5-year storm event and 2.30 in the 100-year storm event. In the proposed condition, the tributary area (OF-AB1,OF-AB2) outfalling to Design Point 1 is 0.23 acres with a runoff of 0.43 cfs for the 5-year storm event and 1.40 cfs in the 100-year storm event discharges. The proposed condition decreases flow from the existing condition, therefore the proposed improvements will not negatively impact the downstream storm infrastructure at Design Point 1.

OFFSITE 64TH AVE

In the existing condition, the tributary area outfalling to Design Point 1 along 64th Avenue is 0.12 acres with a runoff of 0.21 cfs in the 5-year storm event and 0.58 in the 100-year storm event. In the proposed condition, there are no proposed areas outfalling to 64th Avenue The proposed condition decreases flow from the existing condition, therefore the proposed improvements will not negatively impact the downstream storm infrastructure at Design Point 1.

OFFSITE SOUTHEAST (RESIDENTIAL SUBDIVISION)

In the existing condition, the tributary area outfalling to Design Point 1 along Federal Blvd. is 7.26 acres with a runoff of 28.48 cfs in the 5-year storm event and 58.71 in the 100-year storm event. In the proposed condition, the tributary area (OF-E1) outfalling to offsite is 0.10 acres with a runoff of 0.00 cfs for the 5-year storm event and 0.46 cfs in the 100-year storm event discharges. The proposed condition decreases flow from the existing condition; therefore the proposed improvements will not negatively impact the downstream storm infrastructure.

ONSITE

In the existing condition, there are no means for onsite detention or water quality. All stormwater sheet flows southeast across the site to the residential subdivision with a totaling flow of 28.48 cfs in the 5-year storm event and 58.71 cfs in the 100-year storm event. In the proposed condition, the flows will be redirected to the EDB on the eastern side of the site through curb and gutters, concrete pans, and proposed storm pipe. The areas tributary to the EDB (A1-E1, OS-C1, OS-D1) are 7.34 acres with a total flow of 20.07 cfs in the 5-year storm event and 41.24 cfs in the 100-year storm event. A minimum of 1' of freeboard is provided in the pond from the 100-year water surface elevation (WSE) and the top of pond. Detention calculations are provided in **Appendix D**. The pond will have a controlled release that will discharge flows at historic rates via outlet structures to the public storm sewer systems. This pond outfall pipe will also be sized to provide capacity for the 100-year storm event. Clear Creek is the ultimate tributary for the site. An emergency overflow path is also provided for runoff to convey flows from the pond to the 64th Avenue right-of-way.

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DETENTION POND DESIGN

According to adams county Drainage Manual, Detention of flood flows is required for all development and redevelopment projects and should be designed to control the 5-year and 100-year recurrence interval floods. The total tributary area to the proposed detention pond is 7.34-acres including Subbasins A1, B1, C1, D1, E1, Pond,OS-C1,OS-D1, with a weighted imperviousness of 68%. The 100year detention volume required for the pond is 0.396 acre-feet with proposed conditions of the site, as calculated by the MHFD detention spreadsheet included in **Appendix C**. 8

The proposed detention pond is designed to have a bottom elevation of 5209.00 and a top spillway elevation of 5212.00. The pond is a Swirl-Bay design per City and County of Denver Detail Figure 13.1S. The proposed pond will provide a total volume of 0.904 acre-feet. The outlet structure has been designed to meet the Water Quality Capture Volume (WQCV) and drain time requirements in conformance with the Manual. The proposed orifice plate provides a WQCV release rate of 0.10 cfs and a drain time of 40 hours. The 5-year flows are controlled by the orifice plate with a release rate of 0.60 cfs. The 100-year flows are controlled by the overflow weir structure and restrictor plate on the outlet pipe providing a release rate of 8.40 cfs. The release rates with the proposed development are less than those in the existing condition and drain times are in conformance with those in the Manual. Orifice plate and outlet sizing calculations are provided in **Appendix D**.

PERMANENT STORMWATER QUALITY

Permanent water quality will be provided in the on-site surface water quality and detention pond in accordance Mile High Flood District and Adams County code. Each detention facility is sized adequately to treat and release the water quality capture volume (WQCV) in at least 40 hours per the adams county Drainage Manual. The total WQCV for the disturbed Project area is 0.16 acre-feet. The owner will provide long term operation and maintenance of the detention and water quality facilities. Approximately 4.5% of the total disturbed area is discharging without being treated, which is in compliance with the 20% maximum requirement, see **Appendix C** for PSC calculations.

CONCLUSIONS

The stormwater drainage design for the project has been done in accordance with the standards set forth in the Adams County Storm Drainage Design and Stormwater Quality Control Regulations and the Urban Storm Drainage Criteria Manual. Stormwater runoff will be safely conveyed through a series of private storm sewer networks without negatively impacting adjacent properties or the existing infrastructure.



REFERENCES

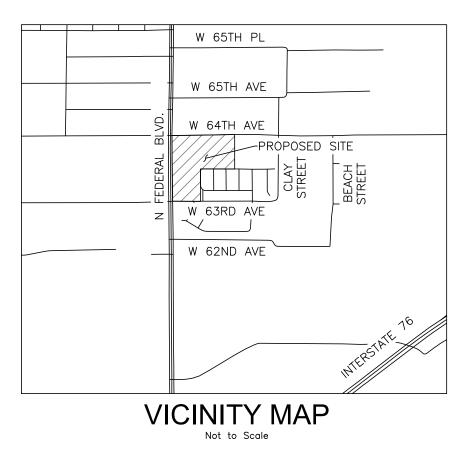
- 1. Storm Water Drainage Design and Stormwater Quality Control Regulations, Dated December, 8 2020, prepared by Adams County.
- 2. Urban Storm Drainage Criteria Manual, Volumes 1-3, prepared by Mile High Flood District, Updated October 2019.
- 3. Flood Insurance Rate Map, Adams County, Colorado and Incorporated Areas, Map Number 08001C0592H, Revised March 5, 2007, prepared by the Federal Emergency Management Agency (FEMA)

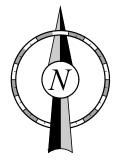


APPENDIX A - MAPS

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Berkley Center Subdivision





National Flood Hazard Layer FIRMette

250

500

1,000

1.500



Legend

regulatory purposes.

105°1'48"W 39°48'55"N SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT Without Base Flood Elevation (BFE) Zone A. V. A9 With BFE or Depth Zone AE, AO, AH, VE, AR SPECIAL FLOOD HAZARD AREAS **Regulatory Floodway** 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X T03S R68W S5 Future Conditions 1% Annual Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF 08001C0584H FLOOD HAZARD Area with Flood Risk due to Levee Zone D eff. 3/5/2007 NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS AREA OF MINIMAL FLOOD HAZARD Area of Undetermined Flood Hazard Zone D Zone X - — – – Channel, Culvert, or Storm Sewer GENERAL STRUCTURES LIIII Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation ADAMS COUNTY **Coastal Transect** UNINCORPOOATED AREAS (5202 Mase Flood Elevation Line (BFE) Limit of Study 080001 Jurisdiction Boundary **Coastal Transect Baseline** OTHER Profile Baseline FEATURES Hydrographic Feature **Digital Data Available** No Digital Data Available MAP PANELS Unmapped T03S R68W S8 LOMR 11-08-0995P eff. 8/30/2011 The pin displayed on the map is an approximate point selected by the user and does not represent 08001C0592 an authoritative property location. Zone AE (EL 5213 Feet This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 11/20/2023 at 6:44 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time. 5213 FE This map image is void if the one or more of the following map NOODWAY elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for 105°1'11"W 39°48'27"N Feet unmapped and unmodernized areas cannot be used for

1:6.000

2,000

Basemap Imagery Source: USGS National Map 2023



APPENDIX B – SOILS INFORMATION



United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Adams County Area, Parts of Adams and Denver Counties, Colorado



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map



| | MAP L | EGEND |) | MAP INFORMATION |
|--------------------|--|-------------------------|---|--|
| | terest (AOI) Area of Interest (AOI) | 8 | Spoil Area Stony Spot | The soil surveys that comprise your AOI were mapped at 1:20,000. |
| • | Soil Map Unit Polygons Soil Map Unit Lines Soil Map Unit Points Point Features | Ø ♥ ▲ Water Fe | Very Stony Spot Wet Spot Other Special Line Features | Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale. |
| © ∞ ≈ ≈ | Blowout Borrow Pit Clay Spot Closed Depression Gravel Pit Gravelly Spot | Transpor | Streams and Canals | Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) |
| © ∧ ∜ | Landfill Lava Flow Marsh or swamp Mine or Quarry | Backgrou | Local Roads | Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. |
| ◎ ○ + :: | Miscellaneous Water Perennial Water Rock Outcrop Saline Spot Sandy Spot | | | This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Adams County Area, Parts of Adams and Denver Counties, Colorado Survey Area Data: Version 19, Sep 1, 2022 |
| ⇒ ♦ Ø | Severely Eroded Spot Sinkhole Slide or Slip Sodic Spot | | | Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jul 1, 2020—Jul 2, 2020 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background |

MAP LEGEND

MAP INFORMATION

imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|-----------------------------|-------------------------------------|--------------|----------------|
| Gr | Gravelly land-Shale outcrop complex | 0.0 | 0.2% |
| Lw | Loamy alluvial land, moderately wet | 1.5 | 21.6% |
| Wt | Wet alluvial land | 5.3 | 78.2% |
| Totals for Area of Interest | | 6.8 | 100.0% |

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The

delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Adams County Area, Parts of Adams and Denver Counties, Colorado

Gr—Gravelly land-Shale outcrop complex

Map Unit Setting

National map unit symbol: 34vy Elevation: 4,400 to 5,500 feet Mean annual precipitation: 12 to 14 inches Mean annual air temperature: 46 to 54 degrees F Frost-free period: 120 to 160 days

Map Unit Composition

Gravelly land: 65 percent *Shale outcrop:* 35 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Gravelly Land

Setting

Landform: Hillslopes Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Linear Parent material: Colluvium derived from mixed and/or slope alluvium derived from mixed

Typical profile

H1 - 0 to 3 inches: gravelly sand *H2 - 3 to 60 inches:* gravelly sand

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7s Hydrologic Soil Group: A Ecological site: R067BY063CO - Gravel Breaks Hydric soil rating: No

Description of Shale Outcrop

Typical profile

H1 - 0 to 60 inches: unweathered bedrock

Properties and qualities

Slope: 15 to 45 percent
Depth to restrictive feature: 0 inches to paralithic bedrock
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8s Hydrologic Soil Group: D Ecological site: R067BY045CO - Shaly Plains Hydric soil rating: No

Lw—Loamy alluvial land, moderately wet

Map Unit Setting

National map unit symbol: 34w5 Elevation: 4,000 to 5,500 feet Mean annual precipitation: 12 to 14 inches Mean annual air temperature: 48 to 52 degrees F Frost-free period: 135 to 155 days Farmland classification: Not prime farmland

Map Unit Composition

Loamy alluvial land: 70 percent Minor components: 30 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Loamy Alluvial Land

Setting

Landform: Drainageways Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from mixed

Typical profile

H1 - 0 to 6 inches: variable H2 - 6 to 36 inches: stratified loam to clay loam H3 - 36 to 60 inches: sand

Properties and qualities

Slope: 0 to 1 percent
Drainage class: Somewhat poorly drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 6.00 in/hr)
Depth to water table: About 18 to 36 inches
Calcium carbonate, maximum content: 5 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 6.0 inches)

Interpretive groups

Land capability classification (irrigated): 3w Land capability classification (nonirrigated): 4w Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Nunn

Percent of map unit: 12 percent *Hydric soil rating:* No

Satanta

Percent of map unit: 12 percent Landform: Paleoterraces Hydric soil rating: No

Fluvaquentic haplustolls

Percent of map unit: 6 percent Landform: Sloughs Hydric soil rating: Yes

Wt—Wet alluvial land

Map Unit Setting

National map unit symbol: 34xj Elevation: 4,000 to 5,600 feet Mean annual precipitation: 12 to 14 inches Mean annual air temperature: 48 to 52 degrees F Frost-free period: 125 to 155 days Farmland classification: Not prime farmland

Map Unit Composition

Wet alluvial land: 100 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Wet Alluvial Land

Setting

Landform: Flood plains Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium derived from mixed

Typical profile

H1 - 0 to 8 inches: variable *H2 - 8 to 36 inches:* stratified sandy loam to clay *H3 - 36 to 60 inches:* sand

Properties and qualities

Slope: 0 to 1 percent
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.06 to 6.00 in/hr)
Depth to water table: About 6 to 24 inches
Calcium carbonate, maximum content: 15 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): 5w

Custom Soil Resource Report

Land capability classification (nonirrigated): 5w Hydrologic Soil Group: D Ecological site: R067BY038CO - Wet Meadow Hydric soil rating: Yes



APPENDIX C - HYDROLOGY

Kimley »Horn

BASIN SUBTOTAL

2%

91%

1%

STANDARD FORM SF-1 EXISTING RUNOFF COEFFICIENTS - IMPERVIOUS CALCULATION

PROJECT NAME: Berkely Center Subdivision PROJECT NUMBER: 096888037

DATE: 3/29/2024 CALCULATED BY: AIA CHECKED BY: JPW SOIL: Hydrologic Soil Group D
 CONCRETE
 BUSINESS
 INDUSTRIAL

 AREA
 SUBURBAN
 LIGHT

 0.79
 0.79
 0.79

 0.81
 0.81
 0.81

 0.83
 0.83
 0.83

 0.87
 0.87
 0.87

 90%
 75%
 80%
 LANDSCAPE ROOF <u>E: AREA</u> <u>AREA</u> <u>F. 0.01 0.79</u> <u>F. 0.05 0.81</u> ASPHALT AREA 0.83 LAND USE: 2-YEAR COEFF. 5-YEAR COEFF. 10-YEAR COEFF. 0.85 0.15 0.83 0.87 100-YEAR COEFF. IMPERVIOUS % 0.87 0.49 0.89 ANDSCAPE AREA (AC) ROOF AREA (AC) ASPHALT AREA (AC) CONCRETE AREA (AC) BUSINESS AREA (AC) INDUSTRIAL AREA (AC) TOTAL AREA DESIGN DESIGN BASIN POINT (AC) C(2) C(5) C(10) C(100) Imp % On-Site Basins 7.29 0.28 0.07 0.05 7.68
 0.82
 0.84
 0.86
 0.89
 98%

 0.83
 0.85
 0.87
 0.89
 100%

 0.83
 0.85
 0.87
 0.89
 100%

 0.01
 0.05
 0.15
 0.49
 2%

 0.82
 0.84
 0.86
 0.88
 98%
 EX-1 0.53 0.00 0.07 6.66 0.05 0.00 0.00 0.00 0.53 7% EX-2 EX-3 0.00 0.00 0.00 0.05 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0% 0.00 0.00 0.28 0.00 7.01 0.12

100%

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|-------------------------|--------------------------------|---|----------------|-----------------------|-------|--|-------|---------------------|-----------------------|------------------|--------------|--------|------------|-------|-------|-----------|
| PROJECT N CALCULA | | Berkely Cent 096888037 AIA JPW | er Subdivision | I | | | | | | | | | | | DATE: | 3/29/2024 |
| SUB-BA | | | | NITIAL | | | TRA | VEL TIM | Е | | | | Тс СНЕС | | | FINAL |
| DATA | | m | | IME (T _i) | | | | (T _t) | | - | | | RBANIZED 1 | , | | Tc |
| DESIGN | AREA | C5 | LENGTH | | Ti | LENGTH | SLOPE | C _v | VEL | T _t | COMP. | TOTAL | TOTAL | TOTAL | Te | |
| BASIN | Ac | | Ft | % | Min. | Ft. | % | | fps | Min. | tc | LENGTH | SLOPE | IMP. | Min. | Min. |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | |
| On-Site Basins | | | | | | | | | | | | | | | | |
| EX-1 | 7.29 | 0.84 | 200 | 0.5% | 8.5 | | 0.5% | 20.0 | 1.4 | | 8.5 | 200 | 0.5% | 98% | 11.3 | 8.5 |
| EX-2 | 0.28 | 0.85 | 20 | 0.5% | 2.6 | | 0.5% | 20.0 | 1.4 | | 2.6 | 20 | 0.5% | 100% | 9.2 | 5.0 |
| EX-3 | 0.07 | 0.85 | 10 | 1.0% | 1.4 | | 1.0% | 20.0 | 2.0 | | 1.4 | 10 | 1.0% | 100% | 9.1 | 5.0 |
| EX-4 | 0.05 | 0.05 | 10 | 2.0% | 4.8 | | 2.0% | 20.0 | 2.8 | | 4.8 | 10 | 2.0% | 2% | 25.8 | 5.0 |
| $t_i = \frac{0.395(}{}$ | $\frac{(1.1-C_5)}{S_o^{0.33}}$ | $\sqrt{L_i}$ | I | $t_t = \frac{1}{60}$ | L_i | $\overline{\underline{b}}_{o} = \frac{L_{t}}{60V_{t}}$ | 8 | $t_{\rm c} = (26 -$ | $17i) + \frac{1}{60}$ | L_t (14i+9) | $\sqrt{S_i}$ | | | | | |

STANDARD FORM SF-3 EXISTING STORM DRAINAGE DESIGN - RATIONAL METHOD 5 YEAR EVENT

PROJECT NAME: Berkely Center Subdivision PROJECT NUMBER: 096888037

 P_1 (1-Hour Rainfall) = 1.42

DATE: 3/29/20

CALCULATED BY: AIA CHECKED BY: JPW

Kimley »Horn

| | | | | DIRI | ECT RU | JNOF | F | | | TOTAL | RUN | OFF | STR | EET |] | PIPE | | TRAV | EL TI | ſ |
|---------------|--------|-----------------|--------------|-----------------|----------|---------|--------------|------------|---------|----------------|--------------|------------|--------------|--------------------|------------|--------------|-------------------|------|--------------|---|
| STORM LINE | DESIGN | DESIGN BASIN | AREA (AC) | RUNOFF COEFF | tc (min) | C*A(ac) | I (in/hr) | Q (cfs) | tc(max) | S(C*A) (ac) | I (in/hr) | Q (cfs) | (%) SLOPE | STREET FLOW(cfs |)))) | SLOPE (%) | PIPE SIZE (in) | E (E | VELOCIT Y | |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | (18) | (19) | (20) | |

On-Site Basins

| | | EX-1 | 7.29 | 0.82 | 8.46 | 5.98 | 4.09 | 24.48 | | | | | | |
|--|---|------|------|------|------|------|------|-------|--|--|--|--|--|--|
| | 1 | EX-2 | 0.28 | 0.83 | 5.00 | 0.23 | 4.82 | 1.12 | | | | | | |
| | 2 | EX-3 | 0.07 | 0.83 | 5.00 | 0.06 | 4.82 | 0.27 | | | | | | |
| | 2 | EX-4 | 0.05 | 0.01 | 5.00 | 0.00 | 4.82 | 0.00 | | | | | | |

| REMARKS |
|---------|
| |
| (22) |
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| |

STANDARD FORM SF-3 EXISTING STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT

PROJECT NAME: Berkely Center Subdivision

P₁ (1-Hour Rainfall) = 2.71 DATE: 3/29/2

PROJECT NUMBER: 096888037

CALCULATED BY: AIA CHECKED BY: JPW

Kimley »Horn

| CILCILL DI | 51 11 | | | | | | | | | | | | | | | | | | |
|---------------|--------------|-----------------|--------------|-----------------|----------|---------|--------------|------------|---------|----------------|--------------|------------|-----------|--------------------|--------------------|------|-------------------|--------------|--------------|
| | | | | DIR | ECT R | UNOFF | | |] | ГОТАL | RUNC |)FF | STR | EET | | PIPE | | TRAV | /EL TI |
| STORM LINE | POINT | DESIGN BASIN | AREA (AC) | RUNOFF COEFF | tc (min) | C*A(ac) | I (in/hr) | Q (cfs) | tc(max) | S(C*A) (ac) | I (in/hr) | Q (cfs) | SLOPE (%) | STREET FLOW(cfs | DESIGN FLOW(cfs | 0% | PIPE SIZE (in) | (ft) (ft) | VELOCIT Y |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | (18) | (19) | (20) |

On-Site Basins

| | | EX-1 | 7.29 | 0.89 | 8.46 | 6.46 | 7.81 | 50.47 | | | | | | |
|--|---|------|------|------|------|------|------|-------|--|--|--|--|--|--|
| | 1 | EX-2 | 0.28 | 0.89 | 5.00 | 0.25 | 9.19 | 2.30 | | | | | | |
| | 2 | EX-3 | 0.07 | 0.89 | 5.00 | 0.06 | 9.19 | 0.55 | | | | | | |
| | 2 | EX-4 | 0.05 | 0.49 | 5.00 | 0.02 | 9.19 | 0.21 | | | | | | |

| 9/202 | 24 | |
|-------|-------------|---------|
| TIN | ME | REMARKS |
| Υ | tt (min) | |
| 0) | (21) | (22) |
| | | |
| | | |
| | | |
| | | |
| | | |
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|-----------------------|----------------|-----------------|-----------------|----------|-----------|
| PROJECT NAME: | Berkely Center | Subdivision | | DATE: | 3/29/2024 |
| PROJECT NUMBER: | 096888037 | | | | |
| CALCULATED BY: | AIA | | | | |
| CHECKED BY: | JPW | | | | |
| | EXISTIN | G RATIONAL CALC | ULATIONS SUMMAR | Y | |
| DESIGN POINT | TRIBUTARY | TRIBUTARY AREA | IMPERVIOUSNESS | PEAK FLO | WS (CFS) |
| DESIGN POINT | BASINS | (AC) | % | Q5 | Q100 |
| On-Site Basins | | | | | |
| | EX-1 | 7.29 | 98% | 24.48 | 50.47 |
| 1 | EX-2 | 0.28 | 100% | 1.12 | 2.30 |
| 2 | EX-3 | 0.07 | 100% | 0.27 | 0.55 |
| 2 | EX-4 | 0.05 | 2% | 0.00 | 0.21 |

Kimley **»Horn**

STANDARD FORM SF-1 PROPOSED RUNOFF COEFFICIENTS - IMPERVIOUS CALCULATION

| PROJECT NAME PROJECT NUMBER CALCULATED BY CHECKED BY | AIA | livision | | | | | | | | | DATE: | 8/1/2024 | |
|---|-----------------|-----------|------|---------|----------|----------|------------|-------|------|------|-------|----------|-------|
| SOIL: Hydrologic So | | | | | | | | | | | | | |
| | | LANDSCAPE | ROOF | ASPHALT | CONCRETE | BUSINESS | INDUSTRIAL | | | | | | |
| | LAND USE: | AREA | AREA | ASPHALI | AREA | SUBURBAN | LIGHT | | | | | | |
| | 2-YEAR COEFF. | 0.01 | 0.79 | 0.83 | 0.79 | 0.79 | 0.79 | | | | | | |
| | 5-YEAR COEFF. | 0.05 | 0.81 | 0.85 | 0.81 | 0.81 | 0.81 | | | | | | |
| | 10-YEAR COEFF. | 0.15 | 0.83 | 0.87 | 0.83 | 0.83 | 0.83 | | | | | | |
| | 100-YEAR COEFF. | 0.49 | 0.87 | 0.89 | 0.87 | 0.87 | 0.87 | | | | | | |
| | IMPERVIOUS % | 2% | 90% | 100% | 90% | 75% | 80% | | | | | | |
| | | LANDSCAPE | ROOF | ASPHALT | CONCRETE | BUSINESS | INDUSTRIAL | TOTAL | | | | | |
| DESIGN | DESIGN | AREA | AREA | AREA | AREA | AREA | AREA | AREA | | | | | |
| BASIN | POINT | (AC) | (AC) | (AC) | (AC) | (AC) | (AC) | (AC) | C(2) | C(5) | C(10) | C(100) | Imp % |
| On-Site Basins | | | | | | | | | | | | | |
| A1 | С | 0.00 | 0.00 | 0.00 | 0.00 | 0.89 | 0.00 | 0.89 | 0.75 | 0.75 | 0.75 | 0.75 | 75% |
| B1 | С | 0.00 | 0.00 | 0.00 | 0.00 | 1.12 | 0.00 | 1.12 | 0.75 | 0.75 | 0.75 | 0.75 | 75% |
| C1 | С | 0.00 | 0.00 | 0.00 | 0.00 | 2.04 | 0.00 | 2.04 | 0.75 | 0.75 | 0.75 | 0.75 | 75% |
| D1 | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.37 | 2.37 | 0.80 | 0.80 | 0.80 | 0.80 | 80% |
| E1 | | 0.76 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.76 | 0.01 | 0.05 | 0.15 | 0.49 | 2% |
| OF-E1 | | 0.10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.10 | 0.01 | 0.05 | 0.15 | 0.49 | 2% |
| OF-AB1 | | 0.09 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.12 | 0.20 | 0.24 | 0.32 | 0.58 | 24% |
| | | 0.95 | 0.00 | 0.00 | 0.03 | 4.05 | 2.37 | 7.41 | 0.67 | 0.68 | 0.69 | 0.73 | 67% |
| BASIN SUBTOTAL | | 13% | 0% | 0% | 0% | 55% | 32% | 1.00 | | | | | |
| Off-Site Basins | | | | | | | | | | | | | |
| OS-C1 | | 0.04 | 0.00 | 0.00 | 0.07 | 0.00 | 0.00 | 0.10 | 0.51 | 0.54 | 0.27 | 0.73 | 58% |
| OF-AB2 | | 0.02 | 0.00 | 0.00 | 0.08 | 0.00 | 0.00 | 0.10 | 0.62 | 0.65 | 0.25 | 0.79 | 71% |
| OS-D1 | | 0.05 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0.06 | 0.13 | 0.17 | 0.41 | 0.55 | 16% |
| | | 0.11 | 0.00 | 0.00 | 0.16 | 0.00 | 0.00 | 0.26 | 0.47 | 0.50 | 0.74 | 0.71 | 54% |
| BASIN SUBTOTAL | | 41% | 0% | 0% | 59% | 0% | 0% | 100% | | | | | |

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|--|--------------------------------|--|---------------------|-----------------------|-------------------------------|---|-------------------|-------------------------|-----------------------|--------------------------------|---------------------|-------------------------|------------------------|-----------------------|--------------------|------------|
| PROJECT N CALCULA | ATED BY: | Berkely Cent 0968888037 AIA JPW | er Subdivision | | | | | | | | | | | | DATE | : 8/1/2024 |
| SUB-BA | SIN | | I | NITIAL | | | TRA | VEL TIM | E | | | | Te CHEC | K | | FINAL |
| DAT | A | | Т | IME (T _i) | | | | (\mathbf{T}_{t}) | | | | (UF | BANIZED | BASINS) | | Tc |
| DESIGN BASIN (1) | AREA Ac (2) | C5 (3) | LENGTH Ft (4) | SLOPE % (5) | T _i Min. (6) | LENGTH Ft. (7) | SLOPE % (8) | C _v (9) | VEL fps (11) | T _t Min. (12) | COMP. tc (13) | TOTAL LENGTH (14) | TOTAL SLOPE (15) | TOTAL IMP. (16) | Tc Min. (17) | Min. |
| On-Site Basins | 0.89 | 0.75 | 250 | 2.0% | 8.1 | 175 | 0.5% | 20.0 | 1.4 | 2.1 | 10.1 | 425 | 1.4% | 75% | 16.3 | 10.1 |
| A1 B1 | 1.12 | 0.75 | 230 | 2.0% | 8.4 | 230 | 0.5% | 20.0 | 1.4 | 2.1 | 10.1 | 423 505 | 1.4% | 75% | 10.3 | 10.1 |
| C1 | 2.04 | 0.75 | 300 | 2.0% | 8.8 | 50 | 0.5% | 22.0 | 1.5 | 0.5 | 9.4 | 350 | 1.8% | 75% | 17.0 | 9.4 |
| D1 | 2.37 | 0.80 | 300 | 2.0% | 7.6 | 00 | 50.0% | 23.0 | 16.3 | 0.0 | 7.6 | 300 | 2.0% | 80% | 14.2 | 7.6 |
| E1 | 0.76 | 0.05 | 75 | 5.0% | 9.7 | 200 | 0.5% | 24.0 | 1.7 | 2.0 | 11.7 | 275 | 1.7% | 2% | 29.4 | 11.7 |
| OF-E1 | 0.10 | 0.05 | 5 | 2.0% | 3.4 | | 50.0% | 25.0 | 17.7 | | 3.4 | 5 | 2.0% | 2% | 25.7 | 5.0 |
| OF-AB1 | 0.12 | 0.24 | 10 | 2.0% | 4.0 | | 50.0% | 26.0 | 18.4 | | 4.0 | 10 | 2.0% | 24% | 22.0 | 5.0 |
| Off-Site Basins | | | | | | | | | | | | | | | | |
| OS-C1 | 0.10 | 0.54 | 10 | 2.0% | 2.6 | | 2.0% | 15.0 | 2.1 | | 2.6 | 10 | 2.0% | 58% | 16.2 | 5.0 |
| OF-AB2 | 0.10 | 0.65 | 10 | 102.0% | 0.6 | | 2.0% | 16.0 | 2.3 | | 0.6 | 10 | 102.0% | 71% | 13.9 | 5.0 |
| OS-D1 | 0.06 | 0.17 | 10 | 202.0% | 0.9 | | 2.0% | 17.0 | 2.4 | | 0.9 | 10 | 202.0% | 16% | 23.3 | 5.0 |
| $t_i = \frac{0.395}{1000000000000000000000000000000000000$ | $\frac{(1.1-C_5)}{S_o^{0.33}}$ | $\sqrt{L_i}$ | | $t_i = \frac{1}{60}$ | L_t | $\frac{1}{e^{0}} = \frac{L_{t}}{60V_{t}}$ | s - 11 | $t_{c} = (26 - 1)^{-1}$ | $17i) + \frac{1}{60}$ | $\frac{L_t}{14i+9}$ | $\sqrt{S_i}$ | | | | | |

STANDARD FORM SF-3 PROPOSED STORM DRAINAGE DESIGN - RATIONAL METHOD X YEAR EVENT

PROJECT NAME: Berkely Center Subdivision

 P_1 (1-Hour Rainfall) = 1.42

DATE: 8/1/2

PROJECT NUMBER: 0968888037

CALCULATED BY: AIA CHECKED BY: JPW

| | | DIRECT RUNOFF | | | | | | | | TOTAL | RUNC |)FF | STREET | | PIPE | | | TRAVEL 7 | |
|----------------|-----------------|-----------------|--------------|-----------------|----------|---------|--------------|------------|---------|----------------|--------------|------------|-----------|--------------------|-------------------------|-----------|-------------------|----------------|--------------|
| STORM LINE | DESIGN POINT | DESIGN BASIN | AREA (AC) | RUNOFF COEFF | tc (min) | C*A(ac) | I (in/hr) | Q (cfs) | tc(max) | S(C*A) (ac) | I (in/hr) | Q (cfs) | SLOPE (%) | STREET FLOW(cfs | DESIGN FLOW(cfs) | SLOPE (%) | PIPE SIZE (in) | LENGTH (ft) | VELOCIT V |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | (18) | (19) | (20) |
| On-Site Basins | | | | | | | | | | | | | | | | | | | |

| | | A1 | 0.89 | 0.75 | 10.12 | 0.67 | 3.82 | 2.55 | | | | | | |
|-------------|------|--------|------|------|-------|------|------|------|--|--|--|--|--|--|
| | | B1 | 1.12 | 0.75 | 11.03 | 0.84 | 3.69 | 3.10 | | | | | | |
| | | C1 | 2.04 | 0.75 | 9.36 | 1.53 | 3.94 | 6.03 | | | | | | |
| | | D1 | 2.37 | 0.80 | 7.56 | 1.90 | 4.26 | 8.07 | | | | | | |
| | | E1 | 0.76 | 0.01 | 11.71 | 0.01 | 3.60 | 0.03 | | | | | | |
| | | OF-E1 | 0.10 | 0.01 | 5.00 | 0.00 | 4.82 | 0.00 | | | | | | |
| | | OF-AB1 | 0.12 | 0.20 | 5.00 | 0.02 | 4.82 | 0.12 | | | | | | |
| Off-Site Ba | sins | | | | | | | | | | | | | |
| | | OS-C1 | 0.10 | 0.51 | 5.00 | 0.05 | 4.82 | 0.25 | | | | | | |
| | | OF-AB2 | 0.10 | 0.62 | 5.00 | 0.06 | 4.82 | 0.31 | | | | | | |
| | | OS-D1 | 0.06 | 0.13 | 5.00 | 0.01 | 4.82 | 0.04 | | | | | | |

Kimley **»Horn**

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|------|-------------|---------|
| TI | ME | REMARKS |
| Υ | tt (min) | |
| 20) | (21) | (22) |
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STANDARD FORM SF-3 PROPOSED STORM DRAINAGE DESIGN - RATIONAL METHOD 100 YEAR EVENT

PROJECT NAME: Berkely Center Subdivision

 P_1 (1-Hour Rainfall) = 2.71

PROJECT NUMBER: 0968888037

Kimley **»Horn**

| | | | DIRECT RUNOFF | | | | | | | ГОТАL | RUN | OFF | STREET | | PIPE | | TRAV | |
|---------------|----------------|-----------------|---------------|-----------------|----------|---------|--------------|------------|---------|----------------|--------------|------------|--------------|--------------------|-------------------------|--------------|-------------------|--------------|
| STORM LINE | POINT POINT | DESIGN BASIN | AREA (AC) | RUNOFF COEFF | tc (min) | C*A(ac) | I (in/hr) | Q (cfs) | tc(max) | S(C*A) (ac) | I (in/hr) | Q (cfs) | (%) SLOPE | STREET FLOW(cfs | DESIGN FLOW(cfs) | SLOPE (%) | PIPE SIZE (in) | (ft) (ft) |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | (18) | (19) |

| CALCULATED CHECKED | BY: AIA | | | | | | | | r ₁ (1-n | our Kain | 11 an) ₌ | 2.11 | | | | | | | | | |
|--------------------|---------|-----------------|--------------|-----------------|----------|---------|--------------|------------|------------------------------------|----------------|---------------------|------------|--------------|--------------------|--------------------|-----------|-------------------|----------------|--------------|-------------|---------|
| | | | | D | IRECT | RUNOF | FF | |] | TOTAL | RUN |)FF | STR | EET | | PIPE | | TRAV | EL TI | ME | REMARKS |
| STORM LINE | DESIGN | DESIGN BASIN | AREA (AC) | RUNOFF COEFF | tc (min) | C*A(ac) | I (in/hr) | Q (cfs) | tc(max) | S(C*A) (ac) | I (in/hr) | Q (cfs) | SLOPE (%) | STREET FLOW(cfs | DESIGN FLOW(cfs | SLOPE (%) | PIPE SIZE (in) | LENGTH (ft) | VELOCIT Y | tt (min) | |
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) | (17) | (18) | (19) | (20) | (21) | (22) |
| On-Site Basins | | A 1 | 0.89 | 0.75 | 10.12 | 0.67 | 7.30 | 4.87 | | | | | <u>г</u> | | | | | | | 1 | |
| | | A1 B1 | 1.12 | 0.75 | 11.03 | 0.84 | 7.05 | 4.87 | | | | | | | | | | | | | |
| | | C1 | 2.04 | 0.75 | 9.36 | 1.53 | 7.52 | 11.51 | | | | | | | | | | | | | |
| | | D1 | 2.37 | 0.80 | 7.56 | 1.90 | 8.12 | 15.40 | | | | | | | | | | | | | |
| | | E1 | 0.76 | 0.49 | 11.71 | 0.37 | 6.87 | 2.56 | | | | | | | | | | | | | |
| | | OF-E1 | 0.10 | 0.49 | 5.00 | 0.05 | 9.19 | 0.46 | | | | | | | | | | | | | |
| | | OF-AB1 | 0.12 | 0.58 | 5.00 | 0.07 | 9.19 | 0.65 | | | | | | | | | | | | | |
| Off-Site Basins | | | | | | | | | | | | | | | | | | | | | |
| | | OS-C1 | 0.10 | 0.73 | 5.00 | 0.08 | 9.19 | 0.69 | | | | | | | | | | | | | |
| | | OF-AB2 | 0.10 | 0.79 | 5.00 | 0.08 | 9.19 | 0.75 | | | | | | | | | | | | | |
| | | OS-D1 | 0.06 | 0.55 | 5.00 | 0.03 | 9.19 | 0.29 | | | | | | | | | | | | | |

DATE: 8/1/2024

| Kimley | orn | | | | |
|----------------------------------|------------------------------|----------------|-----------------|----------|----------|
| PROJECT NAME: PROJECT NUMBER: | Berkely Center 0968888037 | Subdivision | | DATE: | 8/1/2024 |
| CALCULATED BY: CHECKED BY: | | | | | |
| CHECKED D1. | | | CULATIONS SUMMA | DV | |
| | | | | PEAK FLO | |
| DESIGN POINT | TRIBUTARY | TRIBUTARY AREA | IMPERVIOUSNESS | PEAK FLU | WS (CFS) |
| DESIGN FOINT | BASINS | (AC) | % | Q5 | Q100 |
| On-Site Basins | | | | | |
| | A1 | 0.89 | 75% | 2.55 | 4.87 |
| | B1 | 1.12 | 75% | 3.10 | 5.92 |
| | C1 | 2.04 | 75% | 6.03 | 11.51 |
| | D1 | 2.37 | 80% | 8.07 | 15.40 |
| | E1 | 0.76 | 2% | 0.03 | 2.56 |
| | OF-E1 | 0.10 | 2% | 0.00 | 0.46 |
| | OF-AB1 | 0.12 | 24% | 0.12 | 0.65 |
| TOTAL | - | 7.41 | 67% | 19.90 | 41.37 |
| Off-Site Basins | | | | | |
| OS-C1 | OS-C1 | 0.10 | 58% | 0.25 | 0.69 |
| OF-AB2 | OF-AB2 | 0.10 | 71% | 0.31 | 0.75 |
| OS-D1 | OS-D1 | 0.06 | 16% | 0.04 | 0.29 |
| TOTAL | | 0.26 | 54% | 0.60 | 1.74 |



APPENDIX D – HYDRAULICS

DETENTION BASIN STAGE-STORAGE TABLE BUILDER

| A |
|---|
| |

Example Zone Configuration (Retention Pond)

Depth Increment = 0.20 ft

| Watershed | Information | |
|-----------|-------------|--|
| | | |

| atersned information | | |
|---|------------|---------|
| Selected BMP Type = | EDB | |
| Watershed Area = | 7.34 | acres |
| Watershed Length = | 1,000 | ft |
| Watershed Length to Centroid = | 630 | ft |
| Watershed Slope = | 0.015 | ft/ft |
| Watershed Imperviousness = | 67.00% | percent |
| Percentage Hydrologic Soil Group A = | 2.0% | percent |
| Percentage Hydrologic Soil Group B = | 36.0% | percent |
| Percentage Hydrologic Soil Groups C/D = | 62.0% | percent |
| Target WQCV Drain Time = | 40.0 | hours |
| Location for 1-hr Rainfall Depths = | User Input | |
| | | |

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

| the embedded Colorado orban Hydro | gi apri Procedu | ie. |
|--|-----------------|-----------|
| Water Quality Capture Volume (WQCV) = | 0.160 | acre-feet |
| Excess Urban Runoff Volume (EURV) = | 0.501 | acre-feet |
| 2-yr Runoff Volume (P1 = 1 in.) = | 0.391 | acre-feet |
| 5-yr Runoff Volume (P1 = 1.42 in.) = | 0.631 | acre-feet |
| 10-yr Runoff Volume (P1 = 1.68 in.) = | 0.788 | acre-feet |
| 25-yr Runoff Volume (P1 = 1.69 in.) = | 0.813 | acre-feet |
| 50-yr Runoff Volume (P1 = 2.35 in.) = | 1.227 | acre-feet |
| 100-yr Runoff Volume (P1 = 2.71 in.) = | 1.473 | acre-feet |
| 500-yr Runoff Volume (P1 = 3.14 in.) = | 1.751 | acre-feet |
| Approximate 2-yr Detention Volume = | 0.356 | acre-feet |
| Approximate 5-yr Detention Volume = | 0.553 | acre-feet |
| Approximate 10-yr Detention Volume = | 0.667 | acre-feet |
| Approximate 25-yr Detention Volume = | 0.629 | acre-feet |
| Approximate 50-yr Detention Volume = | 0.805 | acre-feet |
| Approximate 100-yr Detention Volume = | 0.898 | acre-feet |
| | | |

| Define | Zones | and | Basin | Geome | etry |
|--------|-------|-----|--------|--------|------|
| | | i | Zone 1 | Volume | (WC |

| Jerine Zones and Basin Geometry | | |
|---|-------|-----------------|
| Zone 1 Volume (WQCV) = | 0.160 | acre-feet |
| Zone 2 Volume (EURV - Zone 1) = | 0.341 | acre-feet |
| Zone 3 Volume (100-year - Zones 1 & 2) = | 0.396 | acre-feet |
| Total Detention Basin Volume = | 0.898 | acre-feet |
| Initial Surcharge Volume (ISV) = | 6 | ft ³ |
| Initial Surcharge Depth (ISD) = | 0.50 | ft |
| Total Available Detention Depth (H _{total}) = | 3.00 | ft |
| Depth of Trickle Channel (H _{TC}) = | 0.50 | ft |
| Slope of Trickle Channel (S _{TC}) = | 0.002 | ft/ft |
| Slopes of Main Basin Sides (Smain) = | 4 | H:V |
| Basin Length-to-Width Ratio (R _{L/W}) = | 4.5 | |
| | | |

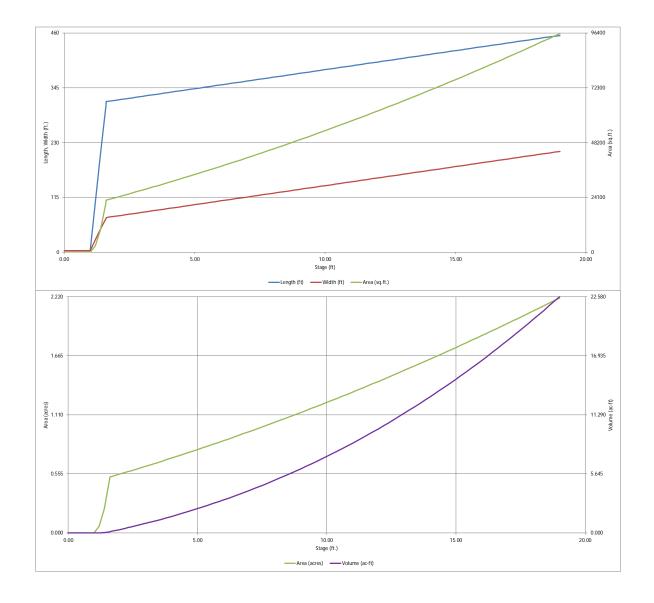
| Initial Surcharge Area (A _{ISV}) = | 12 | ft ² |
|--|--------|-----------------|
| Surcharge Volume Length (L_{ISV}) = | 3.5 | ft |
| Surcharge Volume Width (W_{ISV}) = | 3.5 | ft |
| Depth of Basin Floor (H_{FLOOR}) = | 0.62 | ft |
| Length of Basin Floor $(L_{FLOOR}) =$ | 315.9 | ft |
| Width of Basin Floor (W_{FLOOR}) = | | ft |
| Area of Basin Floor (A _{FLOOR}) = | | ft ² |
| Volume of Basin Floor (V_{FLOOR}) = | 4,835 | ft ³ |
| Depth of Main Basin $(H_{MAIN}) =$ | 1.38 | ft |
| Length of Main Basin $(L_{MAIN}) =$ | 327.0 | ft |
| Width of Main Basin (W_{MAIN}) = | 83.4 | ft |
| Area of Main Basin (A _{MAIN}) = | 27,268 | ft ² |
| Volume of Main Basin (V _{MAIN}) = | 34,543 | ft ³ |

Calculated Total Basin Volume (V_{total}) = 0.904 acre-feet

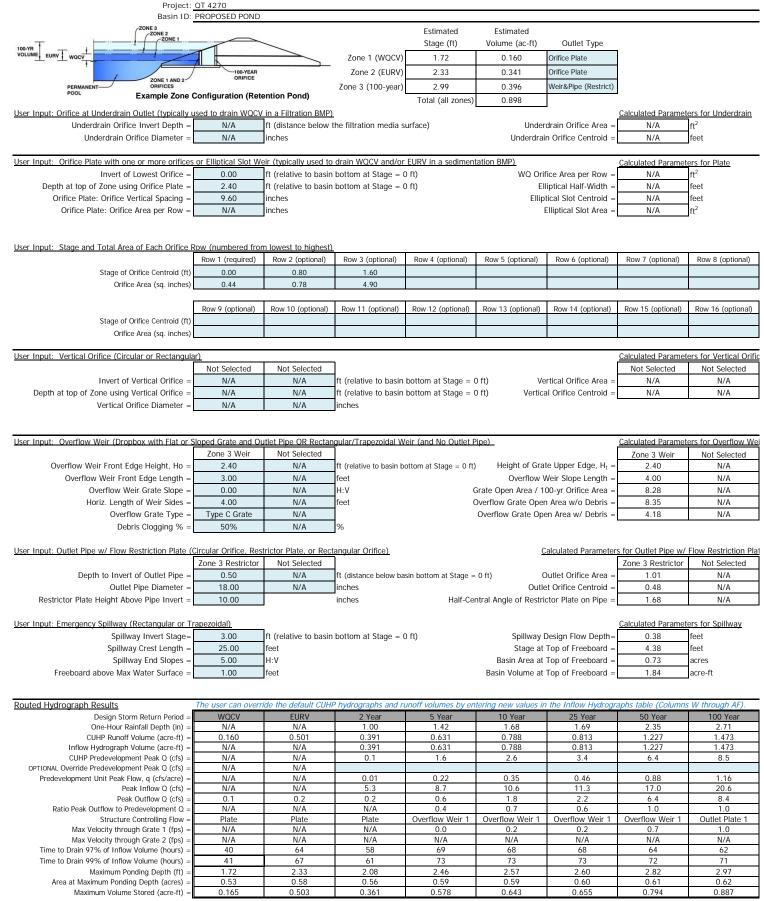
| E Contraction of the second seco | | | Optional | | | | Optional | | | |
|--|-------------------|----------------|------------|----------------|----------------|--------------------------|-------------------------|-------------|--------------------|------------------|
| ntion Pond) | Stage - Storage | Stage | Override | Length | Width | Area | Override | Area | Volume | Volume |
| | Description | (ft) | Stage (ft) | (ft) | (ft) 3.5 | (ft ²) 12 | Area (ft ²) | (acre) | (ft 3) | (ac-ft) |
| | Top of Micropool | 0.00 | | 3.5 | | | | 0.000 | | |
| | ISV | 0.50 | | 3.5 | 3.5 | 12 | | 0.000 | 6 | 0.000 |
| | | 0.60 | | 3.5 | 3.5 | 12 | | 0.000 | 7 | 0.000 |
| | | 0.80 | | 3.5 | 3.5 | 12 | | 0.000 | 10 | 0.000 |
| | | 1.00 | | 3.5 | 3.5 | 12 | | 0.000 | 12 | 0.000 |
| | | | | 104.3 | 25.7 | | | 0.061 | 206 | 0.005 |
| | | 1.20 | | | 47.9 | 2,678 | | | | |
| | | 1.40 | | 205.1 | | 9,824 | | 0.226 | 1,382 | 0.032 |
| | | 1.60 | | 305.9 | 70.1 | 21,450 | | 0.492 | 4,435 | 0.102 |
| | Floor | 1.62 | | 315.9 | 72.4 | 22,860 | | 0.525 | 4,878 | 0.112 |
| | Zone 1 (WQCV) | 1.72 | | 316.7 | 73.2 | 23,171 | | 0.532 | 7,179 | 0.165 |
| | | 1.80 | | 317.4 | 73.8 | 23,421 | | 0.538 | 9,043 | 0.208 |
| | | 2.00 | | 319.0 | 75.4 | 24,049 | | 0.552 | 13,790 | 0.317 |
| | | 2.20 | | 320.6 | 77.0 | 24,683 | | 0.567 | 18,663 | 0.428 |
| | Zone 2 (EURV) | 2.33 | | 321.6 | 78.0 | 25,097 | | 0.576 | 21,899 | 0.503 |
| Optional User Overrides | | 2.40 | | 322.2 | 78.6 | 25,321 | | 0.581 | 23,663 | 0.543 |
| acre-feet | | 2.60 | | 323.8 | 80.2 | 25,965 | | 0.596 | 28,792 | 0.661 |
| | | | | | | | | | | |
| acre-feet | 7 0 (100) | 2.80 | | 325.4 | 81.8 | 26,614 | | 0.611 | 34,050 | 0.782 |
| | Zone 3 (100-year) | 2.99 | | 326.9 | 83.3 | 27,235 | | 0.625 | 39,165 | 0.899 |
| 1.42 inches | | 3.00 | | 327.0 | 83.4 | 27,268 | | 0.626 | 39,438 | 0.905 |
| 1.68 inches | | 3.20 | | 328.6 | 85.0 | 27,927 | | 0.641 | 44,957 | 1.032 |
| inches | | 3.40 | | 330.2 | 86.6 | 28,592 | | 0.656 | 50,609 | 1.162 |
| 2.35 inches | | 3.60 | | 331.8 | 88.2 | 29,261 | | 0.672 | 56,394 | 1.295 |
| 2.71 inches | 1 | 3.80 | | 333.4 | 89.8 | 29,936 | | 0.687 | 62,314 | 1.431 |
| inches | | 4.00 | | 335.0 | 91.4 | 30,615 | | 0.703 | 68,369 | 1.570 |
| L | 1 | 4.20 | | 336.6 | 93.0 | 31,300 | | 0.719 | 74,560 | 1.712 |
| | 1 | 4.40 | | 338.2 | 94.6 | 31,990 | | 0.734 | 80,889 | 1.857 |
| | <u> </u> | 4.40 | | 339.8 | 94.0 | 32,685 | | 0.750 | 87,357 | 2.005 |
| | | 4.60 | | | | 32,085 | | | | |
| | | | | 341.4 | 97.8 | | | 0.766 | 93,963 | 2.157 |
| | | 5.00 | | 343.0 | 99.4 | 34,090 | | 0.783 | 100,711 | 2.312 |
| | | 5.20 | | 344.6 | 101.0 | 34,801 | | 0.799 | 107,600 | 2.470 |
| | | 5.40 | | 346.2 | 102.6 | 35,516 | | 0.815 | 114,631 | 2.632 |
| | 1 | 5.60 | | 347.8 | 104.2 | 36,237 | | 0.832 | 121,807 | 2.796 |
| | | 5.80 | | 349.4 | 105.8 | 36,962 | | 0.849 | 129,126 | 2.964 |
| | | 6.00 | | 351.0 | 107.4 | 37,693 | | 0.865 | 136,592 | 3.136 |
| | | 6.20 | | 352.6 | 109.0 | 38,429 | | 0.882 | 144,204 | 3.310 |
| | | 6.40 | | 354.2 | 110.6 | 39,170 | | 0.899 | 151,964 | 3.489 |
| | | | | | | | | | | |
| | | 6.60 | | 355.8 | 112.2 | 39,916 | | 0.916 | 159,873 | 3.670 |
| | | 6.80 | | 357.4 | 113.8 | 40,668 | | 0.934 | 167,931 | 3.855 |
| | | 7.00 | | 359.0 | 115.4 | 41,424 | | 0.951 | 176,140 | 4.044 |
| | | 7.20 | | 360.6 | 117.0 | 42,186 | | 0.968 | 184,501 | 4.236 |
| | | 7.40 | | 362.2 | 118.6 | 42,952 | | 0.986 | 193,015 | 4.431 |
| | | 7.60 | | 363.8 | 120.2 | 43,724 | | 1.004 | 201,682 | 4.630 |
| | | 7.80 | | 365.4 | 121.8 | 44,501 | | 1.022 | 210,505 | 4.833 |
| | | 8.00 | | 367.0 | 123.4 | 45,283 | | 1.040 | 219,483 | 5.039 |
| | | 8.20 | | 368.6 | 125.0 | 46,070 | | 1.058 | 228,618 | 5.248 |
| | | | | | | | | | | |
| | | 8.40 | | 370.2 | 126.6 | 46,863 | | 1.076 | 237,912 | 5.462 |
| | | 8.60 | | 371.8 | 128.2 | 47,660 | | 1.094 | 247,364 | 5.679 |
| | | 8.80 | | 373.4 | 129.8 | 48,463 | | 1.113 | 256,976 | 5.899 |
| | | 9.00 | | 375.0 | 131.4 | 49,270 | | 1.131 | 266,749 | 6.124 |
| | | 9.20 | | 376.6 | 133.0 | 50,083 | | 1.150 | 276,684 | 6.352 |
| | | 9.40 | | 378.2 | 134.6 | 50,901 | | 1.169 | 286,783 | 6.584 |
| | | 9.60 | | 379.8 | 136.2 | 51,724 | | 1.187 | 297,045 | 6.819 |
| | | 9.80 | | 381.4 | 137.8 | 52,552 | | 1.206 | 307,473 | 7.059 |
| | | 10.00 | | 383.0 | 139.4 | 53,385 | | 1.226 | 318,066 | 7.302 |
| | | | | | 141.0 | | | | | |
| | | 10.20 | | 384.6 | | 54,224 | | 1.245 | 328,827 | 7.549 |
| | L | 10.40 | | 386.2 | 142.6 | 55,067 | | 1.264 | 339,756 | 7.800 |
| | | 10.60 | | 387.8 | 144.2 | 55,916 | | 1.284 | 350,854 | 8.055 |
| | L | 10.80 | | 389.4 | 145.8 | 56,769 | | 1.303 | 362,123 | 8.313 |
| | L | 11.00 | _ | 391.0 | 147.4 | 57,628 | _ | 1.323 | 373,562 | 8.576 |
| | | 11.20 11.40 | | 392.6 394.2 | 149.0 150.6 | 58,492 59,361 | | 1.343 | 385,174 396,960 | 8.842 9.113 |
| | | 11.40 | | 394.2 | 150.6 | 60,236 | | 1.303 | 408,919 | 9.113 |
| | | 11.80 | | 397.4 | 153.8 | 61,115 | | 1.403 | 421,054 | 9.666 |
| | | 12.00 | | 399.0 400.6 | 155.4 157.0 | 61,999 62,889 | | 1.423 | 433,366 445,854 | 9.949 10.235 |
| | | 12.20 | | 400.6 | 157.0 | 62,889 | | 1.444 | 445,854 458,522 | 10.235 |
| | | 12.60 | | 403.8 | 160.2 | 64,683 | | 1.485 | 471,368 | 10.821 |
| | | 12.80 | | 405.4 | 161.8 | 65,588 | | 1.506 | 484,395 | 11.120 |
| | | 13.00 | | 407.0 408.6 | 163.4 165.0 | 66,498 67,414 | | 1.527 | 497,604 510,995 | 11.423 11.731 |
| | 1 | 13.20 | | 408.6 | 165.0 | 67,414 68,334 | | 1.548 | 510,995 | 11.731 12.042 |
| | | 13.60 | | 411.8 | 168.2 | 69,259 | | 1.590 | 538,329 | 12.358 |
| | L | 13.80 | | 413.4 | 169.8 | 70,190 | | 1.611 | 552,274 | 12.678 |
| | | 14.00 14.20 | | 415.0 416.6 | 171.4 173.0 | 71,125 72,066 | | 1.633 | 566,405 580,724 | 13.003 13.332 |
| | | 14.20 | | 418.2 | 173.0 | 73,012 | | 1.676 | 595,232 | 13.332 |
| | | 14.60 | | 419.8 | 176.2 | 73,963 | | 1.698 | 609,929 | 14.002 |
| | | 14.80 | | 421.4 423.0 | 177.8 | 74,919 | | 1.720 | 624,817 | 14.344 |
| | | 15.00 | | 423.0 424.6 | 179.4 181.0 | 75,880 76,847 | | 1.742 | 639,897 655,170 | 14.690 15.041 |
| | 1 | 15.40 | | 426.2 | 182.6 | 77,818 | | 1.786 | 670,636 | 15.396 |
| | | 15.60 | | 427.8 | 184.2 | 78,795 | | 1.809 | 686,297 | 15.755 |
| | L | 15.80 | | 429.4 | 185.8 | 79,777 | | 1.831 | 702,155 | 16.119 |
| | | 16.00 16.20 | | 431.0 432.6 | 187.4 189.0 | 80,763 81,755 | | 1.854 | 718,208 | 16.488 16.861 |
| | | 16.20 | | 432.6 | 189.0 | 81,755 82,752 | | 1.877 | 734,460 750,911 | 16.861 |
| | L | 16.60 | | 435.8 | 192.2 | 83,755 | | 1.923 | 767,562 | 17.621 |
| | | 16.80 | | 437.4 | 193.8 | 84,762 | | 1.946 | 784,413 | 18.008 |
| | | 17.00 | | 439.0 440.6 | 195.4 197.0 | 85,774 86,792 | | 1.969 | 801,467 818,723 | 18.399 18.795 |
| | | 17.20 | | 440.6 | 197.0 | 86,792 87,815 | | 2.016 | 818,723 836,184 | 18.795 |
| | L | 17.60 | | 443.8 | 200.2 | 88,842 | | 2.040 | 853,849 | 19.602 |
| | | 17.80 | | 445.4 | 201.8 | 89,875 | | 2.063 | 871,721 | 20.012 |
| | | 18.00 | | 447.0 | 203.4 | 90,913 | | 2.087 | 889,800 | 20.427 |
| | | 18.20 | | 448.6 450.2 | 205.0 206.6 | 91,957 93.005 | | 2.111 2.135 | 908,087 926,583 | 20.847 21.271 |
| | | 18.60 | | 451.8 | 208.2 | 94,058 | | 2.159 | 945,289 | 21.701 |
| | | 18.80 | | 453.4 | 209.8 | 95,117 | | 2.184 | 964,207 | 22.135 |
| | L | 19.00 | | 455.0 | 211.4 | 96,180 | | 2.208 | 983,336 | 22.574 |

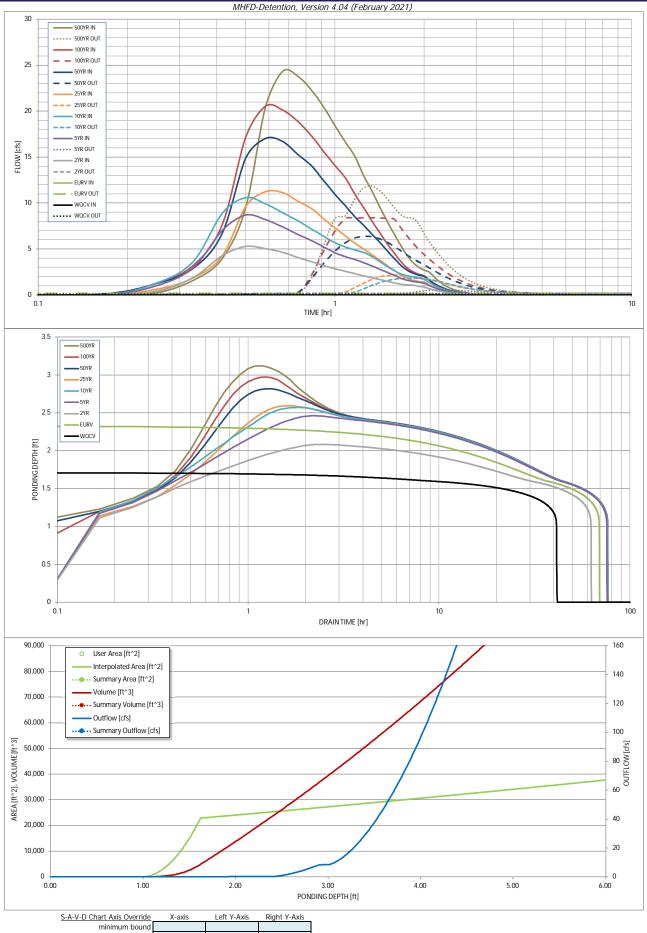
DETENTION BASIN STAGE-STORAGE TABLE BUILDER

MHFD-Detention, Version 4.04 (February 2021)



MHFD-Detention, Version 4.04 (February 2021,





maximum bound

Outflow Hydrograph Workbook Filename:

Inflow Hydrographs The user can override the calculated inflow hydrographs from this workbook with inflow hydrographs developed in a separate program

| | The user can ov | erride the calcul | ated inflow hydro | ographs from this | s workbook with | inflow hydrograp | ohs developed in | a separate progra | im. | |
|---------------|--------------------|-------------------|-------------------|-------------------|-----------------|------------------|------------------|-------------------|----------------|----------------|
| | SOURCE | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP | CUHP |
| Time Interval | TIME | WQCV [cfs] | EURV [cfs] | 2 Year [cfs] | 5 Year [cfs] | 10 Year [cfs] | 25 Year [cfs] | 50 Year [cfs] | 100 Year [cfs] | 500 Year [cfs] |
| 5.00 min | 0:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 0:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.12 | 0.08 | 0.25 |
| | 0:15:00 | 0.00 | 0.00 | 0.42 | 1.00 | 1.28 | 0.63 | 1.24 | 1.27 | 1.62 |
| | 0:20:00 | 0.00 | 0.00 | 1.91 | 2.99 | 3.67 | 1.87 | 2.92 | 3.23 | 3.97 |
| | 0:25:00 | 0.00 | 0.00 | 4.29 | 7.02 | 8.89 | 4.24 | 6.71 | 7.65 | 9.49 |
| | 0:30:00 | 0.00 | 0.00 | 5.29 | 8.69 | 10.59 | 9.61 | 14.86 | 17.13 | 20.45 |
| | 0:35:00 | 0.00 | 0.00 | 5.05 | 8.20 | 9.92 | 11.25 | 17.03 | 20.55 | 24.35 |
| | 0:40:00 | 0.00 | 0.00 | 4.64 | 7.40 | 8.96 | 11.13 | 16.70 | 20.12 | 23.79 |
| | 0:45:00 | 0.00 | 0.00 | 4.09 | 6.60 | 8.07 | 10.21 | 15.28 | 18.86 | 22.28 |
| | 0:50:00 | 0.00 | 0.00 | 3.62 | 5.93 | 7.18 | 9.40 | 14.06 | 17.32 | 20.45 |
| | 0:55:00 | 0.00 | 0.00 | 3.21 | 5.24 | 6.39 | 8.30 | 12.45 | 15.62 | 18.45 |
| | 1:00:00 | 0.00 | 0.00 | 2.85 | 4.61 | 5.70 | 7.30 | 10.96 | 14.09 | 16.64 |
| | 1:10:00 | 0.00 | 0.00 | 2.59 2.32 | 4.17 3.87 | 5.23 4.91 | 6.44 5.63 | 9.70 8.51 | 12.76 10.97 | 15.08 12.99 |
| | 1:15:00 | 0.00 | 0.00 | 2.09 | 3.53 | 4.63 | 5.01 | 7.59 | 9.52 | 11.30 |
| | 1:20:00 | 0.00 | 0.00 | 1.88 | 3.15 | 4.19 | 4.37 | 6.61 | 8.05 | 9.55 |
| | 1:25:00 | 0.00 | 0.00 | 1.69 | 2.80 | 3.63 | 3.80 | 5.72 | 6.74 | 7.99 |
| | 1:30:00 | 0.00 | 0.00 | 1.49 | 2.46 | 3.11 | 3.21 | 4.81 | 5.59 | 6.62 |
| | 1:35:00 | 0.00 | 0.00 | 1.31 | 2.16 | 2.66 | 2.67 | 3.98 | 4.55 | 5.39 |
| | 1:40:00 | 0.00 | 0.00 | 1.18 | 1.83 | 2.31 | 2.20 | 3.25 | 3.64 | 4.32 |
| | 1:45:00 | 0.00 | 0.00 | 1.11 | 1.61 | 2.11 | 1.83 | 2.70 | 2.95 | 3.51 |
| | 1:50:00 | 0.00 | 0.00 | 1.07 | 1.48 | 1.98 | 1.62 | 2.38 | 2.53 | 3.02 |
| | 1:55:00 | 0.00 | 0.00 | 0.96 | 1.38 | 1.86 | 1.48 | 2.17 | 2.26 | 2.70 |
| | 2:00:00 2:05:00 | 0.00 | 0.00 | 0.86 | 1.28 | 1.70 | 1.39 | 2.02 | 2.07 | 2.47 |
| | 2:05:00 | 0.00 | 0.00 | 0.68 | 1.02 0.79 | 1.35 1.05 | 1.10 0.85 | 1.60 | 1.61 | 1.92 1.45 |
| | 2:15:00 | 0.00 | 0.00 | 0.53 | 0.62 | 0.81 | 0.65 | 0.94 | 0.91 | 1.45 |
| | 2:20:00 | 0.00 | 0.00 | 0.42 | 0.02 | 0.62 | 0.50 | 0.74 | 0.69 | 0.82 |
| | 2:25:00 | 0.00 | 0.00 | 0.25 | 0.36 | 0.47 | 0.38 | 0.55 | 0.53 | 0.63 |
| | 2:30:00 | 0.00 | 0.00 | 0.19 | 0.27 | 0.35 | 0.29 | 0.41 | 0.40 | 0.47 |
| | 2:35:00 | 0.00 | 0.00 | 0.14 | 0.20 | 0.26 | 0.21 | 0.31 | 0.30 | 0.36 |
| | 2:40:00 | 0.00 | 0.00 | 0.11 | 0.15 | 0.20 | 0.16 | 0.23 | 0.23 | 0.27 |
| | 2:45:00 | 0.00 | 0.00 | 0.08 | 0.11 | 0.15 | 0.12 | 0.17 | 0.17 | 0.20 |
| | 2:50:00 | 0.00 | 0.00 | 0.05 | 0.07 | 0.10 | 0.09 | 0.12 | 0.12 | 0.14 |
| | 2:55:00 | 0.00 | 0.00 | 0.03 | 0.05 | 0.06 | 0.06 | 0.08 | 0.08 | 0.09 |
| | 3:00:00 | 0.00 | 0.00 | 0.02 | 0.03 | 0.04 | 0.03 | 0.05 | 0.05 | 0.05 |
| | 3:05:00 3:10:00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 | 0.02 | 0.03 |
| | 3:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 |
| | 3:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 3:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:05:00 4:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:15:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:30:00 4:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:40:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 4:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:05:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:10:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:15:00 5:20:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:25:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:30:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:35:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:40:00 5:45:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:50:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 5:55:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | 6:00:00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

MHFD-Detention, Version 4.04 (February 2021)

Summary Stage-Area-Volume-Discharge Relationships The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

| The user should graphically con | Stage | Area | Area | Volume | Volume | Total | ransition points. |
|---------------------------------|-------|--------------------|---------|--------------------|---------|------------------|--|
| Stage - Storage Description | [ft] | [ft ²] | [acres] | [ft ³] | [ac-ft] | Outflow [cfs] | |
| | | | | | | | For best results, include the |
| | | | | | | | stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on |
| | | | | | | | from the S-A-V table on Sheet 'Basin'. |
| | | | | | | | |
| | | | | | | | Also include the inverts of all outlets (e.g. vertical orifice, |
| | | | | | | | overflow grate, and spillway, where applicable). |
| | | | | | | | where applicable). |
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MHFD-Inlet, Version 5.03 (August 2023)

INLET MANAGEMENT

Worksheet Protected

| INLET NAME | Inlet A-4 | Inlet A-5 |
|------------------------------------|-------------------------|-------------------------|
| Site Type (Urban or Rural) | URBAN | URBAN |
| Inlet Application (Street or Area) | AREA | AREA |
| Hydraulic Condition | Swale | Swale |
| Inlet Type | CDOT Type C (Depressed) | CDOT Type C (Depressed) |

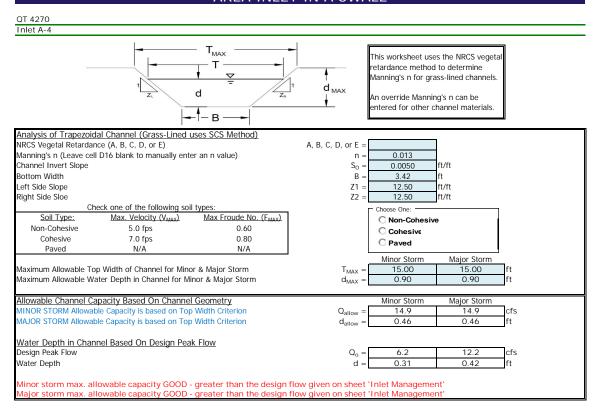
USER-DEFINED INPUT

| SER-DEFINED INPUT | | |
|--|-------------------------|--|
| User-Defined Design Flows | 1 | |
| Minor Q _{Known} (cfs) | 6.2 | 5.7 |
| Major Q _{Known} (cfs) | 12.2 | 10.8 |
| | | |
| Bypass (Carry-Over) Flow from Upstream | | eam (left) to downstream (right) in order fo |
| Receive Bypass Flow from: | No Bypass Flow Received | No Bypass Flow Received |
| Minor Bypass Flow Received, Q _b (cfs) | 0.0 | 0.0 |
| Major Bypass Flow Received, Q _b (cfs) | 0.0 | 0.0 |
| | | |
| Watershed Characteristics | | |
| Subcatchment Area (acres) | | |
| Percent Impervious | | |
| NRCS Soil Type | | |
| | | |
| Watershed Profile | | |
| Overland Slope (ft/ft) | | |
| Overland Length (ft) | | |
| Channel Slope (ft/ft) | | |
| Channel Length (ft) | | |
| | | |
| Minor Storm Rainfall Input | 1 | |
| Design Storm Return Period, T _r (years) | | |
| One-Hour Precipitation, P ₁ (inches) | | |
| C ₁ | | |
| C ₂ | | |
| C ₃ | | |
| User-defined C | | |
| User-defined 5-yr C ₅ | | |
| User-defined T _c | | |
| | | |
| Major Storm Rainfall Input | | |
| Design Storm Return Period, T _r (years) | | |
| One-Hour Precipitation, P ₁ (inches) | | |
| C ₁ | | |
| C ₂ | | |
| C ₃ | | |
| User-defined C | | |
| User-defined 5-yr C ₅ | | |
| User-defined T _c | | |

CALCULATED OUTPUT

| Minor Total Design Peak Flow, Q (cfs) | 6.2 | 5.7 |
|--|------|------|
| Major Total Design Peak Flow, Q (cfs) | 12.2 | 10.8 |
| Minor Flow Bypassed Downstream, Q _b (cfs) | 0.0 | 0.0 |
| Major Flow Bypassed Downstream, Qb (cfs) | 0.0 | 0.0 |

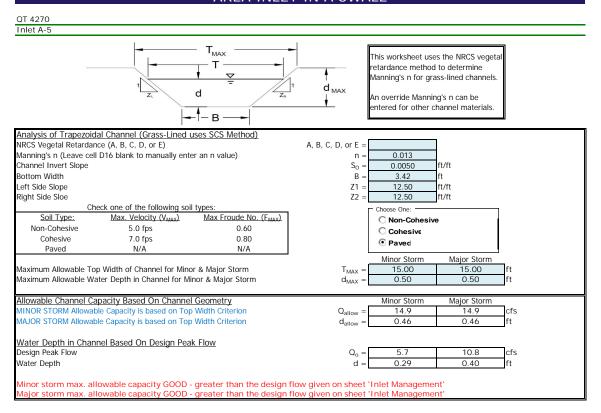
MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN <u>A SWALE</u>



MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN A SWALE

| QT 4270 Inlet A-4 | | | | |
|--|---|-------------------------------------|--|---------------------------|
| Inlet Design Information (Input) Type of Inlet CDOT Type C (Depresser 💌 | Inlet Type = | CDOT Type C (| Depressed) | |
| Angle of Inclined Grate (must be <= 30 degrees) Width of Grate Length of Grate Open Area Ratio Height of Inclined Grate Clogging Factor Grate Discharge Coefficient Orifice Coefficient Weir Coefficient | | | 0.00 3.00 3.00 0.70 0.00 0.50 0.84 0.56 1.81 | degrees ft ft ft |
| Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Total Inlet Interception Capacity (assumes clogged condition) Bypassed Flow Capture Percentage = Qa/Qo | $d = \bigcirc Q_a = \bigcirc Q_b = \bigcirc C\% = \bigcirc$ | MINOR 1.31 16.3 0.0 100 | MAJOR 1.42 17.0 0.0 100 | cfs cfs % |

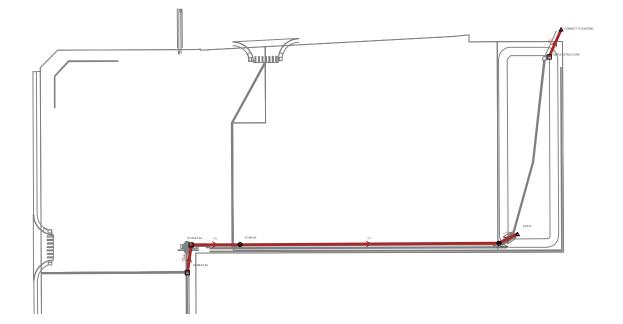
MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN <u>A SWALE</u>



MHFD-Inlet, Version 5.03 (August 2023) AREA INLET IN A SWALE

| QT 4270 Inlet A-5 | | | | |
|--|--|--|--|---------------------------|
| Inlet Design Information (Input) Type of Inlet CDOT Type C (Depresser 💌 | Inlet Type = | CDOT Type C (| Depressed) | |
| Angle of Inclined Grate (must be <= 30 degrees) Width of Grate Length of Grate Open Area Ratio Height of Inclined Grate Clogging Factor Grate Discharge Coefficient Orifice Coefficient Weir Coefficient | d d | $ \begin{array}{c} \theta = \\ W = \\ L = \\ A_{RATIO} = \\ H_{B} = \\ C_{r} = \\ C_{0} = \\ C_{0} = \\ C_{w} = \\ \end{array} $ | 0.00 3.00 0.70 0.00 0.50 0.84 0.56 1.81 | degrees ft ft ft |
| Water Depth at Inlet (for depressed inlets, 1 foot is added for depression) Total Inlet Interception Capacity (assumes clogged condition) Bypassed Flow Capture Percentage = Qa/Qo | $d = \begin{bmatrix} Q_a \\ Q_b \\ Q_b \\ C\% \end{bmatrix}$ | MINOR 1.29 16.2 0.0 100 | MAJOR 1.40 16.8 0.0 100 | cfs cfs % |

Berkley Center Subdivision Overall view



4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 1 of 13

5-Year Storm Event

Catch Basin Table - Time: 0.00 hours

| Label | Elevation (Rim) (ft) | Elevation (Invert) (ft) | Inlet Location | Headloss Coefficient (Standard) | Flow (Total Out) (cfs) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|----------------------------|-------------------------------|-------------------|---------------------------------------|------------------------------|--------------------------------------|--|
| ST INLET A4 | 5,214.79 | 5,211.38 | In Sag | 0.700 | 11.89 | 5,213.13 | 5,212.90 |
| OUTLET STRUCTURE | 5,210.00 | 5,208.50 | In Sag | 0.000 | 0.60 | 5,208.80 | 5,208.80 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 2 of 13

5-Year Storm Event

Conduit Table - Time: 0.00 hours

| Label | Material | Diameter (in) | Invert (Stop) (ft) | Length (Scaled) (ft) | Slope (Calculated) (ft/ft) | Velocity (ft/s) | Flow (cfs) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|-------|----------|------------------|-----------------------|----------------------------|----------------------------------|--------------------|---------------|--------------------------------------|--|
| P5 | PVC | 24.0 | 5,210.18 | 368.7 | 0.002 | 5.21 | 11.89 | 5,212.47 | 5,211.68 |
| P6 | PVC | 24.0 | 5,211.21 | 69.5 | 0.002 | 5.21 | 11.89 | 5,212.90 | 5,212.81 |
| P10 | PVC | 24.0 | 5,210.01 | 29.4 | 0.002 | 5.21 | 11.89 | 5,211.41 | 5,211.25 |
| P11 | PVC | 18.0 | 5,208.30 | 42.9 | 0.005 | 3.04 | 0.60 | 5,208.80 | 5,208.55 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 3 of 13

5-Year Storm Event

Manhole Table - Time: 0.00 hours

| Label | Elevation (Rim) (ft) | Elevation (Invert in 1) (ft) | Elevation (Invert) (ft) | Elevation (Invert Out) (ft) | Headloss Coefficient (Standard) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) |
|----------|-------------------------|------------------------------------|-------------------------------|-----------------------------------|---------------------------------------|------------------------------|---------------------|--|--------------------------------------|
| ST MH A3 | 5,215.38 | 5,211.21 | 5,211.11 | 5,211.11 | 0.800 | 11.89 | 1.36 | 5,212.47 | 5,212.81 |
| ST MH A2 | 5,213.34 | 5,210.18 | 5,210.08 | 5,210.08 | 0.600 | 11.89 | 1.33 | 5,211.41 | 5,211.68 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 4 of 13

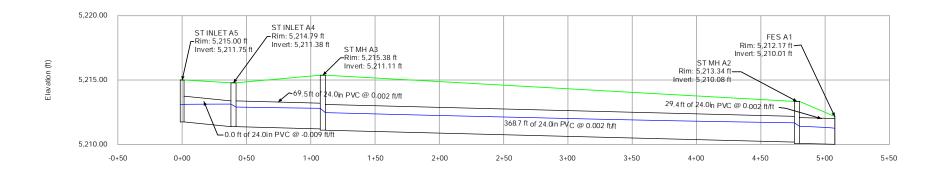
5-Year Storm Event

Outfall Table - Time: 0.00 hours

| Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Boundary Condition Type | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) |
|---------------------|-------------------------------|-------------------------------|----------------------------|--|----------------------------|------------------------------|
| FES A1 | 5,212.17 | 5,210.01 | User Defined Tailwater | 5,210.96 | 5,211.25 | 11.89 |
| CONNECT TO EXISTING | 5,211.48 | 5,208.29 | Free Outfall | 0.00 | 5,208.55 | 0.60 |

4270 Storm CAD.stsw 3/27/2024

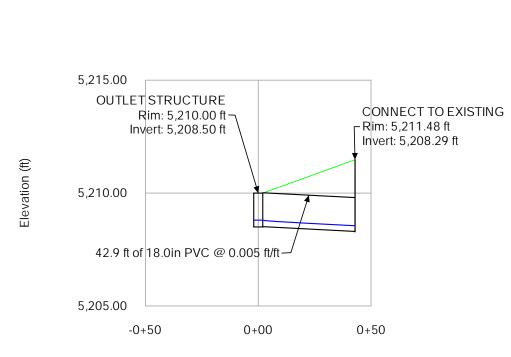
Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 5 of 13 Berkley Center Subdivision STORM LINE A1 PROFILE (5-Year Storm Event)



Station (ft)

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 6 of 13



Berkley Center Subdivision OUTLET PROFILE (5-Year Storm Event)

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 7 of 13

100-Year Storm Event

Catch Basin Table - Time: 0.00 hours

| Label | Elevation (Rim) (ft) | Elevation (Invert) (ft) | Inlet Location | Headloss Coefficient (Standard) | Flow (Total Out) (cfs) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|------------------|----------------------------|-------------------------------|-------------------|---------------------------------------|------------------------------|--------------------------------------|--|
| ST INLET A4 | 5,214.79 | 5,211.38 | In Sag | 0.700 | 22.95 | 5,215.37 | 5,214.79 |
| OUTLET STRUCTURE | 5,210.00 | 5,208.50 | In Sag | 0.000 | 20.50 | 5,210.00 | 5,210.00 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 8 of 13

100-Year Storm Event

Conduit Table - Time: 0.00 hours

| Label | Material | Diameter (in) | Invert (Stop) (ft) | Length (Scaled) (ft) | Slope (Calculated) (ft/ft) | Velocity (ft/s) | Flow (cfs) | Hydraulic Grade Line (In) (ft) | Hydraulic Grade Line (Out) (ft) |
|-------|----------|------------------|-----------------------|----------------------------|----------------------------------|--------------------|---------------|--------------------------------------|--|
| P5 | PVC | 24.0 | 5,210.18 | 368.7 | 0.002 | 7.31 | 22.95 | 5,214.79 | 5,212.54 |
| P6 | PVC | 24.0 | 5,211.21 | 69.5 | 0.002 | 7.31 | 22.95 | 5,215.80 | 5,215.38 |
| P10 | PVC | 24.0 | 5,210.01 | 29.4 | 0.002 | 7.31 | 22.95 | 5,212.04 | 5,211.72 |
| P11 | PVC | 18.0 | 5,208.30 | 42.9 | 0.005 | 11.60 | 20.50 | 5,210.77 | 5,209.80 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 9 of 13

100-Year Storm Event

Manhole Table - Time: 0.00 hours

| Label | Elevation (Rim) (ft) | Elevation (Invert in 1) (ft) | Elevation (Invert) (ft) | Elevation (Invert Out) (ft) | Headloss Coefficient (Standard) | Flow (Total Out) (cfs) | Depth (Out) (ft) | Hydraulic Grade Line (Out) (ft) | Hydraulic Grade Line (In) (ft) |
|----------|-------------------------|------------------------------------|-------------------------------|-----------------------------------|---------------------------------------|------------------------------|---------------------|--|--------------------------------------|
| ST MH A3 | 5,215.38 | 5,211.21 | 5,211.11 | 5,211.11 | 0.800 | 22.95 | 3.68 | 5,214.79 | 5,215.45 |
| ST MH A2 | 5,213.34 | 5,210.18 | 5,210.08 | 5,210.08 | 0.600 | 22.95 | 1.96 | 5,212.04 | 5,212.54 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 10 of 13

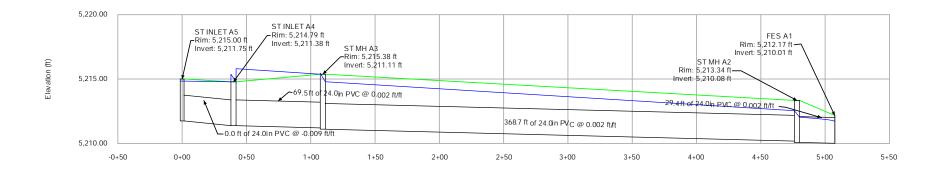
100-Year Storm Event

Outfall Table - Time: 0.00 hours

| Label | Elevation (Ground) (ft) | Elevation (Invert) (ft) | Boundary Condition Type | Elevation (User Defined Tailwater) (ft) | Hydraulic Grade (ft) | Flow (Total Out) (cfs) |
|---------------------|-------------------------------|-------------------------------|----------------------------|--|----------------------------|------------------------------|
| FES A1 | 5,212.17 | 5,210.01 | User Defined Tailwater | 5,211.47 | 5,211.72 | 22.95 |
| CONNECT TO EXISTING | 5,211.48 | 5,208.29 | Crown | 0.00 | 5,209.80 | 20.50 |

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 11 of 13 Berkley Center Subdivision STORM LINE A1 PROFILE (100-Year Storm Event)

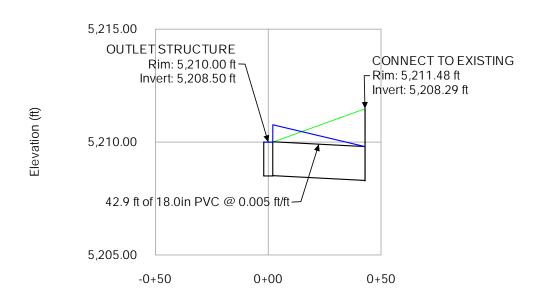


Station (ft)

4270 Storm CAD.stsw 3/27/2024

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 12 of 13

Berkley Center Subdivision STORM LINE A1 PROFILE (100-Year Storm Event)

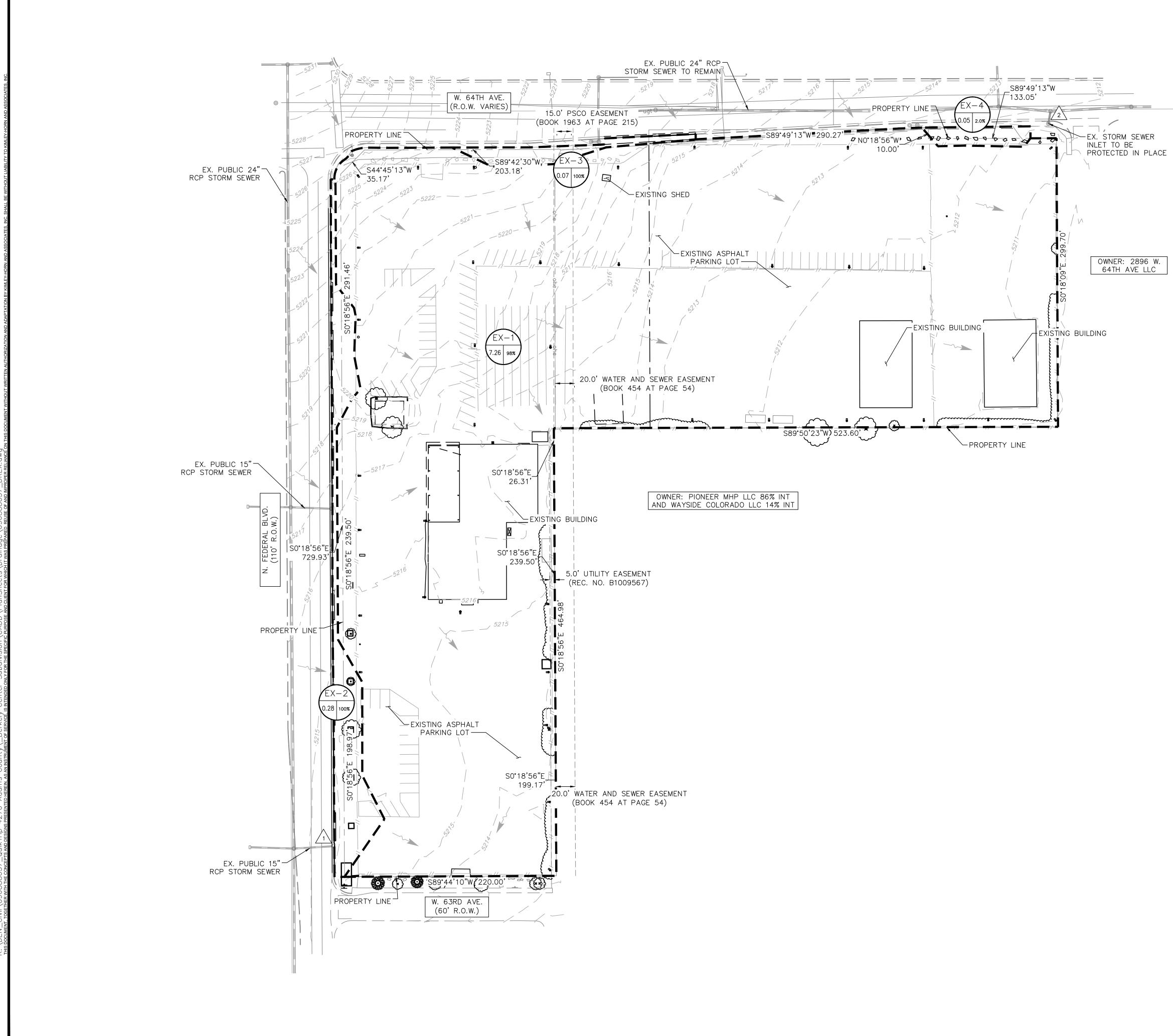


4270 Storm CAD.stsw 3/27/2024

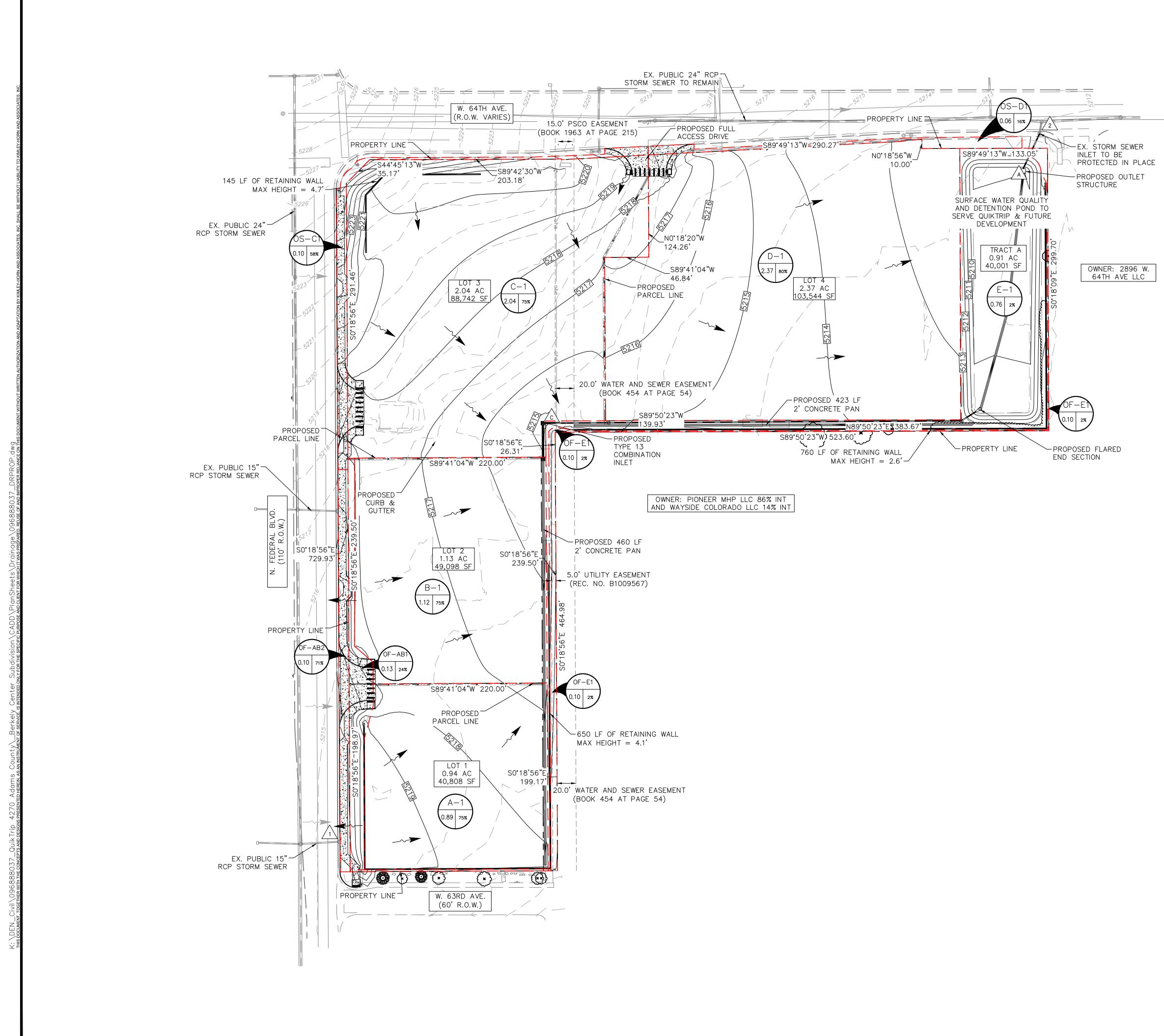
Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666 StormCAD [10.04.00.158] Page 13 of 13



APPENDIX E – DRAINAGE MAPS



| | \frown | ASE NO. PLT2023-0056 | |
|---|--|---|--|
| | ĊA | ASE NO. PLIZUZJ-0030 | APPR. |
| | | | DATE |
| | | | |
| | | | |
| PROPOSED DRAINA | GE LEGEND | | |
| | | | NOIS |
| (#) | # = BASIN DESIGNATION | | REVISION |
| AC I | AC = AREA IN ACRES I = % IMPERVIOUSNESS | | |
| \wedge | | | |
| <u>/</u> # | # = DESIGN POINT | | Image: Second se |
| | EXISTING BASIN BOUNDARY | | |
| -~-> | EXISTING FLOW DIRECTION | | |
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APPENDIX F – LEVEL 3 REPORT CHECKLIST

| | | | Level 3 | 8 – Storm Drainage Study Report |
|------|------------------------|----------|---------|---|
| Item | Submitted ¹ | County U | se Only | |
| No. | Submitted | Rejected | N/A | |
| 1. | | | | Cover sheet – Including project name, proponent's name, address, and telephone number, Project Engineer, and date of submittal. |
| 2. | | | | Table of contents - Show the page numbers for each section of the report, including appendices. |
| 3. | • | | | Project Description – Describe the type of permit(s) for which the applicant is applying, the size and location of the project site, address or parcel number, and legal description of the property, property zoning, etc. Describe other permits required. Describe the project, including proposed land use, site improvements, construction of impervious surfaces, and landscaping. |
| 4. | | | | Existing Conditions - include references to relevant reports such as basin plans, flood studies, groundwater studies, wetland designation, sensitive area designation, environmental impact statements, water quality report, etc. |
| 5. | | | | Existing Conditions - where such reports impose additional conditions on the applicant, those conditions shall be included in the report. In addition, an existing drainage report or master plan (County approved source) may be used as a baseline and updated with the proposed information. |
| 6. | > | | | Developed site drainage conditions - describe the land cover resulting from the proposed project; describe the potential stormwater quantity and quality impacts resulting from the proposed project; describe the proposal for the collection and conveyance of site runoff from the project site, for the control of any increase in stormwater quantity resulting from the project , and for the control of stormwater quality. |
| 7. | | | | Hydrological Analysis – including assumptions, computations, and results. |
| 8. | | | | Describe the drainage basin(s) to which the project site contributes runoff, and identify the receiving waters for each of these drainage basins. |
| 9. | | | | Soils hydrological group(s) |
| 10. | | | | Description of upstream basins - identify any sources of runoff to the project site. This should be based on a field investigation. Any existing drainage or erosion problems upstream which may have an impact on the proposed development should be noted. |
| 11. | | | | Downstream Drainage Analysis – the initial drainage report submittal shall include a Level 1 Downstream Drainage Analysis. Any further analysis of downstream conditions required beyond the Level 1 analysis shall be submitted as part of this Drainage Report. |

| | | A | ГТАСНМЕNT #7 CONTINUED |
|-----|-------------|---|--|
| 12. | | | Geotechnical Report - either supervised or prepared by a registered |
| 12. | | | professional engineer (sealed, signed and dated). |
| 13. | | | Basin map(s) – showing boundaries of project, any offsite contributing drainage basins, onsite drainage basins, approximate locations of all major drainage structures within the basins, and depict the course of stormwater origination from the subject property and extending all the way to the closest receiving body of water. Reference the source of the topographic base map, the scale of the map, and include a north arrow. |
| 14. | | | Hydraulic design computations - supporting the design of proposed conveyance, quantity and quality control facilities, and verifying the capacity of existing drainage facilities. These computations may include capacity and backwater analysis required either as part of the proposed drainage design or as a part of the downstream drainage investigation, and flood routing computations required for the design of detention/retention storage facilities, for wetland impact analysis, or for flood plain analysis. |
| 15. | | | Erosion and Sedimentation Control - include a description of proposed erosion control objectives and strategies; a description of erosion control facilities and other temporary water quality facilities proposed; a description of the revegetation plan for the project site; identification of areas of concern regarding soil stability and/or water quality impacts; computations for the sizing of temporary stormwater conveyance and quantity control facilities; computations for the design and sizing of proposed sediment containment facilities, etc. |
| 16. | > | | Appendices – include copies of any additional relevant reports, prepared by others, which support or corroborate the findings, conclusions, or assumptions contained in the Drainage Report; copies of any additional permits (or completed permit applications) required for the project. |
| | | | Vicinity Map |
| 17. | | | Sheet Size – 11" x 17" or 8 ¹ / ₂ " x 11" |
| 18. | | | Project Title Sheet |
| 19. | | | Project Site Plan |
| 20. | | | Title Block – include name and address of proposed project/development, submittal date, title of drawing, and page number. |
| 21. | • | | Drawing Information – • North arrow indicator • Section-Township-Range • Drawing Scale • Symbol Legend |
| 22. | | | Drawing Scale – as necessary to clearly present details. |

| | | A | ITACHMENT #7 CONTINUED |
|------------------|-----------------|-------------|--|
| 23. | | | Project site topography, land cover and land use; abutting property land cover and land use. |
| 24. | | | Offsite drainage to the property; creeks, lakes, ponds, wetlands, ravines, gullies, steep slopes, springs, and other environmentally sensitive areas on or adjacent to the project site. |
| 25. | | | General soils conditions present within the project site. |
| 26. | | | Existing natural and manmade drainage facilities within and immediately adjacent to the project site. |
| 27. | | | Points of discharge for drainage from the project site. |
| 28. | | | Impact on adjacent properties. Location(s) of downstream outfall points. |
| 29. | | | Signed statement from engineer, developer |
| Developer's Comm | ents (please re | ference the | e item number for each comment) |
| | | | |
| County's Comment | 5 | | |
| | | | |

¹ To be checked by the Developer. If a "submitted" box is not checked, the Applicant must explain (in comment box above) or the application may be rejected for insufficient information.

Traffic Impact Study

Berkley Center Subdivision Adams County, Colorado

Prepared for:

QuikTrip Corporation

Kimley »Horn

Adams County, Colorado

Prepared for QuikTrip Corporation 12000 Washington Street, Suite 175 Thornton, CO 80241

Prepared by Tyler E. Smith, P.E Kimley-Horn and Associates, Inc. 6200 South Syracuse Way Suite 300 Greenwood Village, Colorado 80111 (303) 228-2300



April 2024

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1.0 EXECUTIVE SUMMARY

This report has been prepared to document the results of a Traffic Impact Study for the Berkley Center Subdivision proposed to be located on the southeast corner of the 64th Avenue and Federal Boulevard (US-287) intersection in Adams County, Colorado. The Berkley Center Subdivision is proposed to include 37,920 square feet of general light industrial space, a 5,200 square foot fast food restaurant, a 5,312 square foot convenience store with a 16 fueling position gas station, and a one (1) tunnel car wash. It is expected that the Berkley Center Subdivision will be completed in the next several years; therefore, analysis was conducted for the 2026 short-term buildout horizon as well as the 2045 long-term twenty-year planning horizon.

The purpose of this traffic study is to identify project traffic generation characteristics to determine potential project traffic related impacts on the local street system and to develop the necessary mitigation measures required for the identified traffic impacts. The following intersection of 64th Avenue and Federal Boulevard (US-287) (#1) was incorporated into this traffic study in accordance with Adams County and State of Colorado Department of Transportation (CDOT) standards and requirements.

In addition, the proposed full movement access along the south side of 64th Avenue (#2), and the two proposed right-in/right-out accesses along the east side of Federal Boulevard (US-287) (#3 and #4) were evaluated.

Regional access to the Berkley Center Subdivision will be provided by Interstate 76, Interstate 25, and US Highway 36 (US-36). Primary access will be provided by 64th Avenue and Federal Avenue (US-287). Direct access will be provided by the proposed full movement access along the south side of 64th Avenue (#2), approximately 350 feet east of Federal Boulevard (US-287), measured center to center, and the two proposed right-in/right-out accesses along the east side of Federal Boulevard (US-287) (#3 and #4), approximately 325 feet and 600 feet south of 64th Avenue, measured center to center.

The Berkley Center Subdivision project is expected to generate approximately 9,406 daily weekday driveway trips, with 808 of these trips occurring during the morning peak hour and 634 trips occurring during the afternoon peak hour. Accounting for pass-by, expected net new (non



pass-by) trips to the surrounding street network results in approximately 3,470 weekday daily trips, of which 333 trips and 257 trips are anticipated during the weekday morning and afternoon peak hours, respectively.

Based on the analysis presented in this report, Kimley-Horn believes the overall Berkley Center Subdivision project will be successfully incorporated into the existing and future roadway network. Analysis of the existing street network, the proposed project development, and expected traffic volumes resulted in the following conclusions and recommendations:

- With completion of the Berkley Center Subdivision project, one full movement access is proposed along the south side of 64th Avenue and two right-in/right-out accesses are proposed along the east side of Federal Boulevard (US-287). It is recommended that a R1-1 "STOP" sign be installed on the exiting approaches of all three proposed accesses. A R3-2 "No Left Turn" sign is also recommended to be placed underneath the recommended "STOP" sign to further restrict exiting left turn movements at the two right-in/right-out accesses along Federal Boulevard (US-287).
- The threshold for requiring an access permit along Colorado Department of Transportation (CDOT) roadways occurs when project traffic is anticipated to increase the existing access traffic volumes by more than 20 percent. Based on traffic projections, the addition of project traffic on the east leg of the 64th Avenue and Federal Boulevard (US-287) intersection is anticipated to increase existing traffic by more than 20 percent. Therefore, an access permit is anticipated to be needed at this intersection as development occurs. Additionally, since the two right-in/right-out accesses along Federal Boulevard (US-287) are new accesses, CDOT access permits are anticipated to be needed for these two accesses.
- Any onsite or offsite improvements should be incorporated into the Civil Drawings and conform to standards of Adams County, CDOT, and the Manual on Uniform Traffic Control Devices (MUTCD) – 2009 Edition.



2.0 INTRODUCTION

Kimley-Horn has prepared this report to document the results of a Traffic Impact Study for the Berkley Center Subdivision proposed to be located on the southeast corner of the 64th Avenue and Federal Boulevard (US-287) intersection in Adams County, Colorado. A vicinity map illustrating the Berkley Center Subdivision development location is shown in **Figure 1**. The Berkley Center Subdivision is proposed to include 37,920 square feet of general light industrial space, a 5,200 square foot fast food restaurant, a 5,312 square foot convenience store with a 16 fueling position gas station, and a one (1) tunnel car wash. A conceptual site plan of the project is attached in **Appendix F**. It is expected that the Berkley Center Subdivision will be completed in the next several years; therefore, analysis was conducted for the 2026 short-term buildout horizon as well as the 2045 long-term twenty-year planning horizon.

The purpose of this traffic study is to identify project traffic generation characteristics to determine potential project traffic related impacts on the local street system and to develop the necessary mitigation measures required for the identified traffic impacts. The following intersection of 64th Avenue and Federal Boulevard (US-287) (#1) was incorporated into this traffic study in accordance with Adams County and CDOT standards and requirements.

In addition, the proposed full movement access along the south side of 64th Avenue (#2), and the two proposed right-in/right-out accesses along the east side of Federal Boulevard (US-287) (#3 and #4) were evaluated.

Regional access to the Berkley Center Subdivision will be provided by Interstate 76, Interstate 25, and US Highway 36 (US-36). Primary access will be provided by 64th Avenue and Federal Avenue (US-287). Direct access will be provided by the proposed full movement access along the south side of 64th Avenue (#2), approximately 350 feet east of Federal Boulevard (US-287), measured center to center, and the two proposed right-in/right-out accesses along the east side of Federal Boulevard (US-287) (#3 and #4), approximately 325 feet and 600 feet south of 64th Avenue, measured center to center.







FIGURE 1 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO VICINITY MAP



3.1 Existing Study Area

The existing site is comprised of vacant car dealership. To the north of the site is a gas station, industrial uses, and single-family homes. A trailer park is located south of the project while industrial uses and a car dealership are located to the west of the site. East of the project site is a trailer park and industrial uses.

3.2 Existing Roadway Network

Federal Boulevard (US-287) extends north/south with three through lanes in each direction and a raised median. The posted speed limit along US-287 near the site is 45 miles per hour. CDOT classifies Federal Boulevard as a NR-A: Non-Rural Principal Highway.

64th Avenue extends in the east/west direction with one through lane in each direction and contains a center two-way left turn lane. It has a posted speed limit of 30 miles per hour west of Federal Boulevard (US-287) and a speed limit of 35 miles per hour east of Federal Boulevard (US-287).



The signalized intersection of 64th Avenue and Federal Boulevard (US-287) (#1) operates with protected-permissive left turn phasing on all four approaches. The northbound and southbound Federal Boulevard approaches provide a left turn lane and three through lanes with the outside lane being a shared through/right turn lane. The eastbound and westbound 64th Avenue approaches consist of one left turn lane, one through lane, and a right turn lane. An aerial photo of the existing intersection configuration is below (north is up).



64th Avenue & Federal Boulevard (US-287) (#1)

The existing intersection lane configuration and control for the study area intersection are shown in **Figure 2**.







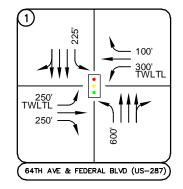
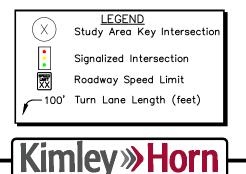


FIGURE 2 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO EXISTING GEOMETRY AND CONTROL



3.3 Existing Traffic Volumes

Existing turning movement counts were conducted at the study intersections on Tuesday, October 31, 2023 during the weekday morning and afternoon peak hours. The counts were conducted during the morning and afternoon peak hours of adjacent street traffic in 15-minute intervals from 7:00 AM to 9:00 AM and 4:00 PM to 6:00 PM on this count date. The existing intersection traffic volumes are shown in **Figure 3** with count sheets provided in **Appendix A**.

3.4 Unspecified Development Traffic Growth

According to information provided on the website for the Colorado Department of Transportation (CDOT), the 20-year growth factor along Federal Boulevard (US-287) in the vicinity of the site is between 1.16 and 1.19. The 20-year growth factor equates to average annual growth rate of 0.81 percent. Traffic information from the CDOT Online Transportation Information System (OTIS) website is included in **Appendix B**. This annual growth rate was used to estimate near-term 2026 and long-term 2045 traffic volume projections at the key intersections. Background traffic volumes for 2026 and 2045 are shown in **Figures 4** and **5**, respectively.







| | 91(20 105(13) 152(13) | , 80) → | 1 | 9(64) 0(193) 5(91) (193) | |
|----|-----------------------------|------------|---------|--|-------|
| 64 | TH AVE | & FED | ERAL BL | VD (US- | -287) |

Tuesday, October 31, 2023 7:45 to 8:45AM (4:15 to 5:15PM)

FIGURE 3 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO 2023 EXISTING TRAFFIC VOLUMES <u>LEGEND</u>

Study Area Key Intersection

XXX(XXX) Weekday AM(PM) Peak Hour Traffic Volumes

Х

XX,X00 Estimated Daily Traffic Volume

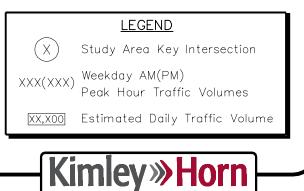






| $108(184) \rightarrow (021) \\ 156(137) \rightarrow (021) \\ 156(137) \rightarrow (021) \\ 9 \\ 9 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$ |
|--|
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FIGURE 4 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO 2026 BACKGROUND TRAFFIC VOLUMES

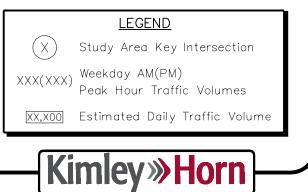






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FIGURE 5 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO 2045 BACKGROUND TRAFFIC VOLUMES



4.1 Trip Generation

Site-generated traffic estimates are determined through a process known as trip generation. Rates and equations are applied to the proposed land use to estimate traffic generated by the development during a specific time interval. The acknowledged source for trip generation rates is the *Trip Generation Manual*¹ published by the Institute of Transportation Engineers (ITE). ITE has established trip rates in nationwide studies of similar land uses. For this study, Kimley-Horn used the ITE Trip Generation Report average rates/fitted curve equations that apply to General Light Industrial (ITE Land Use Code 110), Fast-Food Restaurant with Drive Through (ITE Land Use Code 934), Convenience Store/Gas Station (ITE Land Use Code 945), and Automated Car Wash (ITE Land Use Code 948) for traffic associated with the development.

Since the full buildout of the Berkley Center Subdivision project is proposed to contain a mix of uses, internal capture trips are expected to occur on site as well. These internal capture trips are shared trips from vehicles already within the internal street network. These shared trips reduce the number of total external trips. The trips were calculated by CDOT procedures, limiting morning peak hour trips to two (2) percent internal capture and the afternoon peak hour trips to eight (8) percent internal capture.

Since the project is a commercial development, pass-by trips are expected. These pass-by trips are vehicles already on the street network that will be attracted to the project site en route to a final destination. The pass-by percentages were obtained from the ITE "Trip Generation Manual", Eleventh Edition.

The Berkley Center Subdivision project is expected to generate approximately 9,406 daily weekday driveway trips, with 808 of these trips occurring during the morning peak hour and 634 trips occurring during the afternoon peak hour. Accounting for pass-by, expected net new (non pass-by) trips to the surrounding street network results in approximately 3,470 weekday daily trips, of which 333 trips and 257 trips are anticipated during the weekday morning and afternoon

¹ Institute of Transportation Engineers, *Trip Generation Manual*, Eleventh Edition, Washington DC, 2021.

peak hours, respectively. Calculations were based on the procedure and information provided in the ITE *Trip Generation Manual, 11th Edition – Volume 1: User's Guide and Handbook,* 2021. **Table 1** summarizes the estimated trip generation for the Berkley Center Subdivision. The trip generation worksheets are included in **Appendix C**.

| | | | Weekda | y Vehicl | e Trips | | | |
|---|-------|-----|--------|----------|---------|-------------|-------|--|
| Land Use and Size | Daily | AM | Peak H | our | PM | l Peak Hour | | |
| | Daily | In | Out | Total | In | Out | Total | |
| General Light Industrial (110) – 37,920 Square Feet | 178 | 25 | 4 | 29 | 2 | 17 | 19 | |
| Fast-Food Restaurant w/ DT (934) – 5,200 Square Feet | 2,237 | 116 | 112 | 227 | 82 | 76 | 158 | |
| Convenience Store/Gas Station (945) – 5,312 Square Feet/16 Fueling Positions | 6,273 | 237 | 238 | 475 | 192 | 193 | 385 | |
| Automated Car Wash (948) – 1 Tunnel | 718 | 38 | 38 | 76 | 36 | 36 | 72 | |
| Total Trips after Internal Capture | 9,406 | 416 | 392 | 808 | 312 | 322 | 634 | |
| Total Trips after Internal Capture and Pass-By | 3,470 | 179 | 155 | 333 | 123 | 134 | 257 | |

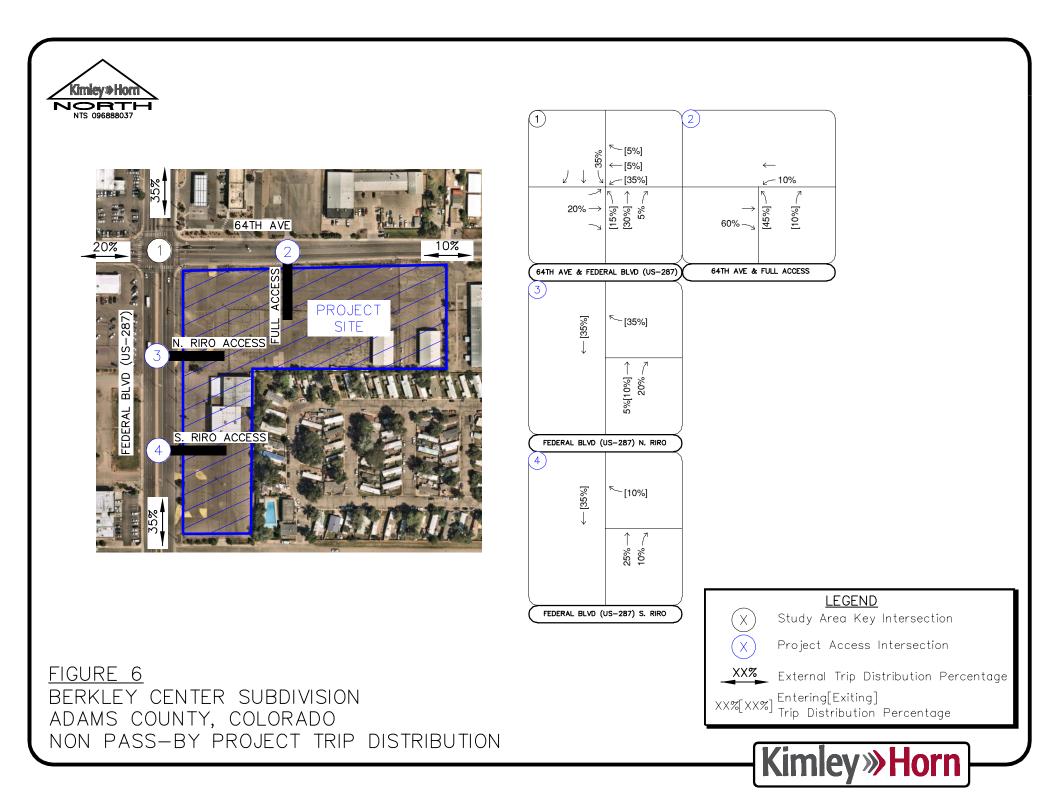
 Table 1 – Berkley Center Subdivision Traffic Generation

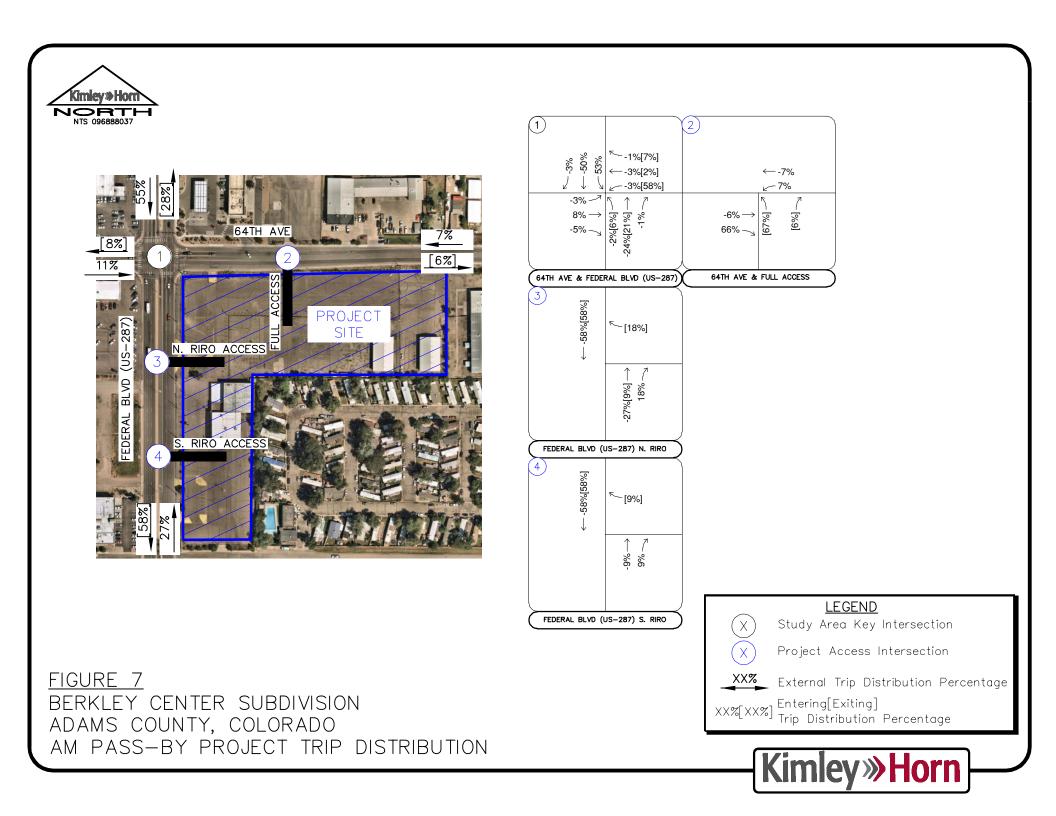
4.2 Trip Distribution

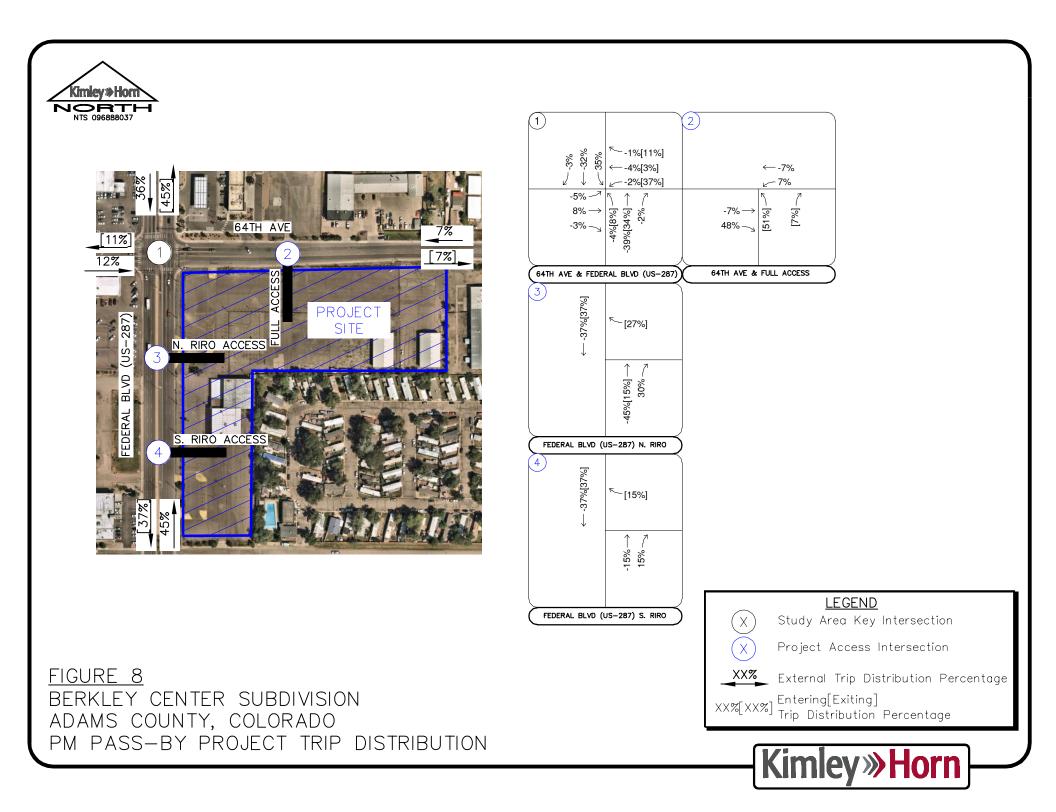
Distribution of site traffic on the street system was based on the area street system characteristics, existing traffic patterns, existing and anticipated surrounding demographic information, and the proposed access system for the project. The directional distribution of traffic is a means to quantify the percentage of site-generated traffic that approaches the site from a given direction and departs the site back to the original source. The non pass-by project trip distribution for the proposed development is illustrated in **Figure 6**.

Since the project is a commercial development, a certain amount of traffic attracted to the gas station and fast-food restaurant will already be passing by the site. This pass-by distribution is a means to quantify the amount of traffic arriving to the site from a given direction and then leaving the site in the same original direction of travel, continuing the driver's trip. The expected weekday morning and afternoon peak hour pass-by trip distributions were calculated based on actual traffic volumes. Directional differences in the morning and afternoon peak hours were accounted for in the pass-by distributions as shown in **Figures 7** and **8**, respectively.









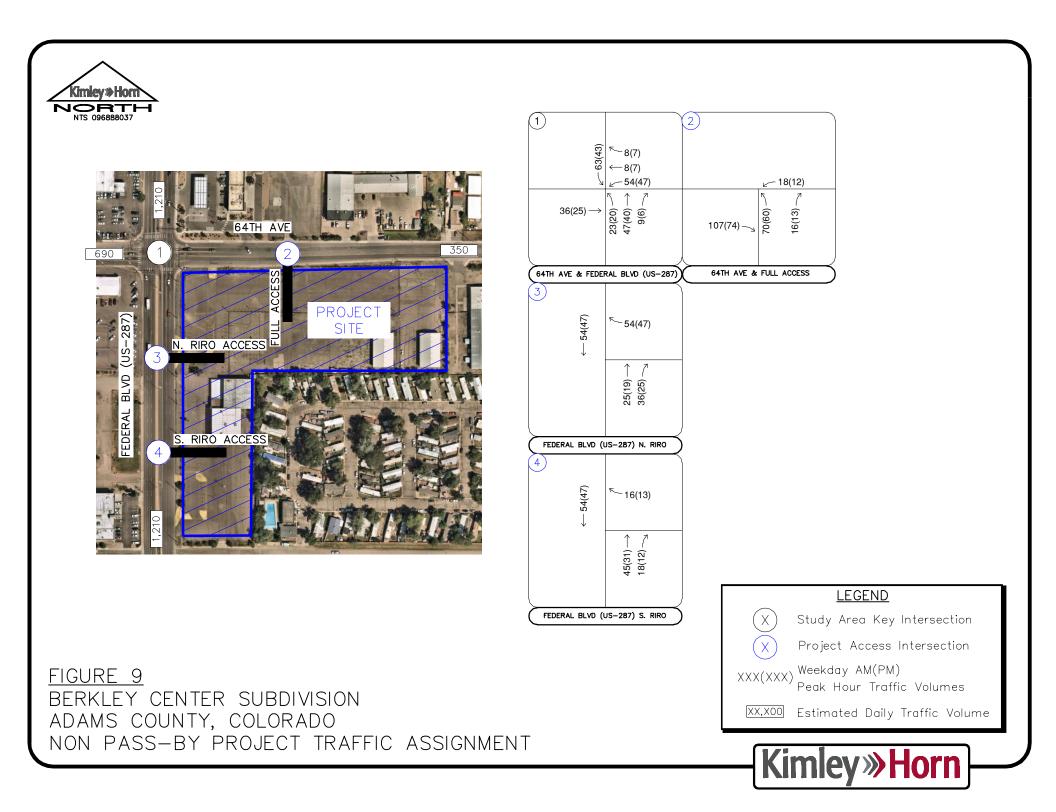
4.3 Traffic Assignment

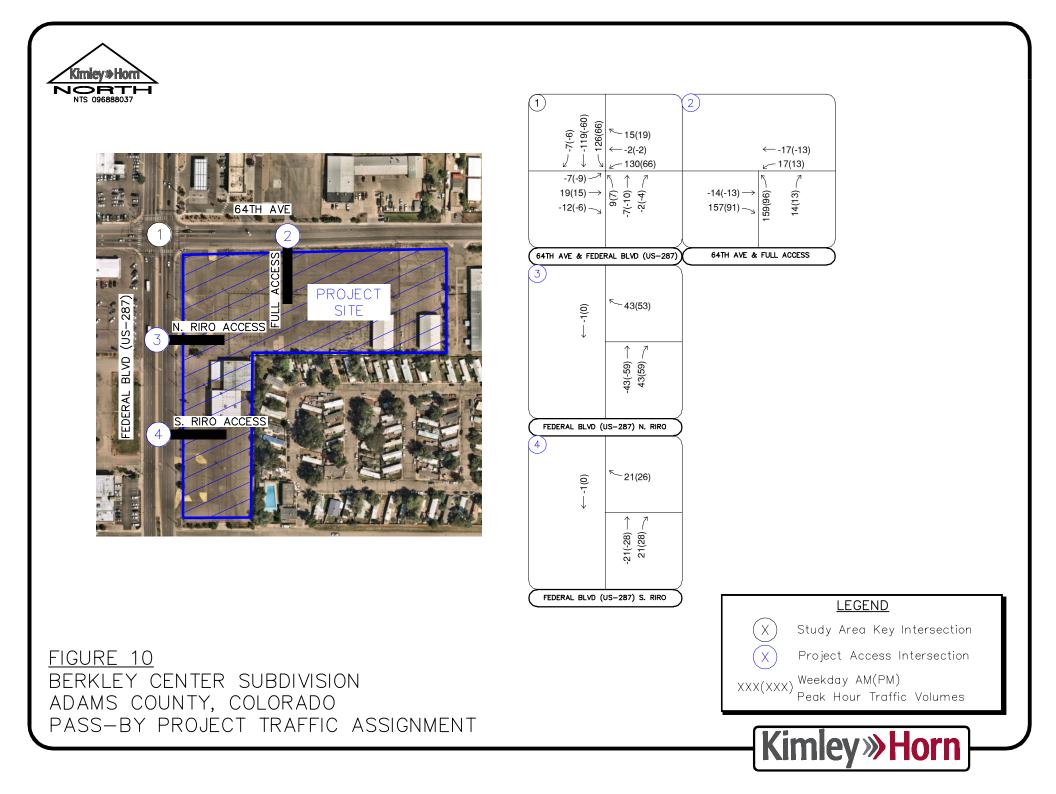
Project traffic assignment was obtained by applying the project trip distribution to the estimated traffic generation of the development shown in **Table 1**. Project non pass-by traffic assignment is shown in **Figure 9**, while **Figure 10** illustrates the expected pass-by traffic assignment for the Berkley Center Subdivision development.

4.4 Total (Background Plus Project) Traffic

Site traffic volumes were added to the background volumes to represent estimated traffic conditions for the short-term 2026 buildout horizon and long-term 2045 twenty-year planning horizon. These total traffic volumes for the study area are illustrated for the 2026 and 2045 horizon years in **Figures 11** and **12**, respectively.

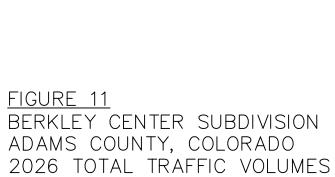


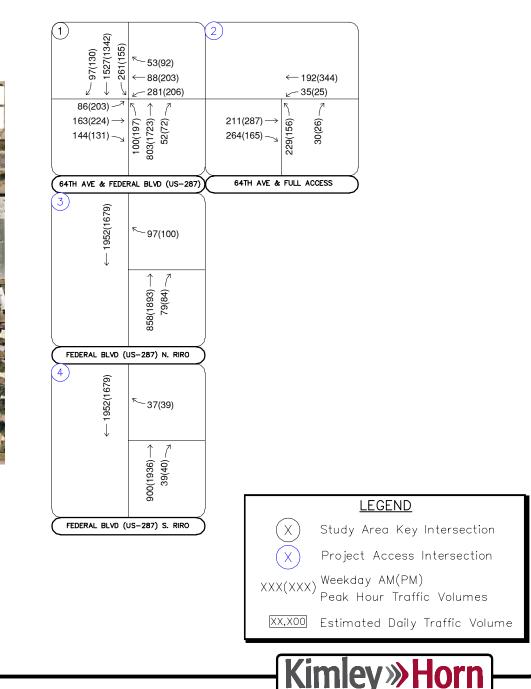








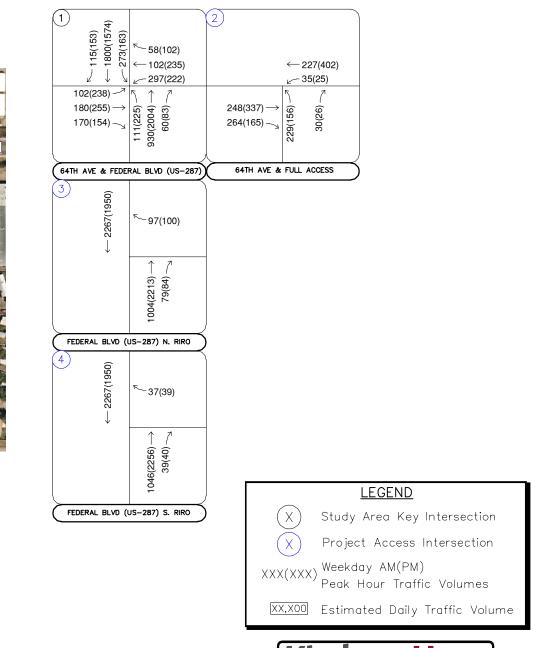












Kimley-Horn's analysis of traffic operations in the site vicinity was conducted to determine potential capacity deficiencies in the 2026 and 2045 development horizons at the identified key intersections. The acknowledged source for determining overall capacity is the *Highway Capacity Manual (HCM)*².

5.1 Analysis Methodology

Capacity analysis results are listed in terms of Level of Service (LOS). LOS is a qualitative term describing operating conditions a driver will experience while traveling on a particular street or highway during a specific time interval. It ranges from A (very little delay) to F (long delays and congestion). For intersections and roadways in this study area, standard traffic engineering practice recommends overall intersection LOS D and movement/approach LOS E as the minimum desirable thresholds for acceptable operations. **Table 2** shows the definition of level of service for signalized and unsignalized intersections.

| Level of Service | Signalized Intersection Average Total Delay (sec/veh) | Unsignalized Intersection Average Total Delay (sec/veh) |
|---------------------|---|---|
| A | ≤ 10 | ≤ 10 |
| В | > 10 and ≤ 20 | > 10 and ≤ 15 |
| С | > 20 and ≤ 35 | > 15 and ≤ 25 |
| D | > 35 and ≤ 55 | > 25 and ≤ 35 |
| E | > 55 and ≤ 80 | > 35 and ≤ 50 |
| F | > 80 | > 50 |

Table 2 – Level of Service Definitions

Definitions provided from the Highway Capacity Manual, Sixth Edition, Transportation Research Board, 2016.

Study area intersections were analyzed based on average total delay analysis for signalized and unsignalized intersections. Under the unsignalized analysis, the LOS for a two-way stop-controlled intersection is determined by the computed or measured control delay and is defined for each minor movement. LOS for a two-way stop-controlled intersection is not defined for the intersection as a whole. LOS for signalized intersections are defined for each approach and for the overall intersection.

² Transportation Research Board, *Highway Capacity Manual*, Sixth Edition, Washington DC, 2016.

5.2 Key Intersection Operational Analysis

Calculations for the operational level of service at the key intersections for the study area are provided in **Appendix D**. The existing year analysis is based on the lane geometry and intersection control shown in **Figure 2**. Existing peak hour factors were utilized in the existing, 2026, and 2045 horizon analysis years. The existing heavy vehicle percentages obtained from the turning movement counts were also used in each horizon year. Based on increased national attention given to establishing appropriate yellow and all-red clearance intervals to improve intersections. The increase in yellow and all red time sacrifices intersection capacity for improved safety. Synchro traffic analysis software was used to analyze the signalized and unsignalized key intersections for HCM level of service.

64th Avenue & Federal Boulevard (US-287)

The signalized intersection of 64th Avenue and Federal Boulevard (US-287) (#1) operates with protected-permissive left turn phasing on all four approaches. The intersection operates acceptably at LOS C during both peak hours under existing conditions. With project traffic, this intersection is anticipated to continue operating at an acceptable level of service throughout the 2045 horizon. Therefore, no improvements or modifications are anticipated to be needed at this intersection based on the addition of project traffic and this operational level of service analysis. **Table 3** provides the results of the LOS analysis conducted at this intersection.

| | | aiù (05-201 | (#1) LO3 Ke | 550115 | | |
|------------------------------|--------------------|-------------|--------------------|--------|--|--|
| | AM Pea | ik Hour | PM Peak Hour | | | |
| Scenario | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | | |
| 2023 Existing | 23.7 | С | 29.3 | С | | |
| 2026 Background | 24.3 | С | 30.2 | С | | |
| 2026 Background Plus Project | 34.1 | С | 35.0 | D | | |
| 2045 Background | 28.9 | С | 38.7 | D | | |
| 2045 Background Plus Project | 40.1 | D | 47.2 | D | | |

Table 3 – 64th Avenue & Federal Boulevard (US-287) (#1) LOS Results

Project Accesses

With completion of the Berkley Center Subdivision project, one full movement access is proposed along the south side of 64th Avenue (#2) and two right-in/right-out accesses are proposed along the east side of Federal Boulevard (US-287) (#3 and #4). It is recommended that a R1-1 "STOP" sign be installed on the exiting approaches of all three proposed project accesses. A R3-2 "No Left Turn" sign is also recommended to be placed underneath the recommended "STOP" sign to further restrict exiting left turn movements at the two right-in/right-out accesses along Federal Boulevard (US-287) (#3 and #4). **Table 4** provides the results of the level of service for this project accesses. As shown in the table, the project accesses are anticipated to have all movements operating with acceptable LOS C or better during the peak hours in both the buildout year 2026 and the 2045 long-term horizons.

| | | 2026 | Total | | 2045 Total | | | | | |
|---------------------------------------|------------------------|--------|------------------------|--------|------------------------|--------|------------------------|-----|--|--|
| Intersection | AM Pea | k Hour | PM Pea | k Hour | AM Pea | k Hour | PM Peak Hour | | | |
| Intersection | Delay (sec/ veh) | LOS | Delay (sec/ veh) | LOS | Delay (sec/ veh) | LOS | Delay (sec/ veh) | LOS | | |
| 64 th Ave Full Access (#2) | | | | | | | | | | |
| Northbound Approach | 15.8 | С | 15.0 | С | 17.0 | С | 16.4 | С | | |
| Westbound Left | 8.6 | А | 8.5 | Α | 8.8 | Α | 8.7 | Α | | |
| Federal Blvd N. RIRO (#3) | | | | | | | | | | |
| Westbound Right | 10.9 | В | 15.0 | С | 11.2 | В | 18.2 | С | | |
| Federal Blvd S. RIRO (#4) | | | | | | | | | | |
| Westbound Right | 10.4 | В | 13.9 | В | 10.7 | В | 15.6 | С | | |

| | Table 4 – Proje | ct Access | Level of | Service | Results |
|--|-----------------|-----------|----------|---------|---------|
|--|-----------------|-----------|----------|---------|---------|

5.3 CDOT Turn Bay Length Analysis

The threshold for requiring an access permit along Colorado Department of Transportation (CDOT) roadways occurs when project traffic is anticipated to increase the existing access traffic volumes by more than 20 percent. Based on traffic projections, the addition of project traffic on the east leg of the 64th Avenue and Federal Boulevard (US-287) (#1) intersection is anticipated to increase existing traffic by more than 20 percent. Therefore, an access permit is anticipated to be needed at this intersection as development occurs. Additionally, since the two right-in/right-out accesses along Federal Boulevard (US-287) (#3 and #4) are new accesses, access permits are anticipated to be needed for these two accesses.

Auxiliary turn lanes along CDOT controlled highways are to be implemented based on volume threshold requirements set forth in the State Highway Access Code. Further, turn lane lengths should be designed based on the State Highway Access Code. Federal Boulevard (US-287) is categorized as a Non-Rural Principal Highway (NR-A) and has a posted speed limit of 45 miles per hour adjacent to the site. According to the State Highway Access Code for category Non-Rural Principal Highway (NR-A) roadways, the turn lane warrants are as follows:

- A left turn deceleration lane and taper with storage length is required for any access with a projected peak hour ingress turning volume greater than 10 vph. The taper length will be included within the required deceleration length.
- A right turn deceleration lane and taper is required for any access with a projected peak hour ingress turning volume greater than 25 vph. The taper length will be included within the required deceleration length.
- Right turn acceleration lane and taper is required for any access with a projected peak hour right turning volume greater than 50 vph when the posted speed on the highway is greater than 40 mph. The taper length will be included within the required acceleration length.
- Right turn deceleration and acceleration lanes are generally not required on roadways with three or more travel lanes in the direction of the right turn.



Based on the traffic volume projections, turn lane requirements at the project access intersections along Federal Boulevard (US-287) are as follows:

64th Avenue & Federal Boulevard (US-287) (#1)

- A southbound left turn lane <u>is</u> warranted and exists based on existing traffic volumes being 70 southbound left turns during the peak hour and the threshold being 10 vph. Based on the 45 mile per hour speed limit, the deceleration length is 275 feet, plus a 160-foot taper. The existing southbound left turn lane provides 225 feet of storage with a 150-foot taper. The storage requirement is 275 feet in 2026 and 2045 based on the projected left turning volume. The existing southbound left turn lane does not meet CDOT access code requirements. However, this southbound left turn lane is built to the maximum length due to the back-to-back turn left turn lane to the north.
- Due to Federal Boulevard (US-287) having three northbound and southbound through lanes, right turn deceleration and acceleration lanes are not required at this intersection based on the CDOT access code.

Federal Boulevard (US-287) North Right-In/Right-Out Access (#3)

• Due to Federal Boulevard (US-287) having three northbound and southbound through lanes, right turn deceleration and acceleration lanes are not required at this access based on the CDOT access code.

Federal Boulevard (US-287) South Right-In/Right-Out Access (#4)

 Due to Federal Boulevard (US-287) having three northbound and southbound through lanes' right turn deceleration and acceleration lanes are not required at this access based on the CDOT access code.



5.4 Vehicle Queuing Analysis

A vehicle queuing analysis was conducted for the study area intersections. The queuing analysis was performed using Synchro presenting the results of the 95th percentile queue lengths. Results are shown in the following **Table 5** with calculations provided within the level of service operational sheets of **Appendix D** for unsignalized intersections and **Appendix E** for signalized intersections.

| T GR | | | IY Analysis Res | | |
|--|---|---------------------------------------|--------------------------------------|---------------------------------------|--------------------------------------|
| Intersection Turn Lane | Existing Turn Lane Length (feet) | 2026 Calculated Queue (feet) | 2026 Recommended Length (feet) | 2045 Calculated Queue (feet) | 2045 Recommended Length (feet) |
| 64 th Ave & Federal Blvd (#1) | | | | | |
| Eastbound Left | 250'/TWLTL | 189' | 250'/TWLTL | 239' | 250'/TWLTL |
| Eastbound Right | 250' | 56' | 250' | 61' | 250' |
| Westbound Left | 300'/TWLTL | 317' | 300'/TWLTL | 367' | 300'/TWLTL |
| Westbound Right | 100' | 25' | 100' | 29' | 100' |
| Northbound Left | 600' | 209' | 600' | 262' | 600' |
| Southbound Left | 225' | 201' | 225' | 223' | 225' |
| 64 th Ave Full Access (#2) | | | | | |
| Westbound Left | TWLTL | 25' | TWLTL | 25' | TWLTL |

Table 5 – Turn Lane Queuing Analysis Results

TWLTL = Two-Way Left Turn Lane

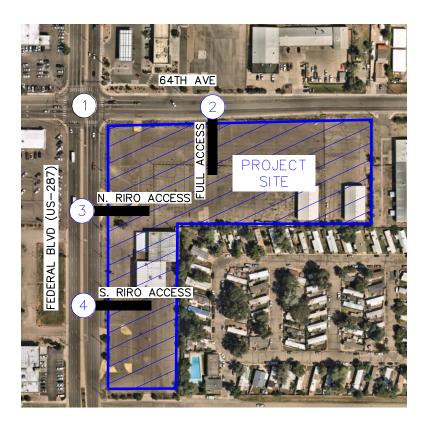
As shown in **Table 5**, all vehicle queues are anticipated to remain within the existing turn lane lengths or center two way left turn lane throughout the 2045 horizon.

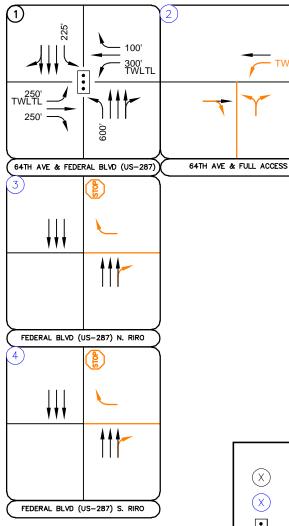
5.5 Improvement Summary

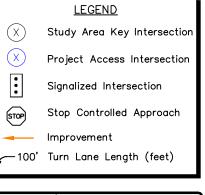
Based on the results of the intersection operational and vehicle queuing analysis, the key intersection recommended improvements and control are shown in **Figure 13**.











Kimley

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TWLTL

STO

FIGURE 13 BERKLEY CENTER SUBDIVISION ADAMS COUNTY, COLORADO RECOMMENDED GEOMETRY AND CONTROL

6.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the analysis presented in this report, Kimley-Horn believes the overall Berkley Center Subdivision project will be successfully incorporated into the existing and future roadway network. Analysis of the existing street network, the proposed project development, and expected traffic volumes resulted in the following conclusions and recommendations:

- With completion of the Berkley Center Subdivision project, one full movement access is proposed along the south side of 64th Avenue and two right-in/right-out accesses are proposed along the east side of Federal Boulevard (US-287). It is recommended that a R1-1 "STOP" sign be installed on the exiting approaches of all three proposed accesses. A R3-2 "No Left Turn" sign is also recommended to be placed underneath the recommended "STOP" sign to further restrict exiting left turn movements at the two right-in/right-out accesses along Federal Boulevard (US-287).
- The threshold for requiring an access permit along Colorado Department of Transportation (CDOT) roadways occurs when project traffic is anticipated to increase the existing access traffic volumes by more than 20 percent. Based on traffic projections, the addition of project traffic on the east leg of the 64th Avenue and Federal Boulevard (US-287) intersection is anticipated to increase existing traffic by more than 20 percent. Therefore, an access permit is anticipated to be needed at this intersection as development occurs. Additionally, since the two right-in/right-out accesses along Federal Boulevard (US-287) are new accesses, CDOT access permits are anticipated to be needed for these two accesses.
- Any onsite or offsite improvements should be incorporated into the Civil Drawings and conform to standards of Adams County, CDOT, and the Manual on Uniform Traffic Control Devices (MUTCD) – 2009 Edition.





APPENDICES

Kimley **»Horn**



APPENDIX A

Intersection Count Sheets

Kimley **»Horn**

| | | | | F | ede 64t | ral E h A | | | | | | | | | | | id | Ж | |
|---|---|-------------------------------------|---------------------------------------|----------|--|---|--|----------------------------|-------------------------------|--------------------------------|---------------------------------------|---|---|----------------------------|----------|--|---|--|--|
| | | ≪ N | 1 | | Pe | eak H | <u>our</u> | | | | | С | | Date Perioe k Hou | d: 7 |)/31/20 7:00 Al 7:45 Al | M to | 9:00 A 8:45 A | |
| | 2 <u>34</u> 348 | → 64 | 0 = 0 91 = 105 = 152 = 1th Ave | | РНІ Л ← | ↓ ↓ 1 21 3,1 1 23 1 23 1 23 | 92 | | 64th A 29 80 95 0 | < _ | :B /B IB ;B | HV %: 2.6% 11.8% 4.0% 2.6% 3.6% | PHF 0.83 0.89 0.91 0.89 0.92 | | | | | | |
| Two-H | lour C | ount | | | s | I | | | | 1 | | | | | | | | | |
| Inter | | | 64th Eastb | - | | | | Ave | | | | al Blvd | | | | al Blvd | | 15-min | Rolling |
| Sta | irt | UT | Lasib | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | Total | One Hour |
| 7:00 |) AM | 0 | 29 | 51 | 33 | 0 | 11 | 17 | 8 | 2 | 3 | 120 | 11 | 2 | 20 | 337 | 4 | 648 | 0 |
| 7:15 | 5 AM | 0 | 14 | 27 | 38 | 0 | 13 | 15 | 13 | 7 | 4 | 179 | 9 | 2 | 9 | 428 | 15 | 773 | 0 |
| 7:30 | | 0 | 25 | 38 | 37 | 0 | 17 | 23 | 4 | 2 | 10 | 162 | 12 | 0 | 10 | 366 | 28 | 734 | 0 |
| 7:45 | | 0 | 23 | 31 | 33 | 0 | 23 | 13 | 8 | 3 | 12 | 203 | 15 | 2 | 14 | 337 | 26 | 743 | 2,898 |
| 8:00 | | 0 | 28 | 28 | 49 | 0 | 25 | 15 | 6 | 3 | 17 | 145 | 5 | 2 | 17 | 448 | 25 | 813 | 3,063 |
| 8:15 8:30 | | 0 | 18 22 | 20 26 | 34 36 | 0 | 25 22 | 23 29 | 9 6 | 3 5 | 15 8 | 204 193 | 13 11 | 6 3 | 14 12 | 453 369 | 29 22 | 866 764 | 3,156 3,186 |
| 8:45 | | 0 | 29 | 20 | 33 | 0 | 14 | 26 | 8 | 9 | 19 | 174 | 10 | 2 | 7 | 357 | 23 | 731 | 3,174 |
| Count | | 0 | 188 | 241 | 293 | 0 | 150 | 161 | 62 | 34 | 88 | 1,380 | 86 | 19 | 103 | 3,095 | 172 | 6,072 | 0 |
| Peak | All | 0 | 91 | 105 | 152 | 0 | 95 | 80 | 29 | 14 | 52 | 745 | 44 | 13 | 57 | 1,607 | 102 | 3,186 | 0 |
| Hour | HV | 0 | 1 | 7 | 1 | 0 | 13 | 7 | 4 | 1 | 1 | 25 | 7 | 0 | 4 | 41 | 2 | 114 | 0 |
| | HV% | | | | | | | | | | | 3% | | | 7% | 3% | 2% | 4% | 0 |
| Note: Tv | vo-nour | count | summa | ry volu | mes ind | ciude h | eavy ve | nicies l | out excl | uae bic | ycies i | n overal | ı count. | | | | | | |
| | | | | | | | | | | | - | | | | | | | | |
| Inter | val | | Hea | vy Veł | nicle To | otals | | | | Bicy | cles | | | | Pe | edestria | ans (Cr | ossing Le | g) |
| Sta | ırt | EB | WB | N | l₿ | SB | Total | EB | WB | N | IB | SB | Total | Eas | | West | Nort | th Sou | th Total |
| Sta 7:00 | n rt) AM | 1 | WB 2 | N | IB 2 | SB 8 | 13 | 0 | 0 | N | IB D | 0 | 0 | 0 | | West 0 | Nort 0 | h Sou | th Total 0 |
| Sta 7:00 7:15 | art) AM 5 AM | 1 2 | WB 2 3 | N | 1B 2 6 | SB 8 8 | 13 19 | 0 0 | 0 0 | N | IB D D | 0 0 | 0 0 | 0 0 | | West 0 0 | Nort 0 0 | th Sou 0 0 | th Total 0 0 |
| Sta 7:00 7:15 7:30 | AM AM AM AM | 1 2 2 | WB 2 3 2 | | NB 2 6 8 | SB 8 8 5 | 13 19 17 | 0 0 0 | 0 0 0 | | IB D D D | 0 0 0 | 0 0 0 | 0 0 0 | | West 0 0 0 | Nort 0 0 0 | h Sou 0 0 0 | th Total 0 0 0 |
| Sta 7:00 7:15 7:30 7:45 | art 2 AM 5 AM 2 AM 5 AM | 1 2 2 2 | WB 2 3 2 4 | N | NB 2 6 8 8 | SB 8 5 13 | 13 19 17 27 | 0 0 0 0 | 0 0 0 0 | <u>N</u> | IB 0 0 0 0 0 | 0 0 0 0 | 0 0 0 0 | 0 0 0 0 | | West 0 0 0 0 | Nort 0 0 0 0 | h Sou 0 0 0 0 | th Total 0 0 0 0 |
| Sta 7:00 7:15 7:30 7:45 8:00 | 9 AM 5 AM 9 AM 9 AM 5 AM 9 AM | 1 2 2 2 3 | WB 2 3 2 4 7 | N | NB 2 6 8 8 8 6 | SB 8 5 13 14 | 13 19 17 27 30 | 0 0 0 0 | 0 0 0 0 0 | | IB D D D D D | 0 0 0 0 | 0 0 0 0 0 | 0 0 0 0 0 | | West 0 0 0 0 0 0 | Nort 0 0 0 0 0 | th Sou 0 0 0 0 0 | th Total 0 0 0 0 0 0 |
| Sta 7:00 7:15 7:30 7:45 | o AM 5 AM 5 AM 5 AM 5 AM 5 AM 5 AM | 1 2 2 2 3 0 | WB 2 3 2 4 7 7 | | IB 2 6 8 8 8 6 8 8 8 8 | SB 8 5 13 | 13 19 17 27 | 0 0 0 0 | 0 0 0 0 | | IB 0 0 0 0 0 | 0 0 0 0 | 0 0 0 0 | 0 0 0 0 | | West 0 0 0 0 | Nort 0 0 0 0 | h Sou 0 0 0 0 0 0 | th Total 0 0 0 0 0 0 0 |
| Sta 7:00 7:15 7:30 7:45 8:00 8:15 8:30 | o AM 5 AM 5 AM 5 AM 5 AM 5 AM 5 AM | 1 2 2 2 3 | WB 2 3 2 4 7 | | NB 2 6 8 8 8 6 | SB 8 5 13 14 11 | 13 19 17 27 30 26 | 0 0 0 0 0 0 | 0 0 0 0 0 0 | | IB 0 0 0 0 0 0 | 0 0 0 0 0 | 0 0 0 0 0 | 0 0 0 0 0 | | West 0 0 0 0 0 0 0 | Nort 0 0 0 0 0 | th Sou 0 0 0 0 0 | th Total 0 0 0 0 0 |
| Sta 7:00 7:15 7:30 7:45 8:00 8:15 8:30 | art art | 1 2 2 3 0 4 | WB 2 3 2 4 7 7 6 | N | IB 2 6 8 8 6 6 8 8 8 8 12 | SB 8 5 13 14 9 | 13 19 17 27 30 26 31 | 0 0 0 0 0 0 | 0 0 0 0 0 0 | | IB 0 0 0 0 0 0 0 | 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | 0 0 0 0 0 2 | | West 0 0 0 0 0 0 0 0 | Nort 0 0 0 0 0 0 0 | h Sou 0 0 0 0 0 0 0 | th Total 0 0 0 0 0 0 0 0 2 0 |

| In tan und | | 64th | Ave | | | 64th | Ave | | | Feder | al Blvd | | | Feder | al Blvd | | 15-min | Rolling |
|-------------------|----|-------|------|----|----|------|-------|----|----|-------|---------|----|----|-------|---------|----|--------|---------|
| Interval Start | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hou |
| Start | UT | LT | ΤН | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | Total | One nou |
| 7:00 AM | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 6 | 0 | 13 | 0 |
| 7:15 AM | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 5 | 1 | 0 | 1 | 7 | 0 | 19 | 0 |
| 7:30 AM | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 1 | 6 | 1 | 0 | 0 | 5 | 0 | 17 | 0 |
| 7:45 AM | 0 | 0 | 2 | 0 | 0 | 2 | 2 | 0 | 1 | 0 | 6 | 1 | 0 | 1 | 11 | 1 | 27 | 76 |
| 8:00 AM | 0 | 1 | 1 | 1 | 0 | 6 | 1 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 14 | 0 | 30 | 93 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 2 | 3 | 2 | 0 | 0 | 7 | 1 | 0 | 2 | 9 | 0 | 26 | 100 |
| 8:30 AM | 0 | 0 | 4 | 0 | 0 | 3 | 1 | 2 | 0 | 1 | 6 | 5 | 0 | 1 | 7 | 1 | 31 | 114 |
| 8:45 AM | 0 | 0 | 2 | 0 | 0 | 0 | 4 | 1 | 0 | 1 | 9 | 4 | 0 | 1 | 8 | 0 | 30 | 117 |
| Count Total | 0 | 1 | 11 | 4 | 0 | 13 | 13 | 10 | 1 | 3 | 47 | 13 | 0 | 8 | 67 | 2 | 193 | 0 |
| Peak Hour | 0 | 1 | 7 | 1 | 0 | 13 | 7 | 4 | 1 | 1 | 25 | 7 | 0 | 4 | 41 | 2 | 114 | 0 |
| Interval | | 64th | - | | | 64th | - | | | | al Blvd | | | | al Blvd | | 15-min | Rolling |
| Start | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hou |
| | LT | TI | H | RT | LT | Т | Ή | RT | LT | ٦ | Ή | RT | LT | T | Ή | RT | | |
| 7:00 AM | 0 | 0 |) | 0 | 0 | (| C | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 |) | 0 | 0 | (| C | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 |) | 0 | 0 | (| 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 |) | 0 | 0 | (| D | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | | 0 | 0 | | D | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | | 0 | 0 | | D | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 |) | 0 | 0 | | D | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Count Total | 0 | 0 | | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | 0 | | 0 | 0 | | D | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |

| Start Eastbound Westbound Northbound Southbound Total One Ho 4:00 PM 0 45 43 34 0 23 39 31 7 37 411 17 3 13 328 29 1,060 0 4:00 PM 0 56 48 31 0 27 56 18 7 40 426 16 1 11 290 37 1,064 0 4:45 PM 0 54 49 35 0 23 41 14 3 36 390 17 4 9 362 31 1,050 0 4:45 PM 0 54 49 35 0 24 50 16 3 39 407 23 3 8 325 29 1,065 4,239 5:00 PM 0 47 50 29 0 15 43 12 8 34 </th <th></th> <th></th> <th></th> <th>F</th> <th></th> <th>ral E h A</th> <th>3lvd ve</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>id</th> <th>Ж</th> <th></th> | | | | F | | ral E h A | 3lvd ve | | | | | | | | | | id | Ж | |
|--|--|---|--|---|---|--|---|---|---|---|---|--|--|--|---|--|---|--|--|
| 474 50 64h Ave 76h OB | | ¶ N | 4 | | <u>Pe</u> | eak H | <u>our</u> | | | | | С | | Perio | d: 4 | 4:00 P | M to | | |
| Interval Statt 64th Ave 64th Ave Federal Bivd Federal Bivd 15-min Southbound Rolling One Ho 4:00 PM 0 45 43 34 0 23 39 31 7 37 411 17 31 328 29 1.060 0 0 4:15 PM 0 56 48 31 0 27 56 18 7 40 426 16 1 11 290 37 1,064 0 4:30 PM 0 51 37 32 0 23 41 14 3 36 390 17 4 9 362 31 1,050 0 4:45 PM 0 54 49 35 0 24 50 16 3 390 12 0 38 325 29 1,065 4,239 5:00 PM 0 47 50 29 0 15 43 12 8 | | → 64 | 0 207 = 180 = 134 = | | | V: 4,3 F: 0.9 1 29 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 | | | 64 193 91 0 | < | 285 285 EB VB VB NB SB | 1.7% 3.2% 1.5% 2.0% | 0.94 0.86 0.96 0.89 | | | | | | |
| Interval Start Eastbound Westbound Northbound Southbound Total Rolling One Ho 4:00 PM 0 45 43 34 0 23 39 31 7 37 411 17 3 13 328 29 1,060 0 4:15 PM 0 56 48 31 0 27 56 18 7 40 426 16 1 11 290 37 1,064 0 4:45 PM 0 54 49 35 0 24 50 16 3 39 407 23 3 8 325 29 1,065 4,239 5:00 PM 0 46 46 36 0 17 4 43 17 3 7 338 21 1,065 4,239 5:00 PM 0 43 30 22 0 14 28 17 8 34 393 13< | Two-Hour | Count | - | | | | | | | | | | | | | | | | |
| 4:00 PM 0 45 43 34 0 23 39 31 7 37 411 17 3 13 328 29 1,060 0 4:15 PM 0 56 48 31 0 27 56 18 7 40 426 16 1 11 290 37 1,064 0 4:45 PM 0 51 37 32 0 23 41 14 3 36 390 17 4 9 362 31 1,060 0 4:45 PM 0 54 49 35 0 24 50 16 3 39 407 23 3 8 325 29 1,065 4,239 5:00 PM 0 46 46 36 0 17 46 16 5 33 430 12 13 318 26 1,031 4,277 5:30 PM 0 413 32 28 0 14 35 17 8 34 | i we near | Count | | | s | | | | | | | | | | | | | | - |
| 4:15 PM 0 56 48 31 0 27 56 18 7 40 426 16 1 11 290 37 1,064 0 4:30 PM 0 51 37 32 0 23 41 14 3 36 390 17 4 9 362 31 1,050 0 4:45 PM 0 54 49 35 0 24 50 16 3 39 407 23 3 8 325 29 1,065 4,239 5:00 PM 0 46 46 36 0 17 46 16 5 33 430 12 0 9 391 36 1,123 4,302 5:30 PM 0 43 30 22 0 14 28 16 0 41 426 100 2 13 318 261 1,314 4,296 6:30 PM 0 51 32 28 14 35 17 8 34 | Interval | | 64th Eastb | Ave bound | | | West | bound | | | North | nbound | | | South | nbound | | | Rolling One Hour |
| 4:30 PM 0 51 37 32 0 23 41 14 3 36 390 17 4 9 362 31 1,050 0 4:45 PM 0 54 49 35 0 24 50 16 3 39 407 23 3 8 325 29 1,065 4,393 5:00 PM 0 46 46 36 0 17 46 16 5 33 430 12 0 9 391 36 1,123 4,302 5:15 PM 0 47 50 29 0 15 43 12 8 34 434 17 3 7 338 21 1,058 4,296 5:30 PM 0 51 32 28 0 14 35 17 8 34 393 13 2 13 318 26 1,011 4,276 6unt Total 0 393 335 247 0 157 338 140 <th< td=""><td>Interval Start</td><td>UT</td><td>64th Eastb LT</td><td>o Ave bound TH</td><td>RT</td><td></td><td>West LT</td><td>bound TH</td><td></td><td></td><td>North LT</td><td>nbound TH</td><td>RT</td><td></td><td>South LT</td><td>nbound TH</td><td>RT</td><td>Total</td><td>One Hour</td></th<> | Interval Start | UT | 64th Eastb LT | o Ave bound TH | RT | | West LT | bound TH | | | North LT | nbound TH | RT | | South LT | nbound TH | RT | Total | One Hour |
| 5:00 PM 0 46 46 36 0 17 46 16 5 33 430 12 0 9 391 36 1,123 4,302 5:15 PM 0 47 50 29 0 15 43 12 8 34 434 17 3 7 338 21 1,058 4,296 5:30 PM 0 43 30 22 0 14 28 16 0 41 468 10 2 13 318 26 1,031 4,277 5:45 PM 0 51 32 28 0 14 35 17 8 34 393 13 2 13 272 22 934 4,146 Count Total 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 | Interval Start 4:00 PM | UT 0 | 64th Eastb LT 45 | o Ave bound TH 43 | RT 34 | 0 | West LT 23 | bound TH 39 | 31 | 7 | North LT 37 | nbound TH 411 | RT 17 | 3 | South LT 13 | nbound TH 328 | RT 29 | Total 1,060 | One Hour |
| 5:15 PM 0 47 50 29 0 15 43 12 8 34 434 17 3 7 338 21 1,058 4,296 5:30 PM 0 43 30 22 0 14 28 16 0 41 468 10 2 13 318 26 1,031 4,277 5:45 PM 0 51 32 28 0 14 35 17 8 34 393 13 2 13 318 26 1,031 4,277 5:45 PM 0 393 335 247 0 157 338 140 41 294 3,359 125 18 83 2,624 231 8,385 0 Peak AII 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 Peak MU 0 1 3 5 0 4 | Interval Start 4:00 PM 4:15 PM | UT 0 0 | 64th Eastb LT 45 56 | Ave bound TH 43 48 | RT 34 31 | 0 0 | West LT 23 27 | bound TH 39 56 | 31 18 | 7 7 | North LT 37 40 | nbound TH 411 426 | RT 17 16 | 3 1 | South LT 13 11 | nbound TH 328 290 | RT 29 37 | Total 1,060 1,064 | One Hour 0 0 |
| 5:30 PM 0 43 30 22 0 14 28 16 0 41 468 10 2 13 318 26 1,031 4,277 5:45 PM 0 51 32 28 0 14 35 17 8 34 393 13 2 13 318 26 1,031 4,277 5:45 PM 0 393 335 247 0 157 338 140 41 294 3,359 125 18 83 2,624 231 8,385 0 Peak All 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 Peak All 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall c | Interval Start 4:00 PM 4:15 PM 4:30 PM | UT 0 0 0 | 64th Eastb LT 45 56 51 | Ave bound TH 43 48 37 | RT 34 31 32 | 0 0 0 | West LT 23 27 23 | bound TH 39 56 41 | 31 18 14 | 7 7 3 | North LT 37 40 36 | 1000000 TH 411 426 390 | RT 17 16 17 | 3 1 4 | South LT 13 11 9 | nbound TH 328 290 362 | RT 29 37 31 | Total 1,060 1,064 1,050 | One Hour 0 0 |
| 5:45 PM 0 51 32 28 0 14 35 17 8 34 393 13 2 13 272 22 934 4,146 Count Total 0 393 335 247 0 157 338 140 41 294 3,359 125 18 83 2,624 231 8,385 0 Peak All 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 Peak HV 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 Howr Hv% 0 1 3% 3% 3% 0% 1% 1% 7% 0% 6 24 1 79 0 0 </td <td>Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM</td> <td>UT 0 0 0 0</td> <td>64th Eastb LT 45 56 51 54</td> <td>Ave bound TH 43 48 37 49</td> <td>RT 34 31 32 35</td> <td>0 0 0 0</td> <td>West LT 23 27 23 24</td> <td>bound TH 39 56 41 50</td> <td>31 18 14 16</td> <td>7 7 3 3</td> <td>North LT 37 40 36 39</td> <td>nbound TH 411 426 390 407</td> <td>RT 17 16 17 23</td> <td>3 1 4 3</td> <td>South LT 13 11 9 8</td> <td>TH 328 290 362 325</td> <td>RT 29 37 31 29</td> <td>Total 1,060 1,064 1,050 1,065</td> <td>One Hour 0 0</td> | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM | UT 0 0 0 0 | 64th Eastb LT 45 56 51 54 | Ave bound TH 43 48 37 49 | RT 34 31 32 35 | 0 0 0 0 | West LT 23 27 23 24 | bound TH 39 56 41 50 | 31 18 14 16 | 7 7 3 3 | North LT 37 40 36 39 | nbound TH 411 426 390 407 | RT 17 16 17 23 | 3 1 4 3 | South LT 13 11 9 8 | TH 328 290 362 325 | RT 29 37 31 29 | Total 1,060 1,064 1,050 1,065 | One Hour 0 0 |
| Count Total 0 393 335 247 0 157 338 140 41 294 3,359 125 18 83 2,624 231 8,385 0 Peak Hour All HV 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 Peak Hour HV 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 Hv% - 0% 2% 4% - 4% 3% 3% 0% 1% 7% 0% 16% 2% 1% 2% 0 Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. East West North South Total Start EB WB NB SB Total East< | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | UT 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 | Ave bound TH 43 48 37 49 46 | RT 34 31 32 35 36 | 0 0 0 0 | West LT 23 27 23 24 17 | bound TH 39 56 41 50 46 | 31 18 14 16 16 | 7 7 3 3 5 | North LT 37 40 36 39 33 | nbound TH 411 426 390 407 430 | RT 17 16 17 23 12 | 3 1 4 3 0 | South LT 13 11 9 8 9 | nbound TH 328 290 362 325 391 | RT 29 37 31 29 36 | Total 1,060 1,064 1,050 1,065 1,123 | One Hour 0 0 4,239 4,302 |
| All Hour 0 207 180 134 0 91 193 64 18 148 1,653 68 8 37 1,368 133 4,302 0 Hour HV 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 HV% - 0% 2% 4% - 4% 3% 3% 0% 1% 7% 0% 16% 2% 1% 2% 0 Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. East West North South Total Start EB WB NB SB Total EB WB NB SB Total East West North South Total 4:00 PM 5 8 8 5 26 0 0 0 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | UT 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 | Ave bound TH 43 48 37 49 49 46 50 | RT 34 31 32 35 36 29 | 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 | bound TH 39 56 41 50 46 43 | 31 18 14 16 16 12 | 7 7 3 3 5 8 | North LT 37 40 36 39 33 34 | nbound TH 411 426 390 407 430 434 | RT 17 16 17 23 12 17 | 3 1 4 3 0 3 | South LT 13 11 9 8 9 7 | nbound TH 328 290 362 325 391 338 | RT 29 37 31 29 36 21 | Total 1,060 1,064 1,050 1,065 1,123 1,058 | One Hour 0 0 4,239 4,302 4,296 |
| Peak Hour HV HV% 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 Mour HV% - 0% 2% 4% - 4% 3% 3% 0% 1% 7% 0% 16% 2% 1% 2% 0 Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. Pedestrians (Crossing Leg) Start EB WB NB SB Total EB WB NB SB Total East West North South Total 4:00 PM 5 8 8 5 26 0 <t< td=""><td>Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM</td><td>UT 0 0 0 0 0 0 0 0 0 0</td><td>64th Eastb LT 45 56 51 54 46 47 43 51</td><td>Ave bound TH 43 48 37 49 46 50 30 32</td><td>RT 34 31 32 35 36 29 22 28</td><td>0 0 0 0 0 0 0 0 0</td><td>West LT 23 27 23 24 17 15 14 14</td><td>bound TH 39 56 41 50 46 43 28 35</td><td>31 18 14 16 12 16 17</td><td>7 7 3 3 5 8 0</td><td>North LT 37 40 36 39 33 34 41 34</td><td>nbound TH 411 426 390 407 430 434 468 393</td><td>RT 17 16 17 23 12 17 10 13</td><td>3 1 4 3 0 3 2 2</td><td>South LT 13 11 9 8 9 7 13 13</td><td>nbound TH 328 290 362 325 391 338 318</td><td>RT 29 37 31 29 36 21 26 22</td><td>Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031</td><td>One Hour 0 0 4,239 4,206 4,296 4,277</td></t<> | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM | UT 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 | Ave bound TH 43 48 37 49 46 50 30 32 | RT 34 31 32 35 36 29 22 28 | 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 | bound TH 39 56 41 50 46 43 28 35 | 31 18 14 16 12 16 17 | 7 7 3 3 5 8 0 | North LT 37 40 36 39 33 34 41 34 | nbound TH 411 426 390 407 430 434 468 393 | RT 17 16 17 23 12 17 10 13 | 3 1 4 3 0 3 2 2 | South LT 13 11 9 8 9 7 13 13 | nbound TH 328 290 362 325 391 338 318 | RT 29 37 31 29 36 21 26 22 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 | One Hour 0 0 4,239 4,206 4,296 4,277 |
| Hour HV 0 1 3 5 0 4 5 2 0 2 21 5 0 6 24 1 79 0 HV% - 0% 2% 4% - 4% 3% 3% 0% 1% 1% 7% 0% 16% 2% 1% 2% 0 Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. Pedestrians (Crossing Leg) Interval Heavy Vehicle Totals Bicycles Pedestrians (Crossing Leg) Start EB WB NB SB Total East West North South Total 4:00 PM 5 8 8 5 26 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM Count Total | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 393 | Ave bound TH 43 48 37 49 46 50 30 32 335 | RT 34 31 32 35 36 29 22 28 247 | 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 | bound TH 39 56 41 50 46 43 28 35 338 | 31 18 14 16 12 16 17 140 | 7 7 3 3 5 8 0 8 41 | North LT 37 40 36 39 33 34 41 34 294 | nbound TH 411 426 390 407 430 434 468 393 3,359 | RT 17 16 17 23 12 17 10 13 125 | 3 1 4 3 0 3 2 2 18 | South LT 13 11 9 8 9 7 13 13 13 83 | nbound TH 328 290 362 325 391 338 318 272 2,624 | RT 29 37 31 29 36 21 26 22 231 | Total 1,060 1,064 1,050 1,065 1,058 1,031 934 8,385 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 |
| Note: Two-hour count summary volumes include heavy vehicles but exclude bicycles in overall count. Interval Start Heavy Vehicle Totals Bicycles Total East West North South Total 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:30 PM 4 3 10 7 24 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM Count Total Peak All | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 393 207 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 | RT 34 31 32 35 36 29 22 28 247 134 | 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 | bound TH 39 56 41 50 46 43 28 35 338 338 193 | 31 18 14 16 12 16 17 140 64 | 7 7 3 3 5 8 0 8 41 18 | North LT 37 40 36 39 33 34 41 34 294 148 | nbound TH 411 426 390 407 430 434 468 393 3,359 1,653 | RT 17 16 17 23 12 17 10 13 125 68 | 3 1 4 3 2 2 18 8 | South LT 13 11 9 8 9 7 13 13 83 37 | TH 328 290 362 325 391 338 318 272 2,624 1,368 | RT 29 37 31 29 36 21 26 22 231 133 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 |
| Interval Start Heavy Vehicle Totals Bicycles Pedestrians (Crossing Leg) 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:30 PM 3 3 9 11 26 0 <td< td=""><td>Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:30 PM 5:45 PM Count Total Peak All Hyur</td><td>UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1</td><td>Ave bound TH 43 48 37 49 46 50 30 32 335 180 3</td><td>RT 34 31 32 35 36 29 22 28 247 134 5</td><td>0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>West LT 23 27 23 24 17 15 14 15 14 157 91 4</td><td>bound TH 39 56 41 50 46 43 28 35 338 338 193 5</td><td>31 18 14 16 12 16 17 140 64 2</td><td>7 7 3 3 5 8 0 8 41 18 0</td><td>North LT 37 40 36 39 33 34 41 34 294 148 2</td><td>nbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21</td><td>RT 17 16 17 23 12 17 10 13 125 68 5</td><td>3 1 4 3 2 2 18 8 0</td><td>South LT 13 11 9 8 9 7 13 13 13 83 37 6</td><td>TH 328 290 362 325 391 338 318 272 2,624 1,368 24</td><td>RT 29 37 31 29 36 21 26 22 231 133 1</td><td>Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79</td><td>One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0</td></td<> | Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:30 PM 5:45 PM Count Total Peak All Hyur | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 | RT 34 31 32 35 36 29 22 28 247 134 5 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 15 14 157 91 4 | bound TH 39 56 41 50 46 43 28 35 338 338 193 5 | 31 18 14 16 12 16 17 140 64 2 | 7 7 3 3 5 8 0 8 41 18 0 | North LT 37 40 36 39 33 34 41 34 294 148 2 | nbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 | RT 17 16 17 23 12 17 10 13 125 68 5 | 3 1 4 3 2 2 18 8 0 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 | TH 328 290 362 325 391 338 318 272 2,624 1,368 24 | RT 29 37 31 29 36 21 26 22 231 133 1 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 |
| Start EB WB NB SB Total EB WB NB SB Total East West North South Total 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:00 PM 5 8 8 5 26 0 0 0 0 1 0 0 0 1 4:15 PM 3 3 9 11 26 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour HV | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% | RT 34 31 35 35 29 22 28 247 134 5 4% | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Westi LT 23 27 23 24 17 15 14 14 157 91 4 4% | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% | 31 18 14 16 12 16 17 140 64 2 3% | 7 3 3 5 8 0 8 41 18 0 % | North LT 37 40 36 39 33 34 41 34 294 148 2 1% | hbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% | RT 17 16 17 23 12 17 10 13 125 68 5 7% | 3 1 4 3 0 3 2 2 18 8 0 0% | South LT 13 11 9 8 9 7 13 13 13 83 37 6 | TH 328 290 362 325 391 338 318 272 2,624 1,368 24 | RT 29 37 31 29 36 21 26 22 231 133 1 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 |
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| 4:15 PM 3 3 9 11 26 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM Count Total Peak Hour HV HV% Note: Two-hou | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 393 207 1 0% Esumma Hea | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ry volu | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles I | 31 18 14 16 12 16 17 140 64 2 3% but excl | 7 7 3 5 8 0 8 41 18 0 0% ude bio | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i ycles | hbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal | RT 17 16 17 23 12 17 10 13 125 68 5 7% | 3 1 4 3 2 2 18 8 0 0% | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% | RT 29 37 31 29 36 21 26 22 231 133 1 1% | Total 1,060 1,064 1,055 1,055 1,058 1,031 934 8,385 4,302 79 2% ossing Le | One Hour 0 0 4,239 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 |
| 4:30 PM 4 3 10 7 24 0 | Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour HV HV% Note: Two-hou | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 393 207 1 0% summa tea WB | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ry volu volu | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc hicle To | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b | 31 18 14 16 12 16 17 140 64 2 3% but excl | 7 7 3 3 5 8 0 8 41 18 0 % ude bio | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB | hbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overall | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count | 3 1 4 3 2 2 18 8 0 0% Eas | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% edestria West | RT 29 37 31 29 36 21 26 22 231 133 1 1% | Total 1,060 1,064 1,055 1,055 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou | One Hour 0 0 0 4,239 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
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| 5:00 PM 0 0 4 6 10 0 0 0 0 1 0 1 0 2 2 3 14 0 0 0 0 0 0 0 3 0 2 0 5 5:15 PM 1 1 9 3 14 0 0 0 0 3 0 2 0 5 5:30 PM 1 1 5 4 11 0 0 0 0 0 3 2 0 5 5:30 PM 1 1 5 4 11 0 0 0 0 3 2 0 5 5:45 PM 3 4 6 9 22 0 0 0 0 0 4 0 0 4 | Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour Total Peak Hour Two-hou Interval Start 4:00 PM 4:15 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastb LT 45 56 51 54 46 47 43 51 393 207 1 0% summa tea WB 8 3 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ry volu | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc hicle To HB 8 9 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b thicles b 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl WB 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% Ude bio | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count Total 0 0 | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% West 0 0 0 | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 | Total 1,060 1,064 1,055 1,055 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 | One Hour 0 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 |
| 5:15 PM 1 1 9 3 14 0 0 0 0 3 0 2 0 5 5:30 PM 1 1 5 4 11 0 0 0 0 0 3 2 0 5 5:30 PM 1 1 5 4 11 0 0 0 0 0 3 2 0 5 5:45 PM 3 4 6 9 22 0 0 0 0 0 4 0 0 4 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM Count Total Peak Hour Peak Hour HV HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% * summa * s | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% http://www.encomester.com/ 3 2% 180 3 2% 180 3 2% 180 3 2% 180 19 10 10 10 10 10 10 10 10 10 10 10 10 10 | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes ind hicle To HB 8 9 9 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve Total 26 26 26 24 | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b thicles b C 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl WB 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 6 8 18 18 0% | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB 0 0 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count Total 0 0 0 0 | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 0 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% edestria West 0 0 0 0 | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 | Total 1,060 1,064 1,055 1,055 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 0 | One Hour 0 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |
| 5:30 PM 1 1 5 4 11 0 0 0 0 0 3 2 0 5 5:45 PM 3 4 6 9 22 0 0 0 0 0 4 0 0 4 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour Peak Hour HV HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:45 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% summa * summa * * * * * * * * * * * * * * * * * * | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ry volu | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc hicle To HB 8 9 10 5 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve Total 26 26 26 24 19 | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b thicles b C 0 0 0 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl 0 0 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 0% 0% Bic: | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB 0 0 0 0 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count Total 0 0 0 0 0 0 | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 0 0 0 0 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% edestria West 0 0 0 0 0 | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 1 | Total 1,060 1,064 1,055 1,055 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 0 0 0 | One Hour 0 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 1 |
| 5:45 PM 3 4 6 9 22 0 0 0 0 0 4 0 0 4 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour Peak Hour All HV HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:30 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% summa esumma B 8 3 3 3 5 0 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ry volu vy Ver 5 N | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes ind hicle To HB 8 9 10 5 4 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 15 14 14 157 91 4 4% eavy ve Eavy ve Total 26 26 26 24 19 10 | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b EB 0 0 0 0 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl 0 0 0 0 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 0% 0% 0% 5 N | North LT 37 40 36 39 33 34 41 34 294 148 2 1% Cycles i Vycles NB 0 0 0 0 0 0 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count // count | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 0 0 1 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% edestria West 0 0 0 0 0 0 | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 1 1 | Total 1,060 1,064 1,055 1,055 1,031 934 8,385 4,302 79 2% 0 0 0 0 0 0 0 0 0 0 0 0 0 | One Hour 0 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 1 2 |
| | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour Peak Hour All HV HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 4:30 PM 5:15 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 393 207 1 0% summa * summa * * * * | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ary volu volu | RT 34 31 32 35 29 22 28 247 134 5 4% mes inc incle To IB 8 9 10 5 4 9 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 157 91 4 4% eavy ve Total 26 26 26 26 24 19 10 14 | bound TH 39 56 41 50 46 43 28 35 338 193 5 3% thicles b EB 0 0 0 0 0 0 0 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl 0 0 0 0 0 0 0 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 0% 0% Bic: | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB 0 0 0 0 0 0 0 0 0 0 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count Total 0 0 0 0 0 0 0 0 0 | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 0 0 1 3 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 1 1 2 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 1 2 5 |
| | Interval Start 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak Hour HV HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% e summa c summa 8 8 3 3 5 0 1 1 1 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ary volu avy Vel 5 N | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc incle To IB 8 9 10 5 4 9 5 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 14 15 14 14 157 91 4 % eavy ve Total 26 26 26 24 19 10 14 11 | bound TH 39 56 41 50 46 43 28 35 338 193 5 338 193 5 3% bhicles b bhicles b 0 0 0 0 0 0 0 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl WB 0 0 0 0 0 0 0 0 0 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 0% 0% 0% | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles NB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | bound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 0 0 0 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% // count Total 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 3 1 4 3 2 2 18 8 0 0% Eas 1 0 0 0 1 3 0 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% 2% edestria West 0 0 0 0 0 0 0 0 0 3 | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 1 1 2 2 2 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | One Hour 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 1 0 1 0 1 2 5 5 |
| Peak Hour 9 11 28 31 79 0 0 0 0 0 1 0 2 0 3 | Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM Count Total Peak HOU HV% Note: Two-hou Interval Start 4:00 PM 4:15 PM 4:30 PM 4:30 PM 5:15 PM 5:30 PM 5:15 PM 5:30 PM 5:15 PM | UT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 64th Eastt LT 45 56 51 54 46 47 43 51 393 207 1 0% 5 summa c summa 8 8 3 3 5 0 1 1 1 4 | Ave bound TH 43 48 37 49 46 50 30 32 335 180 3 2% ary volu vy Vet 5 N | RT 34 31 32 35 36 29 22 28 247 134 5 4% mes inc nicle To IB 8 9 10 5 4 9 5 6 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | West LT 23 27 23 24 17 15 14 15 14 14 157 91 4 % eavy ve Total 26 26 24 19 10 14 11 22 | bound TH 39 56 41 50 46 43 28 35 338 193 5 338 193 5 33% bhicles b bhicles b 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 31 18 14 16 12 16 17 140 64 2 3% but excl WB 0 0 0 0 0 0 0 0 0 0 0 0 0 | 7 7 3 3 5 8 0 8 41 18 0 0% 0% 0% 0% | North LT 37 40 36 39 33 34 41 34 294 148 2 1% cycles i vycles i vycles 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | hbound TH 411 426 390 407 430 434 468 393 3,359 1,653 21 1% n overal SB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | RT 17 16 17 23 12 17 10 13 125 68 5 7% Il count Total 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 3 1 4 3 2 2 18 8 0 0% 5 5 5 6 6 7 7 7 7 8 8 0 0% 5 7 7 7 8 8 0 0% 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | South LT 13 11 9 8 9 7 13 13 13 83 37 6 16% | bound TH 328 290 362 325 391 338 318 272 2,624 1,368 24 2% | RT 29 37 31 29 36 21 26 22 231 133 1 1% ans (Cr Nort 0 0 0 0 1 1 2 2 0 | Total 1,060 1,064 1,050 1,065 1,123 1,058 1,031 934 8,385 4,302 79 2% ossing Le th Sou 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | One Hour 0 0 0 0 4,239 4,302 4,296 4,277 4,146 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 0 1 2 5 5 4 |

| Interval | | 64th | Ave | | | 64th | Ave | | | Feder | al Blvd | | | Federa | al Blvd | | 15-min | Rolling |
|-------------|----|-------|------|----|----|------|-------|----|----|-------|---------|----|----|--------|---------|----|--------|---------|
| Start | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hou |
| otart | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | Total | one nou |
| 4:00 PM | 0 | 0 | 3 | 2 | 0 | 1 | 2 | 5 | 0 | 0 | 5 | 3 | 0 | 1 | 4 | 0 | 26 | 0 |
| 4:15 PM | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 2 | 6 | 1 | 0 | 2 | 8 | 1 | 26 | 0 |
| 4:30 PM | 0 | 0 | 2 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 7 | 3 | 0 | 2 | 5 | 0 | 24 | 0 |
| 4:45 PM | 0 | 0 | 1 | 1 | 0 | 2 | 2 | 1 | 0 | 0 | 5 | 0 | 0 | 1 | 6 | 0 | 19 | 95 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 1 | 5 | 0 | 10 | 79 |
| 5:15 PM | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 5 | 1 | 0 | 0 | 2 | 1 | 14 | 67 |
| 5:30 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 3 | 0 | 0 | 0 | 4 | 0 | 11 | 54 |
| 5:45 PM | 0 | 0 | 2 | 1 | 0 | 1 | 1 | 2 | 0 | 1 | 4 | 1 | 0 | 2 | 7 | 0 | 22 | 57 |
| Count Total | 0 | 1 | 10 | 8 | 0 | 7 | 8 | 10 | 0 | 8 | 38 | 10 | 0 | 9 | 41 | 2 | 152 | 0 |
| Peak Hour | 0 | 1 | 3 | 5 | 0 | 4 | 5 | 2 | 0 | 2 | 21 | 5 | 0 | 6 | 24 | 1 | 79 | 0 |
| Interval | | 0.000 | Ave | | | | Ave | | | | al Blvd | | | | al Blvd | | 15-min | Rolling |
| Start | | Eastb | ound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hou |
| otart | LT | Т | Н | RT | LT | Т | Ή | RT | LT | ٦ | Ή | RT | LT | Т | Ή | RT | Total | |
| 4:00 PM | 0 | (|) | 0 | 0 | (| 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | (|) | 0 | 0 | (| 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | (|) | 0 | 0 | (| 0 | 0 | 0 | | 0 | 0 | 0 | (| 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | (| נ | 0 | 0 | (| 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | | כ | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | |) | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | (| - | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | |) | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Count Total | 0 | |) | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |
| Peak Hour | 0 | (| 1 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 |



APPENDIX B

Future Traffic Projections

Kimley »Horn

| CDOT O | TIS: QT 42 | 270 | | | | | | | |
|--------|------------|----------|--------|-------|--------|------------|-------------|-----|---|
| ROUTE | REFPT | ENDREFPT | LENGTH | AADT | AADTYR | YR20FACTOR | GROWTH RATE | DHV | LOCATION |
| 287C | 286.913 | 287.803 | 0.843 | 33000 | 2022 | 1.16 | 0.74% | 10 | ON SH 287 FEDERAL BLVD N/O I-76 DENVER |
| 287C | 287.803 | 288.815 | 0.999 | 33000 | 2022 | 1.19 | 0.87% | 10 | ON SH 287 FEDERAL BLVD S/O 72ND AVE WESTMINSTER |
| | | | | | | AVERAGE | 0.81% | | |



APPENDIX C

Trip Generation Worksheets

Kimley »Horn

Trip Generation Planner (ITE 11th Edition) - Summary Report

Kimley **»Horn**

Weekday Trip Generation Trips Based on Average Rates/Equations Project Name QT 4270 Project Number 196140009

| | | | | | | | Rates | | | | Т | otal Tri | os | | | | Net Tr | ips aft | er Inter | nal Cap | oture | | Ne | t Trips a | after Int | ternal C | apture & | & Pass- | Ву |
|---------------------------------------|-------------------------------|-------------------------|------------------------|--------|---------------|---------|------------|-------|--------|-------------|-------------|-------------|--------------|-----|--------------|----------------|-------------|---------|----------|---------|-------|--------------|-------|-------------|-------------|-------------|-------------|---------|--------------|
| | | In day an day (| | No. of | Avg | Deilu | | DM | Deilu | | DM | AM | AM | PM | PM | Deile | | DM | AM | AM | PM | PM | Deilu | | DM | AM | AM Trips | PM | PM |
| ITE Internal Capture Land Code Use | Land Use Description | Independent Variable | Setting/Location | | Rate or Eq | | AM Rate | Rate | Trips | AM Trips | PM Trips | Trips In | Trips Out | | Trips Out | Daily Trips | AM Trips | | Trips | Out | | Trips Out | | AM Trips | PM Trips | Trips In | Out | In | Trips Out |
| 110 Office | General Light Industrial | 1,000 Sq Ft | General Urban/Suburban | 37.92 | Eq | N/A | N/A | N/A | 194 | 30 | 20 | 26 | 4 | 2 | 18 | 178 | 29 | 18 | 25 | 4 | 2 | 17 | 178 | 29 | 18 | 25 | 4 | 2 | 17 |
| 934 Restaurant | Fast-Food Restaurant w/ D.T. | 1,000 Sq Ft | General Urban/Suburban | 5.2 | Avg | 467.48 | 44.61 | 33.03 | 2,432 | 232 | 172 | 118 | 114 | 89 | 83 | 2,237 | 227 | 158 | 116 | 112 | 82 | 76 | 1,006 | 114 | 71 | 58 | 56 | 37 | 34 |
| 945 Retail | Convenience Store/Gas Station | 1,000 Sq Ft | General Urban/Suburban | 5.312 | Avg | 1283.38 | 91.35 | 78.95 | 6,818 | 485 | 419 | 242 | 243 | 209 | 210 | 6,273 | 475 | 385 | 237 | 238 | 192 | 193 | 1,568 | 114 | 96 | 57 | 57 | 48 | 48 |
| 948 Retail | Automated Car Wash | Car Wash Tunnel(s) | General Urban/Suburban | 1 | Avg | * | * | 77.50 | 780 | 78 | 78 | 39 | 39 | 39 | 39 | 718 | 76 | 72 | 38 | 38 | 36 | 36 | 718 | 76 | 72 | 38 | 38 | 36 | 36 |
| | | | | | | | Grand | Total | 10,224 | 825 | 689 | 425 | 400 | 339 | 350 | 9,406 | 808 | 634 | 417 | 392 | 312 | 322 | 3,470 | 333 | 257 | 179 | 155 | 123 | 134 |
| | | | | | | | | | | | | | | | | 92% | 98% | 92% | 98% | 98% | 92% | 92% | | | | | | | |

| Project QT 4270 Subject Trip Generation for General Li | aht Industrial | |
|---|--|----------|
| Designed by TES Date Checked by Date | November 01, 2023 Job No. 096888037 | <u> </u> |
| TRIP GENERATION MANUAL TECHNIQU | <u>ES</u> | |
| ITE <u>Trip Generation Manual</u> 11th Edition, Fi | | |
| Land Use Code - General Light Industrial (1 | 10) | |
| Independent Variable - 1000 Square Feet G Gross Floor Area = 37,9 X = 37.9 T = Average Vehicle Trip Ends | | |
| Peak Hour of Adjacent Street Traffic, One | Hour Between 7 and 9 a.m. (100 Series Page 32) | |
| Average Weekday T = 0.68(X) + 3.81 T = 0.68 * 38 + 3.81 | Directional Distribution: 88% ent. 12% exit. T = 30 Average Vehicle Trip Ends 26 entering 4 exiting | |
| (*) TRI | 26 + 4 = 30 P END WAS CHANGED BY 1 TO SATISFY THE TOTAL | |
| Peak Hour of Adjacent Street Traffic, One | Hour Between 4 and 6 p.m. (100 Series Page 33) | |
| Average Weekday Ln(T) = 0.72 Ln(X) + 0.38 Ln(T) = 0.72 * Ln(38) + 0.38 | Directional Distribution: 14% ent. 86% exit. T = 20 Average Vehicle Trip Ends 2 entering 17 exiting | |
| | 2 + 18 = 20 | |
| <u>Weekday (100 Series Page 31)</u> | | |
| Daily Weekday T = 3.76 (X) + 50.47 (T) = 3.76 * 37.92 + 50.47 | Directional Distribution: 50% entering, 50% exiting T = 194 Average Vehicle Trip Ends 97 entering 97 exiting | |
| | 97 + 97 = 194 | |

| Project (| | | | |
|-------------------------------------|-------------------------|--------------------|----------------|--|
| | | | | Restaurant with Drive-Through Window |
| Designed by | | IE2 | | te November 01, 2023 Job No. 09688037 te Sheet No. of |
| Checked by | | | Date | te Sheet No of |
| TRIP GENER | ATION | MANUAL T | ECHNIQUE | <u>:S</u> |
| ITE <u>Trip Gene</u> | ration N | <u>Ianual</u> 11th | n Edition, Ave | erage Rates |
| Land Use Cod | e - Fas | t-Food Res | taurant with | Drive-Through Window (934) |
| T = Avera | 5,20 .200 age Vel | 00 hicle Trip E | nds |) Hour Between 7 and 9 a.m. (900 Series Page 726) |
| | Aujace | | | Directional Distribution: 51% ent. 49% exit. |
| (T) = 44.61 (X) | | | | T = 232 Average Vehicle Trip Ends |
| (T) = 44.61 * | | (5.2) | | 118 entering 114 exiting |
| | | . , | | |
| | | | | 118 + 114 = 232 |
| | | | | |
| Peak Hour of | Adjace | ent Street | raffic, One | Hour Between 4 and 6 p.m. (900 Series Page 727) |
| | | | | Directional Distribution: 52% ent. 48% exit. |
| (T) = 33.03 (X) | | | | T = 172 Average Vehicle Trip Ends |
| (T) = 33.03 * | | (5.2) | | 89 entering 83 exiting |
| | | | | |
| | | | | 89 + 83 = 172 |
| Weekday (900 | Sorio | - Dago 725 | 3 | |
| Weekday (500 | J Ocnes | 5 Taye 120 | <u>u</u> | |
| | | | | Directional Distribution: 50% ent. 50% exit. |
| (T) = 467.48 (λ | <) | | | T = 2432 Average Vehicle Trip Ends |
| (T) = 467.48 * | | (5.2) | | 1216 entering 1216 exiting |
| | | | | 4040 . 4040 0400 |
| | | | | 1216 + 1216 = 2432 |
| Non Pass-Bv | Trip Va | olumes (Pe | er ITE Trip G | Generation Manual, 11th Edition) |
| AM Peak Hour | | | -Pass By | PM Peak Hour = 45% Non-Pass By |
| | IN | Out | Total | |
| AM Peak | 58 | 56 | 114 | |
| PM Peak | 37 | 34 | 71 | |
| Daily | 503 | 503 | 1006 | PM Peak Hour Rate Applied to Daily |
| Pass-Ry Trin | Volum | as (Par Tri | n Generatia | on Manual, 11th Edition) |
| <u>Pass-by I пр</u> AM Peak Hour | | 50% Pas | | PM Peak Hour = 55% Pass By |
| | - IN | Out | Total | |
| | | | 114 | |
| AM Peak | 58 | 56 | 114 | |
| AM Peak PM Peak | 58 45 | 56 42 | 87 | |

| Project QT 4270 | | |
|---|---|---|
| Subject Trip Generation for Conv Designed by TES Checked by | venience Store/Gas Station - VFP (1 Date November 01, 2023 Date | Job No. <u>096888037</u> Sheet No. <u>of</u> |
| TRIP GENERATION MANUAL TECH | NIQUES | |
| ITE Trip Generation Manual 11th Editi | on, Average Rate Equations | |
| Land Use Code - Convenience Store/C | Gas Station - VFP (16-24) (945) | |
| Independent Variable - 1,000 Square I | Feet (X) | |
| SF= 5,312 X = 5.312 T = Average Vehicle Trip Ends | | |
| Peak Hour of Adjacent Street Traffic | c, One Hour Between 7 and 9 a.m. | <u>. (900 Series page 901)</u> |
| Average Weekday T = 91.35 (X) T = 91.35 * 5.312 | Directional Distribution T = 485 Aver 242 entering | : 50% ent. 50% exit. rage Vehicle Trip Ends 243 exiting |
| | 242 + 243 | = 485 |
| Peak Hour of Adjacent Street Traffic | c, One Hour Between 4 and 6 p.m. | . (900 Series page 902) |
| Average Weekday T = 78.95 (X) T = 78.95 * 5.312 | Directional Distribution T = 419 Aven 209 entering | rage Vehicle Trip Ends |
| | 209 + 210 | = 419 |
| <u>Weekday (900 Series page 900)</u> | | |
| Average Weekday T = 1283.38 (X) T = 1283.38 * 5.312 | T = 6818 Ave | : 50% entering, 50% exiting rage Vehicle Trip Ends 3409 exiting |
| | 3409 + 3409 | = 6818 |
| Non Pass-By Trip Volumes (Per ITEPM Peak Hour =25%Non-PassINOutTotaAM Peak5757114PM Peak484896 | By AM Peak Hour = 24% al 4 | <u>ition)</u> Non-Pass By |
| Daily 784 784 156 | 8 PM Peak Hour Rate Applied | d to Daily |
| Pass-By Trip Volumes (Per ITE TripPM Peak Hour =75%Pass ByINOutTotaAM Peak180181361PM Peak144145285 | AM Peak Hour = 76% al 9 | Pass By |
| Daily 2352 2352 470 | 5 PM Peak Hour Rate Applied | d to Daily |

| TRIP GENERATION MANUAL TECHNIQUESITE Trip Generation Manual 11th Edition, Average Rate EquationsLand Use Code - Automated Car Wash (948)Independent Variable - Number of Car Wash Tunnels (X) # of Car Wash Tunnels = 1 X = 1.0 T = Average Vehicle Trip EndsDirectional Distribution: 50% ent. 50% exit. T = 77.50(X) T = 77.50(X) T = 77.50(X)Directional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingDirectional Distribution: 50% ent. 50% exit. T = 780 Average Vehicle Trip Ends 390 entering 390 exiting | Designed byTES Checked by | Date Date | November 01, 2023 | Job No. Sheet No. | 09688037 of |
|---|------------------------------------|----------------|------------------------|----------------------|-----------------|
| Land Use Code - Automated Car Wash (948)Independent Variable - Number of Car Wash Tunnels (X) # of Car Wash Tunnels = 1 X = 1.0 T = Average Vehicle Trip EndsPeak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. (Utilized PM Peak Hour Rates) $T = 77.50(X)$ T = 77.50 * 1Directional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingPeak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Directional Distribution: 50% ent. 50% exit. T = 77.50 * 1Directional Distribution: 50% ent. 50% exit. T = 78 Average Vehicle Trip Ends 39 entering 39 exitingWeekday (10% K-Factor from PM Peak Hour)Average WeekdayDirectional Distribution: 50% ent. 50% exit. T = 780 Average Vehicle Trip Ends | TRIP GENERATION MANUAL TEC | <u>HNIQUES</u> | | | |
| Independent Variable - Number of Car Wash Tunnels (X) # of Car Wash Tunnels = 1 X = 1.0 T = Average Vehicle Trip EndsPeak Hour of Adjacent Street Traffic, One Hour Between 7 and 9 a.m. (Utilized PM Peak Hour Rates)T = 77.50(X) T = 77.50 * 1Directional Distribution: 50% ent. 50% exit. T = 78Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)T = 77.50(X) T = 78Average Vehicle Trip Ends 39T = 77.50(X) T = 77.50 * 1T = 78 39Average Vehicle Trip Ends 39exitingWeekday (10% K-Factor from PM Peak Hour)Average WeekdayDirectional Distribution: 50% ent. 50% exit. T = 780Average Vehicle Trip Ends | ITE Trip Generation Manual 11th Ed | ition, Avera | ge Rate Equations | | |
| # of Car Wash Tunnels =1 $X = 1.0$ TT = Average Vehicle Trip EndsDirectional Distribution: 50% ent. 50% exit.T = 77.50(X)T =T = 77.50 *1Directional Distribution: 50% ent. 50% exit.T = 77.50(X)T =T = 77.50 *1Directional Distribution: 50% ent. 50% exit.T = 77.50(X)T =T = 77.50 *1Directional Distribution: 50% ent. 50% exit.T = 77.50 *1Directional Distribution: 50% ent. 50% exit.T = 78Average Vehicle Trip Ends 39 entering 39 exitingWeekday (10% K-Factor from PM Peak Hour)Average WeekdayDirectional Distribution: 50% ent. 50% exit. T =T = 780Average Vehicle Trip Ends | Land Use Code - Automated Car Wa | ash (948) | | | |
| T = 77.50(X) T = 77.50 * 1Directional Distribution:50% ent.50% exit.T = 78Average Vehicle Trip Ends 39exitingPeak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Directional Distribution:50% ent.50% exit.T = 77.50(X) T = 77.50 * 1T = 78 39Average Vehicle Trip Ends 39exit.Weekday (10% K-Factor from PM Peak Hour)Directional Distribution:50% ent.50% exit.Average WeekdayDirectional Distribution:50% ent.50% exit.T = 780Average Vehicle Trip Ends50% exit.T = 780 Average Vehicle Trip Ends | # of Car Wash Tunnels = X = 1.0 | | nnels (X) | | |
| T = 77.50(X) T = 77.50 *T = 78 39Average Vehicle Trip Ends 39Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)Peak Hour of Adjacent Street Traffic, One Hour Between 4 and 6 p.m. (900 Series Page 931)T = 77.50(X) | Peak Hour of Adjacent Street Traf | fic, One Ho | ur Between 7 and 9 a.r | n. (Utilized PM Pe | eak Hour Rates) |
| T = 77.50(X) T = 77.50 *Directional Distribution: T = 7850% ent. 50% ent. 50% exit. T = 78Weekday (10% K-Factor from PM Peak Hour) Average WeekdayDirectional Distribution: T = 78050% ent. 50% ent. 50% exit. T = 780 | | | T = 78 Ave | erage Vehicle Trip | |
| T = 77.50(X) T = 77.50 *T = 78 39Average Vehicle Trip Ends 39Weekday (10% K-Factor from PM Peak Hour)Directional Distribution:50%ent.50%exit.Average WeekdayDirectional Distribution:50%ent.50%exit.T=780Average Vehicle Trip Ends | Peak Hour of Adjacent Street Traf | fic, One Ho | ur Between 4 and 6 p.ı | n. (900 Series Pa | <u>ge 931)</u> |
| Average WeekdayDirectional Distribution:50% ent.50% exit.T =780Average Vehicle Trip Ends | | | T = 78 Ave | erage Vehicle Trip | |
| T = 780 Average Vehicle Trip Ends | Weekday (10% K-Factor from PM F | Peak Hour) | | | |
| | Average Weekday | | | | |
| | (T) = PM Peak Total / K Factor | 0.1 | | • | Ends |
| 390 + 390 = 780 | | | 390 + 390 | = 780 | |



APPENDIX D

Intersection Analysis Worksheets

Kimley »Horn

Timings 1: Federal Blvd (US-287) & 64th Ave

| | ≯ | - | \rightarrow | 4 | - | • | 1 | 1 | - \ | . ↓ | |
|----------------------|-------|----------|---------------|-------|----------|-------|-------|----------|------------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ۲ | † | 1 | ۲ | † | 1 | ľ | ^ | ۲ | ተተኈ | |
| Traffic Volume (vph) | 91 | 105 | 152 | 95 | 80 | 29 | 66 | 745 | 70 | 1607 | |
| Future Volume (vph) | 91 | 105 | 152 | 95 | 80 | 29 | 66 | 745 | 70 | 1607 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 11.0 | 24.0 | 24.0 | 23.0 | 36.0 | 36.0 | 12.0 | 35.0 | 38.0 | 61.0 | |
| Total Split (%) | 9.2% | 20.0% | 20.0% | 19.2% | 30.0% | 30.0% | 10.0% | 29.2% | 31.7% | 50.8% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 80

Control Type: Actuated-Coordinated

Splits and Phases: 1: Federal Blvd (US-287) & 64th Ave

| ▶ _{Ø1} | 🚽 🕈 ø2 (R) | √ Ø3 | <i>4</i> ∞4 |
|-----------------|------------|-------------|-------------|
| 38 s | 35 s | 23 s | 24 s |
| ▲ Ø5 🕹 Ø6 (R) | • | | 3 |
| 12 s 61 s | | 11 s 36 s | |

HCM 6th Signalized Intersection Summary 1: Federal Blvd (US-287) & 64th Ave

| | ≯ | + | \mathbf{F} | 4 | + | • | 1 | 1 | 1 | 1 | ţ | ~ |
|------------------------------|-----------|-----------|--------------|-----------|-----------|-----------|-------|-------------|-----------|----------|-------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ↑ | 1 | <u>۲</u> | ↑ | 1 | ሻ | <u>ተተ</u> ጮ | | <u>۲</u> | <u>ተተ</u> ጮ | |
| Traffic Volume (veh/h) | 91 | 105 | 152 | 95 | 80 | 29 | 66 | 745 | 44 | 70 | 1607 | 102 |
| Future Volume (veh/h) | 91 | 105 | 152 | 95 | 80 | 29 | 66 | 745 | 44 | 70 | 1607 | 102 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1722 | 1722 | 1722 | 1841 | 1841 | 1841 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 99 | 114 | 165 | 103 | 87 | 32 | 72 | 810 | 48 | 76 | 1747 | 111 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 12 | 12 | 12 | 4 | 4 | 4 | 3 | 3 | 3 |
| Cap, veh/h | 267 | 228 | 193 | 240 | 260 | 220 | 206 | 2762 | 163 | 436 | 2774 | 176 |
| Arrive On Green | 0.04 | 0.12 | 0.12 | 0.07 | 0.15 | 0.15 | 0.04 | 0.57 | 0.57 | 0.04 | 0.57 | 0.57 |
| Sat Flow, veh/h | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 4853 | 287 | 1767 | 4868 | 309 |
| Grp Volume(v), veh/h | 99 | 114 | 165 | 103 | 87 | 32 | 72 | 558 | 300 | 76 | 1211 | 647 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 1675 | 1789 | 1767 | 1689 | 1800 |
| Q Serve(g_s), s | 5.0 | 6.9 | 12.3 | 6.5 | 5.4 | 2.3 | 2.0 | 10.3 | 10.4 | 2.1 | 28.9 | 29.0 |
| Cycle Q Clear(g_c), s | 5.0 | 6.9 | 12.3 | 6.5 | 5.4 | 2.3 | 2.0 | 10.3 | 10.4 | 2.1 | 28.9 | 29.0 |
| Prop In Lane | 1.00 | 000 | 1.00 | 1.00 | 0 (0 | 1.00 | 1.00 | 4007 | 0.16 | 1.00 | 1001 | 0.17 |
| Lane Grp Cap(c), veh/h | 267 | 228 | 193 | 240 | 260 | 220 | 206 | 1907 | 1018 | 436 | 1924 | 1025 |
| V/C Ratio(X) | 0.37 | 0.50 | 0.85 | 0.43 | 0.34 | 0.15 | 0.35 | 0.29 | 0.29 | 0.17 | 0.63 | 0.63 |
| Avail Cap(c_a), veh/h | 267 | 278 | 236 | 359 | 431 | 365 | 228 | 1907 | 1018 | 839 | 1924 | 1025 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.7 | 49.2 | 51.6 | 42.0 | 45.6 | 44.2 | 14.6 | 13.4 | 13.4 | 10.2 | 17.3 | 17.3 |
| Incr Delay (d2), s/veh | 0.9 | 1.7 | 21.7 | 1.2 | 0.8 | 0.3 | 1.0 | 0.4 | 0.7 | 0.2 | 1.6 | 2.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 2.7 | 3.3 | 6.0 | 2.7 | 2.4 | 0.8 | 0.8 | 3.9 | 4.3 | 0.8 | 11.2 | 12.4 |
| Unsig. Movement Delay, s/veh | | FO 0 | 70.0 | 12.2 | 4/ 2 | 44.5 | 1 Г / | 107 | 1/1 | 10 / | 10.0 | 20.2 |
| LnGrp Delay(d),s/veh | 45.6 D | 50.9 D | 73.3 E | 43.2 D | 46.3 D | 44.5 D | 15.6 | 13.7 B | 14.1 B | 10.4 | 18.9 B | 20.3 |
| LnGrp LOS | D | | E | D | | D | B | | Б | В | | <u> </u> |
| Approach Vol, veh/h | | 378 | | | 222 | | | 930 | | | 1934 | |
| Approach Delay, s/veh | | 59.3 | | | 44.6 | | | 14.0 | | | 19.0 | |
| Approach LOS | | E | | | D | | | В | | | В | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.6 | 74.3 | 14.4 | 20.7 | 10.5 | 74.4 | 11.0 | 24.1 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | 29.0 | 17.0 | 18.0 | 6.0 | 55.0 | 5.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 4.1 | 12.4 | 8.5 | 14.3 | 4.0 | 31.0 | 7.0 | 7.4 | | | | |
| Green Ext Time (p_c), s | 0.2 | 5.3 | 0.1 | 0.4 | 0.0 | 15.2 | 0.0 | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 23.7 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

| | ≯ | - | \rightarrow | 1 | + | • | 1 | 1 | - \ | . ↓ | |
|----------------------|-------|----------|---------------|-------|----------|-------|-------|----------|------------|----------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ľ | † | 1 | ľ | † | 1 | ľ | ^ | ۲ | ^ | |
| Traffic Volume (vph) | 207 | 180 | 134 | 91 | 193 | 64 | 166 | 1653 | 45 | 1368 | |
| Future Volume (vph) | 207 | 180 | 134 | 91 | 193 | 64 | 166 | 1653 | 45 | 1368 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 22.0 | 25.0 | 25.0 | 22.0 | 25.0 | 25.0 | 21.0 | 58.0 | 15.0 | 52.0 | |
| Total Split (%) | 18.3% | 20.8% | 20.8% | 18.3% | 20.8% | 20.8% | 17.5% | 48.3% | 12.5% | 43.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 80

Control Type: Actuated-Coordinated

| Ø1 | <1 _{@2 (R)} | √ Ø3 | ₽ 04 |
|---------|----------------------|-------------|-------------|
| 15 s | 58 s | 22 s | 25 s |
| ▲ Ø5 | 🖉 🗸 🖉 Ø6 (R) | ▶ Ø1 | |
| 21 s | 52 s | 22 s | 25 s |

| | ۶ | + | * | 4 | + | • | • | 1 | 1 | * | ţ | ~ |
|------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--------------|-----------|-----------|--------------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | ↑ | 1 | <u>٦</u> | ↑ | 1 | <u>۲</u> | <u> ተ</u> ተጮ | | <u>۲</u> | <u> ተተ</u> ኑ | |
| Traffic Volume (veh/h) | 207 | 180 | 134 | 91 | 193 | 64 | 166 | 1653 | 68 | 45 | 1368 | 133 |
| Future Volume (veh/h) | 207 | 180 | 134 | 91 | 193 | 64 | 166 | 1653 | 68 | 45 | 1368 | 133 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1856 | 1856 | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 216 | 188 | 140 | 95 | 201 | 67 | 173 | 1722 | 71 | 47 | 1425 | 139 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 295 | 346 | 293 | 266 | 235 | 199 | 266 | 2620 | 108 | 190 | 2305 | 225 |
| Arrive On Green | 0.12 | 0.18 | 0.18 | 0.06 | 0.13 | 0.13 | 0.07 | 0.52 | 0.52 | 0.03 | 0.49 | 0.49 |
| Sat Flow, veh/h | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 5030 | 207 | 1781 | 4730 | 461 |
| Grp Volume(v), veh/h | 216 | 188 | 140 | 95 | 201 | 67 | 173 | 1165 | 628 | 47 | 1025 | 539 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 1702 | 1833 | 1781 | 1702 | 1787 |
| Q Serve(g_s), s | 12.2 | 10.9 | 9.5 | 5.5 | 12.7 | 4.7 | 5.8 | 29.9 | 30.0 | 1.6 | 26.5 | 26.5 |
| Cycle Q Clear(g_c), s | 12.2 | 10.9 | 9.5 | 5.5 | 12.7 | 4.7 | 5.8 | 29.9 | 30.0 | 1.6 | 26.5 | 26.5 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.11 | 1.00 | | 0.26 |
| Lane Grp Cap(c), veh/h | 295 | 346 | 293 | 266 | 235 | 199 | 266 | 1773 | 955 | 190 | 1659 | 871 |
| V/C Ratio(X) | 0.73 | 0.54 | 0.48 | 0.36 | 0.85 | 0.34 | 0.65 | 0.66 | 0.66 | 0.25 | 0.62 | 0.62 |
| Avail Cap(c_a), veh/h | 321 | 346 | 293 | 394 | 294 | 249 | 370 | 1773 | 955 | 265 | 1659 | 871 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 38.2 | 44.3 | 43.7 | 41.9 | 51.3 | 47.8 | 19.4 | 20.9 | 20.9 | 17.6 | 22.6 | 22.6 |
| Incr Delay (d2), s/veh | 7.6 | 1.7 | 1.2 | 0.8 | 17.8 | 1.0 | 2.7 | 1.9 | 3.5 | 0.7 | 1.7 | 3.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 5.9 | 5.2 | 3.8 | 2.5 | 7.1 | 1.9 | 2.5 | 12.1 | 13.4 | 0.7 | 10.8 | 11.7 |
| Unsig. Movement Delay, s/veh | 45.8 | 46.1 | 44.9 | 42.7 | 69.1 | 48.8 | 22.1 | 22.9 | 24.5 | 18.3 | 24.3 | 25.9 |
| LnGrp Delay(d),s/veh | 45.8 D | 40.1 D | 44.9 D | 42.7 D | 09.1 E | 48.8 D | 22.1 C | 22.9 C | 24.5 C | 18.3 B | 24.3 C | 25.9 C |
| LnGrp LOS | D | | D | D | | D | C | | C | D | | |
| Approach Vol, veh/h | | 544 | | | 363 | | | 1966 | | | 1611 | |
| Approach Delay, s/veh | | 45.7 | | | 58.4 | | | 23.3 | | | 24.6 | |
| Approach LOS | | D | | | E | | | С | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.0 | 68.5 | 13.3 | 28.2 | 14.0 | 64.5 | 20.3 | 21.2 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 52.0 | 16.0 | 19.0 | 15.0 | 46.0 | 16.0 | 19.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 3.6 | 32.0 | 7.5 | 12.9 | 7.8 | 28.5 | 14.2 | 14.7 | | | | |
| Green Ext Time (p_c), s | 0.0 | 13.0 | 0.1 | 0.8 | 0.3 | 10.3 | 0.1 | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 29.3 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ሻ | ↑ | 1 | ሻ | ↑ | 1 | ሻ | ተተኈ | ሻ | ተተኈ | |
| Traffic Volume (vph) | 93 | 108 | 156 | 97 | 82 | 30 | 68 | 763 | 72 | 1646 | |
| Future Volume (vph) | 93 | 108 | 156 | 97 | 82 | 30 | 68 | 763 | 72 | 1646 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 11.0 | 24.0 | 24.0 | 23.0 | 36.0 | 36.0 | 12.0 | 35.0 | 38.0 | 61.0 | |
| Total Split (%) | 9.2% | 20.0% | 20.0% | 19.2% | 30.0% | 30.0% | 10.0% | 29.2% | 31.7% | 50.8% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 80

Control Type: Actuated-Coordinated

| Ø1 | 🗖 🗖 ø2 (R) | √ Ø3 | ₩ Ø4 | |
|---------------|------------|-------------------|-------------|--|
| 38 s | 35 s | 23 s | 24 s | |
| ▲ Ø5 🕨 Ø6 (R) | | ▶ _{Ø7} 🛟 | 28 | |
| 12 s 61 s | | 11 s 36 s | | |

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|------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-------------|-----------|-----------|--------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | ↑ | 1 | ሻ | ↑ | 1 | <u>۲</u> | <u></u> ↑↑₽ | | <u>۲</u> | <u> ተተ</u> ኑ | |
| Traffic Volume (veh/h) | 93 | 108 | 156 | 97 | 82 | 30 | 68 | 763 | 45 | 72 | 1646 | 104 |
| Future Volume (veh/h) | 93 | 108 | 156 | 97 | 82 | 30 | 68 | 763 | 45 | 72 | 1646 | 104 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1722 | 1722 | 1722 | 1841 | 1841 | 1841 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 101 | 117 | 170 | 105 | 89 | 33 | 74 | 829 | 49 | 78 | 1789 | 113 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 12 | 12 | 12 | 4 | 4 | 4 | 3 | 3 | 3 |
| Cap, veh/h | 270 | 233 | 198 | 243 | 266 | 226 | 200 | 2743 | 162 | 426 | 2754 | 174 |
| Arrive On Green | 0.04 | 0.13 | 0.13 | 0.07 | 0.15 | 0.15 | 0.04 | 0.57 | 0.57 | 0.04 | 0.57 | 0.57 |
| Sat Flow, veh/h | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 4853 | 286 | 1767 | 4870 | 307 |
| Grp Volume(v), veh/h | 101 | 117 | 170 | 105 | 89 | 33 | 74 | 571 | 307 | 78 | 1239 | 663 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 1675 | 1789 | 1767 | 1689 | 1800 |
| Q Serve(g_s), s | 5.0 | 7.1 | 12.7 | 6.6 | 5.5 | 2.3 | 2.1 | 10.7 | 10.8 | 2.2 | 30.2 | 30.4 |
| Cycle Q Clear(g_c), s | 5.0 | 7.1 | 12.7 | 6.6 | 5.5 | 2.3 | 2.1 | 10.7 | 10.8 | 2.2 | 30.2 | 30.4 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.16 | 1.00 | | 0.17 |
| Lane Grp Cap(c), veh/h | 270 | 233 | 198 | 243 | 266 | 226 | 200 | 1893 | 1011 | 426 | 1910 | 1018 |
| V/C Ratio(X) | 0.37 | 0.50 | 0.86 | 0.43 | 0.33 | 0.15 | 0.37 | 0.30 | 0.30 | 0.18 | 0.65 | 0.65 |
| Avail Cap(c_a), veh/h | 270 | 278 | 236 | 360 | 431 | 365 | 221 | 1893 | 1011 | 829 | 1910 | 1018 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.5 | 48.9 | 51.4 | 41.6 | 45.2 | 43.9 | 15.5 | 13.7 | 13.7 | 10.4 | 17.9 | 17.9 |
| Incr Delay (d2), s/veh | 0.9 | 1.7 | 23.0 | 1.2 | 0.7 | 0.3 | 1.1 | 0.4 | 0.8 | 0.2 | 1.7 | 3.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 2.8 | 3.4 | 6.3 | 2.8 | 2.4 | 0.9 | 0.9 | 4.1 | 4.5 | 0.9 | 11.8 | 13.1 |
| Unsig. Movement Delay, s/veh | | FO / | 744 | 40.0 | 45.0 | 110 | 1// | 1/1 | 14 Г | 10 / | 10 / | 21.2 |
| LnGrp Delay(d),s/veh | 45.3 D | 50.6 D | 74.4 E | 42.8 D | 45.9 D | 44.2 D | 16.6 В | 14.1 B | 14.5 B | 10.6 B | 19.6 B | 21.2 |
| LnGrp LOS | D | | E | D | | D | D | | D | D | | С |
| Approach Vol, veh/h | | 388 | | | 227 | | | 952 | | | 1980 | |
| Approach Delay, s/veh | | 59.7 | | | 44.2 D | | | 14.4 | | | 19.8 D | |
| Approach LOS | | E | | | D | | | В | | | В | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.6 | 73.8 | 14.5 | 21.1 | 10.6 | 73.9 | 11.0 | 24.6 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | 29.0 | 17.0 | 18.0 | 6.0 | 55.0 | 5.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 4.2 | 12.8 | 8.6 | 14.7 | 4.1 | 32.4 | 7.0 | 7.5 | | | | |
| Green Ext Time (p_c), s | 0.2 | 5.3 | 0.1 | 0.4 | 0.0 | 15.0 | 0.0 | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 24.3 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ሻ | ↑ | 1 | ሻ | ↑ | 1 | ሻ | ተተኈ | ሻ | <u>ተ</u> ተጮ | |
| Traffic Volume (vph) | 212 | 184 | 137 | 93 | 198 | 66 | 170 | 1693 | 46 | 1402 | |
| Future Volume (vph) | 212 | 184 | 137 | 93 | 198 | 66 | 170 | 1693 | 46 | 1402 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 22.0 | 25.0 | 25.0 | 22.0 | 25.0 | 25.0 | 21.0 | 58.0 | 15.0 | 52.0 | |
| Total Split (%) | 18.3% | 20.8% | 20.8% | 18.3% | 20.8% | 20.8% | 17.5% | 48.3% | 12.5% | 43.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 80

Control Type: Actuated-Coordinated

| Ø1 | <1 _{@2 (R)} | √ Ø3 | ₽ 04 |
|---------|----------------------|-------------|-------------|
| 15 s | 58 s | 22 s | 25 s |
| ▲ Ø5 | 🖉 🗸 🖉 Ø6 (R) | ▶ Ø1 | |
| 21 s | 52 s | 22 s | 25 s |

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|------------------------------|----------|----------|--------------|----------|----------|------|----------|-------------|------|----------|--------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | ↑ | 1 | <u>۲</u> | ↑ | 1 | <u>۲</u> | <u>ተተ</u> ጮ | | <u>۲</u> | <u> ተተ</u> ኑ | |
| Traffic Volume (veh/h) | 212 | 184 | 137 | 93 | 198 | 66 | 170 | 1693 | 70 | 46 | 1402 | 136 |
| Future Volume (veh/h) | 212 | 184 | 137 | 93 | 198 | 66 | 170 | 1693 | 70 | 46 | 1402 | 136 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1856 | 1856 | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 221 | 192 | 143 | 97 | 206 | 69 | 177 | 1764 | 73 | 48 | 1460 | 142 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 299 | 353 | 299 | 269 | 240 | 203 | 261 | 2596 | 107 | 183 | 2277 | 221 |
| Arrive On Green | 0.12 | 0.19 | 0.19 | 0.06 | 0.13 | 0.13 | 0.07 | 0.52 | 0.52 | 0.03 | 0.48 | 0.48 |
| Sat Flow, veh/h | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 5029 | 208 | 1781 | 4732 | 460 |
| Grp Volume(v), veh/h | 221 | 192 | 143 | 97 | 206 | 69 | 177 | 1193 | 644 | 48 | 1050 | 552 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 1702 | 1833 | 1781 | 1702 | 1788 |
| Q Serve(g_s), s | 12.5 | 11.1 | 9.7 | 5.6 | 13.0 | 4.8 | 5.9 | 31.3 | 31.4 | 1.6 | 27.8 | 27.8 |
| Cycle Q Clear(g_c), s | 12.5 | 11.1 | 9.7 | 5.6 | 13.0 | 4.8 | 5.9 | 31.3 | 31.4 | 1.6 | 27.8 | 27.8 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.11 | 1.00 | | 0.26 |
| Lane Grp Cap(c), veh/h | 299 | 353 | 299 | 269 | 240 | 203 | 261 | 1757 | 946 | 183 | 1638 | 860 |
| V/C Ratio(X) | 0.74 | 0.54 | 0.48 | 0.36 | 0.86 | 0.34 | 0.68 | 0.68 | 0.68 | 0.26 | 0.64 | 0.64 |
| Avail Cap(c_a), veh/h | 320 | 353 | 299 | 395 | 294 | 249 | 362 | 1757 | 946 | 258 | 1638 | 860 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 37.9 | 44.0 | 43.4 | 41.6 | 51.2 | 47.6 | 20.7 | 21.6 | 21.6 | 18.3 | 23.4 | 23.4 |
| Incr Delay (d2), s/veh | 8.2 | 1.7 | 1.2 | 0.8 | 18.6 | 1.0 | 3.1 | 2.1 | 3.9 | 0.7 | 1.9 | 3.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 6.1 | 5.3 | 3.9 | 2.5 | 7.3 | 1.9 | 2.6 | 12.7 | 14.2 | 0.7 | 11.4 | 12.4 |
| Unsig. Movement Delay, s/veh | | 45.0 | | 10.1 | (0.0 | 40 F | 00.0 | 00.0 | 05 (| 10.1 | 05.0 | 07.0 |
| LnGrp Delay(d),s/veh | 46.2 | 45.8 | 44.6 | 42.4 | 69.8 | 48.5 | 23.8 | 23.8 | 25.6 | 19.1 | 25.3 | 27.0 |
| LnGrp LOS | D | D | D | D | E | D | С | C | С | В | C | <u> </u> |
| Approach Vol, veh/h | | 556 | | | 372 | | | 2014 | | | 1650 | |
| Approach Delay, s/veh | | 45.6 | | | 58.7 | | | 24.4 | | | 25.7 | _ |
| Approach LOS | | D | | | E | | | С | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.0 | 67.9 | 13.5 | 28.6 | 14.2 | 63.7 | 20.5 | 21.5 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 52.0 | 16.0 | 19.0 | 15.0 | 46.0 | 16.0 | 19.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 3.6 | 33.4 | 7.6 | 13.1 | 7.9 | 29.8 | 14.5 | 15.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 12.6 | 0.1 | 0.8 | 0.3 | 10.1 | 0.1 | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 30.2 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ٦ | † | 1 | ሻ | † | 1 | ሻ | ተተኈ | ሻ | ተተኈ | |
| Traffic Volume (vph) | 86 | 163 | 144 | 281 | 88 | 53 | 100 | 803 | 261 | 1527 | |
| Future Volume (vph) | 86 | 163 | 144 | 281 | 88 | 53 | 100 | 803 | 261 | 1527 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 11.0 | 24.0 | 24.0 | 23.0 | 36.0 | 36.0 | 12.0 | 35.0 | 38.0 | 61.0 | |
| Total Split (%) | 9.2% | 20.0% | 20.0% | 19.2% | 30.0% | 30.0% | 10.0% | 29.2% | 31.7% | 50.8% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | 🗖 🗖 ø2 (R) | √ Ø3 | ₩ Ø4 | |
|---------------|------------|-------------------|-------------|--|
| 38 s | 35 s | 23 s | 24 s | |
| ▲ Ø5 🕨 Ø6 (R) | | ▶ _{Ø7} 🛟 | 28 | |
| 12 s 61 s | | 11 s 36 s | | |

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|--|------------|--------------|-------------|-------------|------------|------------|-------------|-------------|------------|-------------|--------------|-------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | <u>†</u> | 1 | <u> </u> | <u>†</u> | 1 | <u></u> | ተተጮ | | <u></u> | ተተጮ | |
| Traffic Volume (veh/h) | 86 | 163 | 144 | 281 | 88 | 53 | 100 | 803 | 52 | 261 | 1527 | 97 |
| Future Volume (veh/h) | 86 | 163 | 144 | 281 | 88 | 53 | 100 | 803 | 52 | 261 | 1527 | 97 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1 0 0 | 1.00 | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 105/ | No | 105/ | 1700 | No | 1700 | 1041 | No | 1041 | 105/ | No 1057 | 105/ |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1722 | 1722 | 1722 | 1841 | 1841 | 1841 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h Peak Hour Factor | 93 0.92 | 177 0.92 | 157 0.92 | 305 0.92 | 96 0.92 | 58 0.92 | 109 0.92 | 873 0.92 | 57 0.92 | 284 0.92 | 1660 0.92 | 105 0.92 |
| Percent Heavy Veh, % | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Cap, veh/h | 280 | 221 | 188 | 318 | 378 | 320 | 207 | 2076 | 135 | 433 | 2382 | 151 |
| Arrive On Green | 0.04 | 0.12 | 0.12 | 0.14 | 0.22 | 0.22 | 0.05 | 0.43 | 0.43 | 0.11 | 0.49 | 0.49 |
| Sat Flow, veh/h | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 4820 | 314 | 1767 | 4870 | 308 |
| Grp Volume(v), veh/h | 93 | 177 | 157 | 305 | 96 | 58 | 109 | 606 | 324 | 284 | 1151 | 614 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 1675 | 1784 | 1767 | 1689 | 1800 |
| Q Serve(g_s), s | 5.0 | 11.1 | 11.7 | 17.0 | 5.5 | 3.9 | 4.1 | 15.1 | 15.2 | 10.2 | 31.7 | 31.7 |
| Cycle Q Clear(g_c), s | 5.0 | 11.1 | 11.7 | 17.0 | 5.5 | 3.9 | 4.1 | 15.1 | 15.2 | 10.2 | 31.7 | 31.7 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.18 | 1.00 | | 0.17 |
| Lane Grp Cap(c), veh/h | 280 | 221 | 188 | 318 | 378 | 320 | 207 | 1443 | 768 | 433 | 1652 | 881 |
| V/C Ratio(X) | 0.33 | 0.80 | 0.84 | 0.96 | 0.25 | 0.18 | 0.53 | 0.42 | 0.42 | 0.66 | 0.70 | 0.70 |
| Avail Cap(c_a), veh/h | 280 | 278 | 236 | 318 | 431 | 365 | 208 | 1443 | 768 | 713 | 1652 | 881 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 44.6 | 51.4 | 51.7 | 41.0 | 38.7 | 38.1 | 21.6 | 23.7 | 23.8 | 16.5 | 23.7 | 23.8 |
| Incr Delay (d2), s/veh | 0.7 | 12.2 | 18.7 | 39.6 | 0.4 | 0.3 | 2.4 | 0.9 | 1.7 | 1.7 | 2.5 | 4.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 2.5 | 5.9 | 5.6 | 5.0 | 2.4 | 1.4 | 1.8 | 6.1 | 6.7 | 4.2 | 12.9 | 14.3 |
| Unsig. Movement Delay, s/veh | | (a m | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 45.3 | 63.7 | 70.4 | 80.6 | 39.1 | 38.3 | 24.0 | 24.6 | 25.5 | 18.1 | 26.2 | 28.3 |
| LnGrp LOS | D | E | E | F | D | D | С | C | С | В | C | C |
| Approach Vol, veh/h | | 427 | | | 459 | | | 1039 | | | 2049 | |
| Approach Delay, s/veh | | 62.1 | | | 66.6 | | | 24.8 | | | 25.7 | |
| Approach LOS | | E | | | E | | | С | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 19.0 | 57.7 | 23.0 | 20.3 | 12.0 | 64.7 | 11.0 | 32.3 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | 29.0 | 17.0 | 18.0 | 6.0 | 55.0 | 5.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 12.2 | 17.2 | 19.0 | 13.7 | 6.1 | 33.7 | 7.0 | 7.5 | | | | |
| Green Ext Time (p_c), s | 0.8 | 4.8 | 0.0 | 0.6 | 0.0 | 13.3 | 0.0 | 0.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 34.1 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

| | ٦ | - | \mathbf{r} | 4 | - | • | 1 | Ť | 1 | Ļ | |
|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------------|-------|-------------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ሻ | † | 1 | ሻ | ↑ | 1 | ሻ | <u>ተተ</u> ኑ | ሻ | <u>ተተ</u> ጮ | |
| Traffic Volume (vph) | 203 | 224 | 131 | 206 | 203 | 92 | 197 | 1723 | 155 | 1342 | |
| Future Volume (vph) | 203 | 224 | 131 | 206 | 203 | 92 | 197 | 1723 | 155 | 1342 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 22.0 | 25.0 | 25.0 | 22.0 | 25.0 | 25.0 | 21.0 | 58.0 | 15.0 | 52.0 | |
| Total Split (%) | 18.3% | 20.8% | 20.8% | 18.3% | 20.8% | 20.8% | 17.5% | 48.3% | 12.5% | 43.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | <1 _{@2 (R)} | √ Ø3 | ₽ 04 |
|---------|----------------------|-------------|-------------|
| 15 s | 58 s | 22 s | 25 s |
| ▲ Ø5 | ♥ ♥ Ø6 (R) | ▶ Ø1 | |
| 21 s | 52 s | 22 s | 25 s |

| | ≯ | → | \mathbf{F} | 4 | + | • | • | 1 | 1 | 1 | ţ | ~ |
|--|-------------|-----------|--------------|-----------|-----------|-----------|-----------|--------------|------------|-----------|-------------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ↑ | 1 | <u> </u> | ↑ | 1 | ሻ | <u>ተተ</u> ጮ | | <u>۲</u> | <u>ተተ</u> ጮ | |
| Traffic Volume (veh/h) | 203 | 224 | 131 | 206 | 203 | 92 | 197 | 1723 | 72 | 155 | 1342 | 130 |
| Future Volume (veh/h) | 203 | 224 | 131 | 206 | 203 | 92 | 197 | 1723 | 72 | 155 | 1342 | 130 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 1070 | No | 1070 | 105/ | No | 105/ | 1070 | No | 1070 | 1070 | No | 1070 |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1856 | 1856 | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 211 0.96 | 233 | 136 | 215 | 211 | 96 | 205 | 1795 0.96 | 75 0.96 | 161 | 1398 | 135 |
| Peak Hour Factor Percent Heavy Veh, % | 0.96 | 0.96 2 | 0.96 2 | 0.96 3 | 0.96 3 | 0.96 3 | 0.96 2 | 0.96 | 0.96 | 0.96 2 | 0.96 2 | 0.96 2 |
| Cap, veh/h | 306 | 266 | 226 | 292 | 269 | 228 | 279 | 2382 | 2 99 | 219 | 2174 | 210 |
| Arrive On Green | 0.12 | 0.14 | 0.14 | 0.12 | 0.14 | 0.14 | 0.08 | 0.47 | 0.47 | 0.06 | 0.46 | 0.46 |
| Sat Flow, veh/h | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 5027 | 210 | 1781 | 4735 | 457 |
| Grp Volume(v), veh/h | 211 | 233 | 136 | 215 | 211 | 96 | 205 | 1215 | 655 | 161 | 1005 | 528 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 1702 | 1833 | 1781 | 1702 | 1788 |
| Q Serve(g_s), s | 11.9 | 14.6 | 9.7 | 12.3 | 13.2 | 6.7 | 7.2 | 35.0 | 35.1 | 5.7 | 27.2 | 27.2 |
| Cycle Q Clear(g_c), s | 11.9 | 14.6 | 9.7 | 12.3 | 13.2 | 6.7 | 7.2 | 35.0 | 35.1 | 5.7 | 27.2 | 27.2 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | 10.2 | 1.00 | 1.00 | 0010 | 0.11 | 1.00 | | 0.26 |
| Lane Grp Cap(c), veh/h | 306 | 266 | 226 | 292 | 269 | 228 | 279 | 1613 | 868 | 219 | 1563 | 821 |
| V/C Ratio(X) | 0.69 | 0.88 | 0.60 | 0.74 | 0.78 | 0.42 | 0.73 | 0.75 | 0.75 | 0.74 | 0.64 | 0.64 |
| Avail Cap(c_a), veh/h | 335 | 296 | 251 | 316 | 294 | 249 | 361 | 1613 | 868 | 238 | 1563 | 821 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 38.2 | 50.4 | 48.3 | 38.3 | 49.5 | 46.7 | 21.8 | 25.8 | 25.9 | 24.6 | 24.9 | 24.9 |
| Incr Delay (d2), s/veh | 5.3 | 22.6 | 3.4 | 8.1 | 12.1 | 1.2 | 5.5 | 3.3 | 6.0 | 10.4 | 2.0 | 3.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%), veh/In | 5.7 | 8.5 | 4.0 | 6.0 | 7.0 | 2.7 | 3.3 | 14.6 | 16.4 | 2.9 | 11.2 | 12.2 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 43.4 | 73.0 | 51.6 | 46.4 | 61.6 | 48.0 | 27.2 | 29.1 | 31.9 | 35.1 | 27.0 | 28.8 |
| LnGrp LOS | D | E | D | D | E | D | С | C | С | D | C | C |
| Approach Vol, veh/h | | 580 | | | 522 | | | 2075 | | | 1694 | |
| Approach Delay, s/veh | | 57.2 | | | 52.8 | | | 29.8 | | | 28.3 | |
| Approach LOS | | E | | | D | | | С | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 13.7 | 62.9 | 20.4 | 23.1 | 15.5 | 61.1 | 20.1 | 23.4 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 52.0 | 16.0 | 19.0 | 15.0 | 46.0 | 16.0 | 19.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.7 | 37.1 | 14.3 | 16.6 | 9.2 | 29.2 | 13.9 | 15.2 | | | | |
| Green Ext Time (p_c), s | 0.1 | 10.8 | 0.1 | 0.4 | 0.3 | 9.9 | 0.1 | 0.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 35.0 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ሻ | † | 1 | ሻ | † | 1 | ሻ | ተተኈ | ሻ | ተተኈ | |
| Traffic Volume (vph) | 109 | 125 | 182 | 113 | 96 | 35 | 79 | 890 | 84 | 1919 | |
| Future Volume (vph) | 109 | 125 | 182 | 113 | 96 | 35 | 79 | 890 | 84 | 1919 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 11.0 | 24.0 | 24.0 | 23.0 | 36.0 | 36.0 | 12.0 | 35.0 | 38.0 | 61.0 | |
| Total Split (%) | 9.2% | 20.0% | 20.0% | 19.2% | 30.0% | 30.0% | 10.0% | 29.2% | 31.7% | 50.8% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | 🗖 🗖 ø2 (R) | √ Ø3 | ₩ Ø4 | |
|---------------|------------|-------------------|-------------|--|
| 38 s | 35 s | 23 s | 24 s | |
| ▲ Ø5 🕨 Ø6 (R) | | ▶ _{Ø7} 🛟 | 28 | |
| 12 s 61 s | | 11 s 36 s | | |

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|------------------------------|------|----------|------|----------|----------|------|------|-------------|------|----------|-------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦. | ↑ | 1 | <u>۲</u> | ↑ | 1 | ሻ | <u>ተተ</u> ጮ | | <u>۲</u> | <u>ተተ</u> ኑ | |
| Traffic Volume (veh/h) | 109 | 125 | 182 | 113 | 96 | 35 | 79 | 890 | 53 | 84 | 1919 | 122 |
| Future Volume (veh/h) | 109 | 125 | 182 | 113 | 96 | 35 | 79 | 890 | 53 | 84 | 1919 | 122 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1722 | 1722 | 1722 | 1841 | 1841 | 1841 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 118 | 136 | 198 | 123 | 104 | 38 | 86 | 967 | 58 | 91 | 2086 | 133 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 12 | 12 | 12 | 4 | 4 | 4 | 3 | 3 | 3 |
| Cap, veh/h | 291 | 263 | 223 | 262 | 309 | 262 | 161 | 2614 | 156 | 362 | 2626 | 167 |
| Arrive On Green | 0.04 | 0.14 | 0.14 | 0.08 | 0.18 | 0.18 | 0.04 | 0.54 | 0.54 | 0.04 | 0.54 | 0.54 |
| Sat Flow, veh/h | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 4848 | 290 | 1767 | 4868 | 309 |
| Grp Volume(v), veh/h | 118 | 136 | 198 | 123 | 104 | 38 | 86 | 668 | 357 | 91 | 1443 | 776 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 1675 | 1788 | 1767 | 1689 | 1800 |
| Q Serve(g_s), s | 5.0 | 8.1 | 14.8 | 7.5 | 6.3 | 2.6 | 2.6 | 13.8 | 13.8 | 2.7 | 41.3 | 41.8 |
| Cycle Q Clear(g_c), s | 5.0 | 8.1 | 14.8 | 7.5 | 6.3 | 2.6 | 2.6 | 13.8 | 13.8 | 2.7 | 41.3 | 41.8 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.16 | 1.00 | | 0.17 |
| Lane Grp Cap(c), veh/h | 291 | 263 | 223 | 262 | 309 | 262 | 161 | 1806 | 964 | 362 | 1822 | 971 |
| V/C Ratio(X) | 0.41 | 0.52 | 0.89 | 0.47 | 0.34 | 0.14 | 0.53 | 0.37 | 0.37 | 0.25 | 0.79 | 0.80 |
| Avail Cap(c_a), veh/h | 291 | 278 | 236 | 364 | 431 | 365 | 180 | 1806 | 964 | 763 | 1822 | 971 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 43.5 | 47.7 | 50.6 | 39.2 | 43.0 | 41.5 | 24.3 | 15.9 | 15.9 | 12.2 | 22.2 | 22.4 |
| Incr Delay (d2), s/veh | 0.9 | 1.6 | 30.0 | 1.3 | 0.6 | 0.3 | 2.7 | 0.6 | 1.1 | 0.4 | 3.6 | 6.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 3.2 | 3.9 | 7.7 | 3.1 | 2.8 | 1.0 | 1.4 | 5.4 | 5.9 | 1.1 | 16.6 | 18.8 |
| Unsig. Movement Delay, s/veh | | 40.0 | 00 (| 10 (| 40 (| 41 7 | 07.0 | 1/ 5 | 17.0 | 10 F | 25.0 | 20.0 |
| LnGrp Delay(d),s/veh | 44.4 | 49.3 | 80.6 | 40.6 | 43.6 | 41.7 | 27.0 | 16.5 | 17.0 | 12.5 | 25.9 | 29.2 |
| LnGrp LOS | D | D | F | D | D | D | С | В | В | В | C | <u> </u> |
| Approach Vol, veh/h | | 452 | | | 265 | | | 1111 | | | 2310 | |
| Approach Delay, s/veh | | 61.7 | | | 41.9 | | | 17.5 | | | 26.5 | |
| Approach LOS | | E | | | D | | | В | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.8 | 70.7 | 15.5 | 23.0 | 10.7 | 70.7 | 11.0 | 27.6 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | 29.0 | 17.0 | 18.0 | 6.0 | 55.0 | 5.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 4.7 | 15.8 | 9.5 | 16.8 | 4.6 | 43.8 | 7.0 | 8.3 | | | | |
| Green Ext Time (p_c), s | 0.2 | 5.7 | 0.2 | 0.2 | 0.0 | 9.5 | 0.0 | 0.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 28.9 | | | | | | | | | |
| HCM 6th LOS | | | С | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ሻ | † | 1 | ሻ | † | 1 | ሻ | ተተኈ | ሻ | ተተኈ | |
| Traffic Volume (vph) | 247 | 215 | 160 | 109 | 230 | 76 | 198 | 1974 | 54 | 1634 | |
| Future Volume (vph) | 247 | 215 | 160 | 109 | 230 | 76 | 198 | 1974 | 54 | 1634 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 22.0 | 25.0 | 25.0 | 22.0 | 25.0 | 25.0 | 21.0 | 58.0 | 15.0 | 52.0 | |
| Total Split (%) | 18.3% | 20.8% | 20.8% | 18.3% | 20.8% | 20.8% | 17.5% | 48.3% | 12.5% | 43.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | <1 _{@2 (R)} | √ Ø3 | ₽ 04 |
|---------|----------------------|-------------|-------------|
| 15 s | 58 s | 22 s | 25 s |
| ▲ Ø5 | ♥ ♥ Ø6 (R) | ▶ Ø1 | |
| 21 s | 52 s | 22 s | 25 s |

| | ۶ | - | \mathbf{F} | ∢ | - | • | 1 | Ť | 1 | 1 | ţ | ∢ |
|------------------------------|----------|-----------|--------------|----------|-----------|-----------|----------|-----------|------|------|--------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | ↑ | 1 | <u>۲</u> | ↑ | 1 | <u>۲</u> | ተተጮ | | - ሽ | 4 41> | |
| Traffic Volume (veh/h) | 247 | 215 | 160 | 109 | 230 | 76 | 198 | 1974 | 81 | 54 | 1634 | 159 |
| Future Volume (veh/h) | 247 | 215 | 160 | 109 | 230 | 76 | 198 | 1974 | 81 | 54 | 1634 | 159 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1856 | 1856 | 1856 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 257 | 224 | 167 | 114 | 240 | 79 | 206 | 2056 | 84 | 56 | 1702 | 166 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 318 | 391 | 331 | 284 | 271 | 230 | 236 | 2443 | 100 | 147 | 2077 | 202 |
| Arrive On Green | 0.13 | 0.21 | 0.21 | 0.07 | 0.15 | 0.15 | 0.08 | 0.49 | 0.49 | 0.04 | 0.44 | 0.44 |
| Sat Flow, veh/h | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 5033 | 205 | 1781 | 4731 | 460 |
| Grp Volume(v), veh/h | 257 | 224 | 167 | 114 | 240 | 79 | 206 | 1389 | 751 | 56 | 1223 | 645 |
| Grp Sat Flow(s), veh/h/ln | 1781 | 1870 | 1585 | 1767 | 1856 | 1572 | 1781 | 1702 | 1833 | 1781 | 1702 | 1788 |
| Q Serve(g_s), s | 14.2 | 12.9 | 11.2 | 6.5 | 15.2 | 5.4 | 7.6 | 42.5 | 42.9 | 2.0 | 37.8 | 38.0 |
| Cycle Q Clear(g_c), s | 14.2 | 12.9 | 11.2 | 6.5 | 15.2 | 5.4 | 7.6 | 42.5 | 42.9 | 2.0 | 37.8 | 38.0 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.11 | 1.00 | | 0.26 |
| Lane Grp Cap(c), veh/h | 318 | 391 | 331 | 284 | 271 | 230 | 236 | 1653 | 890 | 147 | 1494 | 785 |
| V/C Ratio(X) | 0.81 | 0.57 | 0.50 | 0.40 | 0.89 | 0.34 | 0.87 | 0.84 | 0.84 | 0.38 | 0.82 | 0.82 |
| Avail Cap(c_a), veh/h | 318 | 391 | 331 | 395 | 294 | 249 | 313 | 1653 | 890 | 218 | 1494 | 785 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.3 | 42.6 | 42.0 | 39.5 | 50.3 | 46.1 | 26.9 | 26.8 | 26.9 | 25.4 | 29.5 | 29.5 |
| Incr Delay (d2), s/veh | 14.4 | 2.0 | 1.2 | 0.9 | 24.8 | 0.9 | 18.6 | 5.3 | 9.6 | 1.6 | 5.1 | 9.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 7.4 | 6.2 | 4.5 | 2.9 | 8.9 | 2.2 | 4.3 | 18.0 | 20.5 | 0.9 | 16.2 | 18.0 |
| Unsig. Movement Delay, s/veh | | 44.7 | 43.2 | 40.4 | 75 1 | 17.0 | | 32.2 | 27 Г | 27.0 | 247 | 39.0 |
| LnGrp Delay(d),s/veh | 50.6 | 44.7 D | | | 75.1 E | 47.0 D | 45.5 | 32.2 C | 36.5 | | 34.6 | |
| LnGrp LOS | D | | D | D | | D | D | | D | С | <u>C</u> | <u> </u> |
| Approach Vol, veh/h | | 648 | | | 433 | | | 2346 | | | 1924 25.0 | |
| Approach Delay, s/veh | | 46.6 | | | 60.8 | | | 34.7 | | | 35.8 | |
| Approach LOS | | D | | | E | | | С | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.2 | 64.3 | 14.4 | 31.1 | 15.8 | 58.7 | 22.0 | 23.5 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | 52.0 | 16.0 | 19.0 | 15.0 | 46.0 | 16.0 | 19.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 4.0 | 44.9 | 8.5 | 14.9 | 9.6 | 40.0 | 16.2 | 17.2 | | | | |
| Green Ext Time (p_c), s | 0.0 | 6.2 | 0.1 | 0.7 | 0.3 | 5.0 | 0.0 | 0.3 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 38.7 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

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|----------------------|-------|----------|--------------|-------|----------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | ٦ | † | 1 | ሻ | † | 1 | ሻ | ተተኈ | ሻ | ተተጮ | |
| Traffic Volume (vph) | 102 | 180 | 170 | 297 | 102 | 58 | 111 | 930 | 273 | 1800 | |
| Future Volume (vph) | 102 | 180 | 170 | 297 | 102 | 58 | 111 | 930 | 273 | 1800 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 11.0 | 24.0 | 24.0 | 23.0 | 36.0 | 36.0 | 12.0 | 35.0 | 38.0 | 61.0 | |
| Total Split (%) | 9.2% | 20.0% | 20.0% | 19.2% | 30.0% | 30.0% | 10.0% | 29.2% | 31.7% | 50.8% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | 🗖 🗖 ø2 (R) | √ Ø3 | ₩ Ø4 | |
|---------------|------------|-------------------|-------------|--|
| 38 s | 35 s | 23 s | 24 s | |
| ▲ Ø5 🕨 Ø6 (R) | | ▶ _{Ø7} 🛟 | 28 | |
| 12 s 61 s | | 11 s 36 s | | |

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|-----------------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u>۲</u> | ↑ | 1 | - ሽ | ↑ | 1 | - ሽ | ተተጮ | | - ሽ | ^ | |
| Traffic Volume (veh/h) | 102 | 180 | 170 | 297 | 102 | 58 | 111 | 930 | 60 | 273 | 1800 | 115 |
| Future Volume (veh/h) | 102 | 180 | 170 | 297 | 102 | 58 | 111 | 930 | 60 | 273 | 1800 | 115 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1856 | 1856 | 1856 | 1722 | 1722 | 1722 | 1841 | 1841 | 1841 | 1856 | 1856 | 1856 |
| Adj Flow Rate, veh/h | 111 | 196 | 185 | 323 | 111 | 63 | 121 | 1011 | 65 | 297 | 1957 | 125 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 3 | 3 | 3 | 12 | 12 | 12 | 4 | 4 | 4 | 3 | 3 | 3 |
| Cap, veh/h | 296 | 251 | 213 | 323 | 405 | 343 | 170 | 1962 | 126 | 395 | 2303 | 147 |
| Arrive On Green | 0.04 | 0.14 | 0.14 | 0.14 | 0.24 | 0.24 | 0.05 | 0.41 | 0.41 | 0.12 | 0.47 | 0.47 |
| Sat Flow, veh/h | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 4825 | 310 | 1767 | 4867 | 310 |
| Grp Volume(v), veh/h | 111 | 196 | 185 | 323 | 111 | 63 | 121 | 701 | 375 | 297 | 1356 | 726 |
| Grp Sat Flow(s), veh/h/ln | 1767 | 1856 | 1572 | 1640 | 1722 | 1459 | 1753 | 1675 | 1785 | 1767 | 1689 | 1800 |
| Q Serve(g_s), s | 5.0 | 12.3 | 13.8 | 17.0 | 6.3 | 4.1 | 4.8 | 18.9 | 18.9 | 11.2 | 42.4 | 42.8 |
| Cycle Q Clear(g_c), s | 5.0 | 12.3 | 13.8 | 17.0 | 6.3 | 4.1 | 4.8 | 18.9 | 18.9 | 11.2 | 42.4 | 42.8 |
| Prop In Lane | 1.00 | 054 | 1.00 | 1.00 | 105 | 1.00 | 1.00 | 40/0 | 0.17 | 1.00 | 4500 | 0.17 |
| Lane Grp Cap(c), veh/h | 296 | 251 | 213 | 323 | 405 | 343 | 170 | 1362 | 726 | 395 | 1598 | 851 |
| V/C Ratio(X) | 0.37 | 0.78 | 0.87 | 1.00 | 0.27 | 0.18 | 0.71 | 0.52 | 0.52 | 0.75 | 0.85 | 0.85 |
| Avail Cap(c_a), veh/h | 296 | 278 | 236 | 323 | 431 | 365 | 170 | 1362 | 726 | 661 | 1598 | 851 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 43.5 | 50.2 | 50.8 | 40.6 | 37.5 | 36.7 | 27.6 | 26.7 | 26.7 | 19.5 | 27.8 | 27.9 |
| Incr Delay (d2), s/veh | 0.8 | 12.2 | 25.9 | 50.1 | 0.4 | 0.3 | 12.8 | 1.4 | 2.6 | 2.9 0.0 | 5.8 | 10.6 |
| Initial Q Delay(d3),s/veh | 0.0 3.0 | 0.0 6.5 | 0.0 7.0 | 0.0 6.6 | 0.0 2.7 | 0.0 1.5 | 0.0 2.6 | 0.0 7.8 | 0.0 8.5 | 4.8 | 0.0 17.9 | 0.0 |
| %ile BackOfQ(50%),veh/In | | 0.0 | 7.0 | 0.0 | Ζ.Ι | 1.5 | 2.0 | 7.0 | 0.0 | 4.8 | 17.9 | 20.4 |
| Unsig. Movement Delay, s/veh | 44.2 | 62.4 | 76.8 | 90.7 | 37.9 | 36.9 | 40.5 | 28.1 | 29.4 | 22.4 | 33.6 | 38.5 |
| LnGrp Delay(d),s/veh LnGrp LOS | 44.Z D | 02.4 E | 70.0 E | 90.7 F | 57.9 D | 30.9 D | 40.5 D | 20.1 C | 29.4 C | 22.4 C | 33.0 C | |
| | D | | E | Г | | D | D | | C | C | | <u>D</u> |
| Approach Vol, veh/h | | 492 | | | 497 | | | 1197 | | | 2379 | |
| Approach Delay, s/veh | | 63.7 | | | 72.1 | | | 29.8 C | | | 33.7 C | |
| Approach LOS | | E | | | E | | | U | | | C | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 20.0 | 54.8 | 23.0 | 22.2 | 12.0 | 62.8 | 11.0 | 34.2 | | | | |
| Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Max Green Setting (Gmax), s | 32.0 | 29.0 | 17.0 | 18.0 | 6.0 | 55.0 | 5.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 13.2 | 20.9 | 19.0 | 15.8 | 6.8 | 44.8 | 7.0 | 8.3 | | | | |
| Green Ext Time (p_c), s | 0.8 | 4.3 | 0.0 | 0.4 | 0.0 | 8.5 | 0.0 | 0.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 40.1 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

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|----------------------|-------|-------|--------------|-------|-------|-------|-------|-------|-------|-------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Configurations | 1 | • | 1 | ľ | • | 1 | ۲ | ተተኈ | ٦ | ተተኈ | |
| Traffic Volume (vph) | 238 | 255 | 154 | 222 | 235 | 102 | 225 | 2004 | 163 | 1574 | |
| Future Volume (vph) | 238 | 255 | 154 | 222 | 235 | 102 | 225 | 2004 | 163 | 1574 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 24.0 | 11.0 | 24.0 | 11.0 | 24.0 | |
| Total Split (s) | 22.0 | 25.0 | 25.0 | 22.0 | 25.0 | 25.0 | 21.0 | 58.0 | 15.0 | 52.0 | |
| Total Split (%) | 18.3% | 20.8% | 20.8% | 18.3% | 20.8% | 20.8% | 17.5% | 48.3% | 12.5% | 43.3% | |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0 | 4.0 | 4.0 | |
| All-Red Time (s) | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | None | C-Max | |

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBTL and 6:SBTL, Start of Green

Natural Cycle: 90

Control Type: Actuated-Coordinated

| Ø1 | <1 _{@2 (R)} | √ Ø3 | ₽ 04 |
|---------|----------------------|-------------|-------------|
| 15 s | 58 s | 22 s | 25 s |
| ▲ Ø5 | ♥ ♥ Ø6 (R) | ▶ Ø1 | |
| 21 s | 52 s | 22 s | 25 s |

| Movement FBI EBT EBR WBI WBI VBI NBI NBI NBI NBI SBI SB | | ۶ | + | \mathbf{F} | 4 | + | • | 1 | 1 | 1 | 1 | ţ | ~ |
|--|--------------------------|------|------|--------------|------|------|------|------|------|------|------|------|------|
| Traffic Volume (veh/n) 238 255 154 222 235 102 225 2004 83 163 1574 153 Future Volume (veh/n) 238 255 154 222 235 102 225 2004 83 163 1574 153 Future Volume (veh/n) 238 255 154 222 235 100 225 2004 83 163 1574 153 Perklike Adj(A_pb7) 1.00 1.01 1.01 | Movement | | | | | | | | | NBR | | | SBR |
| Future Volume (veh/h) 238 255 154 222 235 102 225 2004 83 163 1574 153 Initial Q (Qb), veh 0 | | | | | | | | | | | | ተተጮ | |
| Initial Q(Db), ven 0 | . , | | | | | | | | | | | | |
| Ped-Bike Adj(A_pbT) 1.00 1.01 1.01 1.02 1.02 1.02 1.02 1.02 1.01 1.01 1.02 1.02 1.01 1.01 | | | | | | | | | | | | | |
| Parking Bus, Adj 1.00 1.01 1.0 | | | 0 | | | 0 | | | 0 | | | 0 | |
| Work Zone On Åpproach No No No No No Adj Sat Flow, veh/h1/n 1870 1870 1856 1856 1856 1870 1872 22 | | | | | | | | | | | | | |
| Acij Sat Flow, veh/nh 1870 170 1728 <td< td=""><td></td><td>1.00</td><td></td><td>1.00</td><td>1.00</td><td></td><td>1.00</td><td>1.00</td><td></td><td>1.00</td><td>1.00</td><td></td><td>1.00</td></td<> | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Adj Flow Rate, veh/h 248 266 160 231 245 106 234 2088 86 170 1640 159 Peak Hour Factor 0.96 0.45 0.87 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.87 0.71 | | 1070 | | 1070 | 105/ | | 105/ | 1070 | | 1070 | 1070 | | 1070 |
| Peak Hour Factor 0.96 0.92 0.92 0.9 | | | | | | | | | | | | | |
| Percent Heavy Veh, % 2 2 2 2 3 3 3 2 1 1 1 1 1 1 1 2 1 2 3 3 | | | | | | | | | | | | | |
| Cap, veh/h 318 293 249 299 279 236 263 2241 92 197 1987 192 Arrive On Green 0.13 0.16 0.13 0.15 0.15 0.10 0.45 0.45 0.07 0.42 0.42 0.42 Sat Flow, veh/h 1781 1780 1585 1767 1856 1572 1781 1701 1179 620 Grp Sat Flow, veh/h 1781 1870 1585 1767 1856 1572 1781 1702 1833 1781 1702 1783 Q Serve(g_s), s 13.9 16.8 11.4 13.1 15.5 7.4 9.5 47.1 47.5 6.6 6.6 9.7 700 Prop In Lane 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.30 0.48 0.48 0.89 0.93 0.68 6.8 0.83 0.84 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 < | | | | | | | | | | | | | |
| Arrive On Green 0.13 0.16 0.13 0.15 0.15 0.10 0.45 0.45 0.07 0.42 0.42 Sat Flow, veh/h 1781 1870 1585 1767 1856 1572 1781 5031 207 1781 4734 458 Grp Volume(v), veh/h 248 266 160 231 245 106 234 1411 763 170 1179 620 Grp Sat Flow(s), veh/h/in 1781 1870 1585 1767 1856 1572 1781 1702 1781 1702 1788 O serve(g_s), s 13.9 16.8 11.4 13.1 15.5 7.4 9.5 47.1 47.5 6.6 36.9 37.0 Oya In Lane 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.10 0.11 1.00 0.26 Lane Gro Cap(c), veh/h 318 293 249 299 279 236 263 1516 817 203 1.429 750 V/C Ratio(X) 0. | | | | | | | | | | | | | |
| Sat Flow, veh/h 1781 1870 1585 1767 1856 1572 1781 5031 207 1781 4734 458 Grp Volume(v), veh/h 248 266 160 231 245 106 234 1411 763 170 1179 620 Grp Sat Flow(s),veh/h/ln 1781 1870 1585 1767 1856 1572 1781 1702 1833 1781 1702 1788 Q Serve(g.s), s 13.9 16.8 11.4 13.1 15.5 7.4 9.5 47.1 47.5 6.6 36.9 37.0 Orge Calc(c), veh/h 318 293 249 299 279 236 263 1516 817 197 1429 750 V/C Ratio(X) 0.78 0.91 0.64 0.77 0.88 0.45 0.89 0.93 0.93 0.86 0.82 0.83 Avait Cap(c, a), veh/h 319 296 251 312 294 249 312 1516 817 203 1429 750 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | | | | | | | |
| Grp Volume(v), veh/h24826616023124510623414117631701179620Grp Sat Flow(s), veh/h/ln178118701585176718561572178117021833178117021788Q Serve(g_s), s13.916.811.413.115.57.49.547.147.56.636.937.0Oycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0Orycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0Orycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0Orycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0V/C Ratio(X)0.780.910.640.770.880.450.890.930.930.860.820.83Avail Cap(C, a), veh/h31929625131229424931215168172031429750HCM Platoon Ratio1.001.001.001.001.001.001.001.001.001.001.001.001.00Inor Delay (d), sveh37.149.747.437.449.946.528.4 </td <td></td> | | | | | | | | | | | | | |
| Grp Sat Flow(s), veh/h/ln178118701585176718561572178117021833178117021788O Serve(g_s), s13.916.811.413.115.57.49.547.147.56.636.937.0Cycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0Cycle Q Clear(g_c), s13.916.811.413.115.57.49.547.147.56.636.937.0Cycle Q Clear(g_c), veh/h31829324929927923626315168171971429750V/C Ratio(X)0.780.910.640.770.880.450.890.930.930.860.820.83Avail Cap(c_a), veh/h31929625131229424931215168172031429750HCM Platoon Ratio1.001.001.001.001.001.001.001.001.001.001.001.001.00Upstram Filter(f)1.001.001.001.001.001.001.001.001.001.001.001.00Uniform Delay (d), s/veh37.149.747.437.449.946.528.431.531.628.530.930.9Incr Delay (d2), s/veh17.110.24.96.59.03.05. | | | | | | | | | | | | | |
| Q Serve(g_s), s 13.9 16.8 11.4 13.1 15.5 7.4 9.5 47.1 47.5 6.6 36.9 37.0 Cycle O Clear(g_c), s 13.9 16.8 11.4 13.1 15.5 7.4 9.5 47.1 47.5 6.6 36.9 37.0 Prop In Lane 1.00 1.00 1.00 1.00 1.00 0.11 1.00 0.26 Lane Grp Cap(c), veh/h 318 293 249 299 279 236 263 1516 817 197 1429 750 V/C Ratio(X) 0.78 0.91 0.64 0.77 0.88 0.45 0.89 0.93 0.93 0.86 0.82 0.83 Avail Cap(c_a), veh/h 319 296 251 312 294 249 312 1516 817 197 1429 750 Upstream Filter(I) 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 | | | | | | | | | | | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | | | | | | | | | | |
| Prop In Lane 1.00 1.00 1.00 1.00 1.00 0.11 1.00 0.26 Lane Grp Cap(c), veh/h 318 293 249 299 279 236 263 1516 817 197 1429 750 V/C Ratio(X) 0.78 0.91 0.64 0.77 0.88 0.45 0.89 0.93 0.93 0.86 0.82 0.83 Avail Cap(c_a), veh/h 319 296 251 312 294 249 312 1516 817 203 1429 750 HCM Platoon Ratio 1.00 | | | | | | | | | | | | | |
| Lane Grp Cap(c), veh/h31829324929927923626315168171971429750V/C Ratio(X)0.780.910.640.770.880.450.890.930.930.860.820.83Avail Cap(c_a), veh/h31929625131229424931215168172031429750HCM Platoon Ratio1.001.0 | | | | | | 1010 | | | | | | 0017 | |
| V/C Ratio(X) 0.78 0.91 0.64 0.77 0.88 0.45 0.89 0.93 0.93 0.86 0.82 0.83 Avail Cap(c_a), veh/h 319 296 251 312 294 249 312 1516 817 203 1429 750 HCM Platoon Ratio 1.00 | | | 293 | | | 279 | | | 1516 | | | 1429 | |
| HCM Platoon Ratio1.001 | | | | | | | | | | | | | |
| Upstream Filter(I)1.00 | Avail Cap(c_a), veh/h | 319 | 296 | 251 | 312 | 294 | 249 | 312 | 1516 | 817 | 203 | 1429 | 750 |
| Uniform Delay (d), s/veh37.149.747.437.449.946.528.431.531.628.530.930.9Incr Delay (d2), s/veh11.729.45.511.024.01.323.211.619.129.45.510.1Initial Q Delay(d3), s/veh0.00.00.00.00.00.00.00.00.00.00.00.00.0%ile BackOfQ(50%), veh/ln7.110.24.96.59.03.05.621.224.74.315.917.8Unsig. Movement Delay, s/veh71.110.24.96.59.03.05.621.224.74.315.917.8Unsig. Movement Delay, s/veh71.152.948.474.047.851.643.150.857.936.441.1LnGrp DCSDEDDEDDDEDDApproach Vol, veh/h67458224081969Approach LOSEEDDDDDTimer - Assigned Phs12345678Phs Duration (G+Y+Rc), s14.659.421.124.817.756.421.924.0Change Period (Y+Rc), s6.06.06.06.06.06.06.06.06.0Max Green Setting (Gmax), s9.052.016.019.015.9< | HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Initial Q Delay(d3),s/veh 0.0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | | | | | | | |
| %ile BackOfQ(50%), veh/ln 7.1 10.2 4.9 6.5 9.0 3.0 5.6 21.2 24.7 4.3 15.9 17.8 Unsig. Movement Delay, s/veh 48.8 79.1 52.9 48.4 74.0 47.8 51.6 43.1 50.8 57.9 36.4 41.1 LnGrp Delay(d),s/veh 48.8 79.1 52.9 48.4 74.0 47.8 51.6 43.1 50.8 57.9 36.4 41.1 LnGrp DOS D E D D D D E D D E D D E D D E D D E D D E D D E D D E D D D E D D D E D D D E D D D E D D D E D D D E D D D D D D D D E D D D D | | | | | | | | | | | | | |
| Unsig. Movement Delay, s/veh LnGrp Delay(d), s/veh 48.8 79.1 52.9 48.4 74.0 47.8 51.6 43.1 50.8 57.9 36.4 41.1 LnGrp Dols D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D E D D D E D D D E D D D E D D E D D E D D E D D E D D C D D D E D D D D D D D D D <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh48.879.152.948.474.047.851.643.150.857.936.441.1LnGrp LOSDEDDEDDDDEDDApproach Vol, veh/h67458224081969Approach Delay, s/veh61.759.046.439.8Approach LOSEEDDDDTimer - Assigned Phs1234567Phs Duration (G+Y+Rc), s14.659.421.124.817.756.421.924.0Change Period (Y+Rc), s6.06.06.06.06.06.06.06.0Max Green Setting (Gmax), s9.052.016.019.015.046.016.019.0Max Q Clear Time (g_c+I1), s8.649.515.118.811.539.015.917.5Green Ext Time (p_c), s0.02.30.10.10.25.60.00.3Intersection Summary47.2 | | | 10.2 | 4.9 | 6.5 | 9.0 | 3.0 | 5.6 | 21.2 | 24.7 | 4.3 | 15.9 | 17.8 |
| LnGrp LOS D E D D E D D D D E D D D D E D <thd< th=""> D D<</thd<> | | | | | | | | | | | | | |
| Approach Vol, veh/h 674 582 2408 1969 Approach Delay, s/veh 61.7 59.0 46.4 39.8 Approach LOS E E D D Timer - Assigned Phs 1 2 3 4 5 6 7 8 Phs Duration (G+Y+Rc), s 14.6 59.4 21.1 24.8 17.7 56.4 21.9 24.0 Change Period (Y+Rc), s 6.0 </td <td>1 3 ()</td> <td></td> | 1 3 () | | | | | | | | | | | | |
| Approach Delay, s/veh 61.7 59.0 46.4 39.8 Approach LOS E E D D Timer - Assigned Phs 1 2 3 4 5 6 7 8 Phs Duration (G+Y+Rc), s 14.6 59.4 21.1 24.8 17.7 56.4 21.9 24.0 Change Period (Y+Rc), s 6.0< | | D | | D | D | | D | D | | D | E | | D |
| Approach LOS E E D D Timer - Assigned Phs 1 2 3 4 5 6 7 8 Phs Duration (G+Y+Rc), s 14.6 59.4 21.1 24.8 17.7 56.4 21.9 24.0 Change Period (Y+Rc), s 6.0 6.0 6.0 6.0 6.0 6.0 6.0 Max Green Setting (Gmax), s 9.0 52.0 16.0 19.0 15.0 46.0 16.0 19.0 Max Q Clear Time (g_c+I1), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 47.2 47.2 47.2 47.2 47.2 | | | | | | | | | | | | | |
| Timer - Assigned Phs 1 2 3 4 5 6 7 8 Phs Duration (G+Y+Rc), s 14.6 59.4 21.1 24.8 17.7 56.4 21.9 24.0 Change Period (Y+Rc), s 6.0 6.0 6.0 6.0 6.0 6.0 6.0 Max Green Setting (Gmax), s 9.0 52.0 16.0 19.0 15.0 46.0 16.0 19.0 Max Q Clear Time (g_c+11), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 47.2 47.2 47.2 47.2 47.2 | | | | | | | | | | | | | |
| Phs Duration (G+Y+Rc), s 14.6 59.4 21.1 24.8 17.7 56.4 21.9 24.0 Change Period (Y+Rc), s 6.0 6.0 6.0 6.0 6.0 6.0 6.0 Max Green Setting (Gmax), s 9.0 52.0 16.0 19.0 15.0 46.0 16.0 19.0 Max Q Clear Time (g_c+I1), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 47.2 47.2 47.2 47.2 47.2 | Approach LUS | | E | | | E | | | D | | | D | |
| Change Period (Y+Rc), s 6.0 6.0 6.0 6.0 6.0 6.0 Max Green Setting (Gmax), s 9.0 52.0 16.0 19.0 15.0 46.0 16.0 19.0 Max Q Clear Time (g_c+I1), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 | Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Max Green Setting (Gmax), s 9.0 52.0 16.0 19.0 15.0 46.0 16.0 19.0 Max Q Clear Time (g_c+l1), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 | Phs Duration (G+Y+Rc), s | 14.6 | 59.4 | 21.1 | 24.8 | 17.7 | 56.4 | 21.9 | 24.0 | | | | |
| Max Q Clear Time (g_c+l1), s 8.6 49.5 15.1 18.8 11.5 39.0 15.9 17.5 Green Ext Time (p_c), s 0.0 2.3 0.1 0.1 0.2 5.6 0.0 0.3 Intersection Summary 47.2 | Change Period (Y+Rc), s | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | | | | |
| Green Ext Time (p_c), s 0.0 2.3 0.1 0.2 5.6 0.0 0.3 Intersection Summary | | | 52.0 | 16.0 | 19.0 | | 46.0 | 16.0 | | | | | |
| Intersection Summary HCM 6th Ctrl Delay 47.2 | | | | | | | | | | | | | |
| HCM 6th Ctrl Delay 47.2 | Green Ext Time (p_c), s | 0.0 | 2.3 | 0.1 | 0.1 | 0.2 | 5.6 | 0.0 | 0.3 | | | | |
| | Intersection Summary | | | | | | | | | | | | |
| | | | | 47.2 | | | | | | | | | |
| | | | | | | | | | | | | | |

HCM 95th %tile Q(veh)

2.4

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0.1

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| Intersection | | | | | | |
|------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 4.6 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4Î | | ሻ | ↑ | ۰¥ | |
| Traffic Vol, veh/h | 211 | 264 | 35 | 192 | 229 | 30 |
| Future Vol, veh/h | 211 | 264 | 35 | 192 | 229 | 30 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 50 | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 2 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 3 | 2 | 2 | 12 | 2 | 2 |
| Mvmt Flow | 229 | 287 | 38 | 209 | 249 | 33 |

| Major/Minor M | ajor1 | Ν | /lajor2 | 1 | Vinor1 | |
|-----------------------|-------|-------|---------|-----|-----------|------|
| Conflicting Flow All | 0 | 0 | 516 | 0 | 658 | 373 |
| Stage 1 | - | - | - | - | 373 | - |
| Stage 2 | - | - | - | - | 285 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | |
| Pot Cap-1 Maneuver | - | - | 1034 | - | | 739 |
| Stage 1 | - | - | - | - | 728 | - |
| Stage 2 | - | - | - | - | 763 | - |
| Platoon blocked, % | - | - | 1 | - | 1 | 1 |
| Mov Cap-1 Maneuver | - | - | 1034 | - | 127 | 739 |
| Mov Cap-2 Maneuver | - | - | - | - | 599 | - |
| Stage 1 | - | - | - | - | 728 | - |
| Stage 2 | - | - | - | - | 735 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 1.3 | | 15.8 | |
| HCM LOS | 0 | | 1.5 | | 13.0 C | |
| | | | | | 0 | |
| | | | | | | |
| Minor Lane/Major Mvmt | N | IBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 612 | - | - | 1034 | - |
| HCM Lane V/C Ratio | | 0.46 | - | - | 0.037 | - |
| HCM Control Delay (s) | | 15.8 | - | - | 8.6 | - |
| HCM Lane LOS | | С | - | - | А | - |

| Intersection | | | | | | |
|------------------------|------------|------|------|------|------|------|
| Int Delay, s/veh | 2.9 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | f a | | ሻ | ↑ | ۰¥ | |
| Traffic Vol, veh/h | 287 | 165 | 25 | 344 | 156 | 26 |
| Future Vol, veh/h | 287 | 165 | 25 | 344 | 156 | 26 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 50 | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 2 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 3 | 2 | 2 |
| Mvmt Flow | 312 | 179 | 27 | 374 | 170 | 28 |

| Major/Minor N | 1ajor1 | N | Najor2 | | Vinor1 | |
|-----------------------|--------|-------|--------|-----|--------|-------|
| Conflicting Flow All | 0 | 0 | 491 | 0 | 830 | 402 |
| Stage 1 | - | - | - | - | 402 | - |
| Stage 2 | - | - | - | - | 428 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | ···- | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1065 | - | 342 | 756 |
| Stage 1 | - | - | - | - | 728 | - |
| Stage 2 | - | - | - | - | 657 | - |
| Platoon blocked, % | - | - | 1 | - | 1 | 1 |
| Mov Cap-1 Maneuver | - | - | 1065 | - | | 756 |
| Mov Cap-2 Maneuver | - | - | - | - | 534 | - |
| Stage 1 | - | - | - | - | 728 | - |
| Stage 2 | - | - | - | - | 641 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.6 | | 15 | |
| HCM LOS | Ū | | 0.0 | | C | |
| | | | | | Ŭ | |
| | | | EDT | | | WDT |
| Minor Lane/Major Mvm | t ľ | VBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 557 | - | - | | - |
| HCM Lane V/C Ratio | | 0.355 | - | - | 0.026 | - |
| HCM Control Delay (s) | | 15 | - | - | 0.0 | - |
| HCM Lane LOS | | С | - | - | A | - |
| HCM 95th %tile Q(veh) | | 1.6 | - | - | 0.1 | - |

| Intersection | | | | | | |
|------------------------|-------|------|------|------|------|------|
| Int Delay, s/veh | 4.6 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4 | | ٦ | | Y | |
| Traffic Vol, veh/h | 248 | 264 | 35 | 227 | 229 | 30 |
| Future Vol, veh/h | 248 | 264 | 35 | 227 | 229 | 30 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 50 | - | 0 | - |
| Veh in Median Storage | e,# 0 | - | - | 0 | 2 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 3 | 2 | 2 | 12 | 2 | 2 |
| Mvmt Flow | 270 | 287 | 38 | 247 | 249 | 33 |

| Major/Minor | Major1 | ſ | Major2 | ſ | Minor1 | |
|----------------------|--------|-------|--------|-----|--------|-------|
| Conflicting Flow All | 0 | | 557 | 0 | 737 | 414 |
| Stage 1 | - | - | - | - | 414 | - |
| Stage 2 | - | - | - | - | 323 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 991 | - | | 708 |
| Stage 1 | - | - | - | - | 699 | - |
| Stage 2 | - | - | - | - | 734 | - |
| Platoon blocked, % | - | - | 1 | - | 1 | 1 |
| Mov Cap-1 Maneuver | | - | 991 | - | | 708 |
| Mov Cap-2 Maneuver | · - | - | - | - | 565 | - |
| Stage 1 | - | - | - | - | • • • | - |
| Stage 2 | - | - | - | - | 706 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | s 0 | | 1.2 | | 17 | |
| HCM LOS | | | | | С | |
| | | | | | | |
| Minor Lane/Major Mv | mt | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 579 | - | - | 0.01 | - |
| HCM Lane V/C Ratio | | 0.486 | - | - | 0.038 | - |
| HCM Control Delay (s | 5) | 17 | - | - | | - |
| HCM Lane LOS | , | С | - | - | А | - |
| HCM 95th %tile Q(ve | | 2.6 | | | 0.1 | |

| Intersection | | | | | | |
|------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.9 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4 | | | ↑ | ۰¥ | |
| Traffic Vol, veh/h | 337 | 165 | 25 | 402 | 156 | 26 |
| Future Vol, veh/h | 337 | 165 | 25 | 402 | 156 | 26 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | 50 | - | 0 | - |
| Veh in Median Storage | ,# 0 | - | - | 0 | 2 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 3 | 2 | 2 |
| Mvmt Flow | 366 | 179 | 27 | 437 | 170 | 28 |

| Major/Minor M | lajor1 | Ν | Major2 | | Minor1 | |
|-----------------------|--------|-------|--------|-----|--------|-------|
| Conflicting Flow All | 0 | 0 | 545 | 0 | 947 | 456 |
| Stage 1 | - | - | - | - | 456 | - |
| Stage 2 | - | - | - | - | 491 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1006 | - | | 707 |
| Stage 1 | - | - | - | - | 686 | - |
| Stage 2 | - | - | - | - | 615 | - |
| Platoon blocked, % | - | - | 1 | - | 1 | 1 |
| Mov Cap-1 Maneuver | - | - | 1006 | - | | 707 |
| Mov Cap-2 Maneuver | - | - | - | - | 488 | - |
| Stage 1 | - | - | - | - | 000 | - |
| Stage 2 | - | - | - | - | 598 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0.5 | | 16.4 | |
| HCM LOS | | | | | С | |
| | | | | | | |
| Minor Long/Major Mumt | | | ГДТ | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 511 | - | | 1006 | - |
| HCM Lane V/C Ratio | | 0.387 | - | | 0.027 | - |
| HCM Control Delay (s) | | 16.4 | - | - | 0.7 | - |
| HCM Lane LOS | | C | - | - | A | - |
| HCM 95th %tile Q(veh) | | 1.8 | - | - | 0.1 | - |

| Int Delay, s/veh | 0.4 | | | | | |
|------------------------|------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴。 | | | ^ |
| Traffic Vol, veh/h | 0 | 97 | 858 | 79 | 0 | 1952 |
| Future Vol, veh/h | 0 | 97 | 858 | 79 | 0 | 1952 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 4 | 2 | 2 | 3 |
| Mvmt Flow | 0 | 105 | 933 | 86 | 0 | 2122 |

| Major/Minor | Minor1 | Ν | /lajor1 | N | lajor2 | |
|----------------------|--------|------|---------|-------|--------|---|
| Conflicting Flow All | - | 510 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | *712 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuver | | *712 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 5 10.9 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lang/Major Mu | mt | NBT | NBRWI | Din 1 | SBT | |
| Minor Lane/Major Mvi | III | ND I | NDRVI | | | |
| Capacity (veh/h) | | - | - | 712 | - | |
| HCM Lane V/C Ratio | | - | - (|).148 | - | |
| HCM Control Delay (s | 5) | - | - | 10.9 | - | |

Notes

HCM Lane LOS

HCM 95th %tile Q(veh)

~: Volume exceeds capacity

\$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

В

0.5

-

_

-

-

-

HCM 95th %tile Q(veh)

Notes

| Int Delay, s/veh | 0.4 | | | | | |
|------------------------|------|------|------|------|------|------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | *** |
| Traffic Vol, veh/h | 0 | 100 | 1893 | 84 | 0 | 1679 |
| Future Vol, veh/h | 0 | 100 | 1893 | 84 | 0 | 1679 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 109 | 2058 | 91 | 0 | 1825 |

| Major/Minor | Minor1 | Ν | Najor1 | Ν | /lajor2 | |
|----------------------|-----------|------|--------|-------|---------|---|
| Conflicting Flow All | - | 1075 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | | *469 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuve | | *469 | - | - | - | - |
| Mov Cap-2 Maneuve | er - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, | | | 0 | | 0 | |
| HCM LOS | 3 13 C | | 0 | | 0 | |
| | C | | | | | |
| | | | | | | |
| Minor Lane/Major M | /mt | NBT | NBRW | BLn1 | SBT | |
| Capacity (veh/h) | | - | - | 469 | - | |
| HCM Lane V/C Ratio |) | - | - (|).232 | - | |
| HCM Control Delay (| (S) | - | - | 15 | - | |
| HCM Lane LOS | | - | - | С | - | |

~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

0.9

| Int Delay, s/veh | 0.3 | | | | | |
|------------------------|-------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | ^ |
| Traffic Vol, veh/h | 0 | 97 | 1004 | 79 | 0 | 2267 |
| Future Vol, veh/h | 0 | 97 | 1004 | 79 | 0 | 2267 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | , # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 4 | 2 | 2 | 3 |
| Mvmt Flow | 0 | 105 | 1091 | 86 | 0 | 2464 |

| Major/Minor | Minor1 | Ν | /lajor1 | Ν | Najor2 | |
|----------------------|--------|------|---------|------|--------|---|
| Conflicting Flow All | - | 589 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | *690 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuver | · - | *690 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 5 11.2 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lane/Major Mvi | mt | NBT | NBRWI | 3Ln1 | SBT | |
| Capacity (veh/h) | | - | - | 690 | - | |

| | ¢. Dala | | 200- | Communication Net Defined | * All main walking in alata an |
|-----------------------|---------|---------|----------|---------------------------|--------------------------------|
| Notes | | | | | |
| HCM 95th %tile Q(veh) | - | - 0.5 | , , - | | |
| HCM Lane LOS | - | - E | | | |
| HCM Control Delay (s) | - | - 11.2 | ! - | | |
| HCM Lane V/C Ratio | - | - 0.153 | - | | |
| Capacity (ven/n) | - | - 090 | | • | |

-: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

| Int Delay, s/veh | 0.4 | | | | | |
|------------------------|------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | ^ |
| Traffic Vol, veh/h | 0 | 100 | 2213 | 84 | 0 | 1950 |
| Future Vol, veh/h | 0 | 100 | 2213 | 84 | 0 | 1950 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 109 | 2405 | 91 | 0 | 2120 |

| Major/Minor | Minor1 | Μ | lajor1 | Ма | ijor2 | |
|----------------------|--------|------|--------|----|-------|---|
| Conflicting Flow All | - | 1248 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | *381 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuver | | *381 | - | - | - | - |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 18.2 | | 0 | | 0 | |
| HCM LOS | С | | | | | |

| Minor Lane/Major Mvmt | NBT | NBRWB | Ln1 Sł | BT | | |
|----------------------------|-------|------------|----------|----|----------------------------|--------------------------------|
| Capacity (veh/h) | - | - | 381 | - | | |
| HCM Lane V/C Ratio | - | - 0. | 285 | - | | |
| HCM Control Delay (s) | - | - 1 | 8.2 | - | | |
| HCM Lane LOS | - | - | С | - | | |
| HCM 95th %tile Q(veh) | - | - | 1.2 | - | | |
| Notes | | | | | | |
| ~: Volume exceeds capacity | \$: D | elay excee | eds 300s | + | -: Computation Not Defined | *: All major volume in platoon |

Synchro 11 Report Page 1

| Int Delay, s/veh | 0.1 | | | | | |
|------------------------|------|------|------|------|------|------------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴序 | | | *†† |
| Traffic Vol, veh/h | 0 | 37 | 900 | 39 | 0 | 1952 |
| Future Vol, veh/h | 0 | 37 | 900 | 39 | 0 | 1952 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 4 | 2 | 2 | 3 |
| Mvmt Flow | 0 | 40 | 978 | 42 | 0 | 2122 |

| Major/Minor | Minor1 | Μ | lajor1 | Ма | ajor2 | |
|----------------------|--------|------|--------|----|-------|---|
| Conflicting Flow All | - | 510 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | | *712 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuver | | *712 | - | - | - | - |
| Mov Cap-2 Maneuver | r - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | s 10.4 | | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | | | | |

| Minor Lane/Major Mvmt | NBT | NBRWBLn1 | SBT | |
|-----------------------|-----|----------|-----|--|
| Capacity (veh/h) | - | - 712 | - | |
| HCM Lane V/C Ratio | - | - 0.056 | - | |
| HCM Control Delay (s) | - | - 10.4 | - | |
| HCM Lane LOS | - | - B | - | |
| HCM 95th %tile Q(veh) | - | - 0.2 | - | |
| Notes | | | | |
| | | | | |

-: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

| Int Delay, s/veh | 0.1 | | | | | |
|------------------------|-------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | ^ |
| Traffic Vol, veh/h | 0 | 39 | 1936 | 40 | 0 | 1679 |
| Future Vol, veh/h | 0 | 39 | 1936 | 40 | 0 | 1679 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | , # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 42 | 2104 | 43 | 0 | 1825 |

| Major/Minor | Minor1 | Ν | Najor1 | Ν | /lajor2 | |
|----------------------|--------|------|--------|---------|---------|---|
| Conflicting Flow All | - | | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | | *447 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuve | | *447 | - | - | - | - |
| Mov Cap-2 Maneuver | r - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, | | | 0 | | 0 | |
| HCM LOS | В | | Ŭ | | Ŭ | |
| | | | | | | |
| | | NDT | | 1 س ا ط | CDT | |
| Minor Lane/Major Mv | mt | NBT | NBRW | | SBT | |
| Capacity (veh/h) | | - | - | 447 | - | |
| HCM Lane V/C Ratio | | - | - (| 0.095 | - | |
| HCM Control Delay (| S) | - | - | 13.9 | - | |
| HCM Lane LOS | | - | - | В | - | |

Notes

~: Volume exceeds capacity

HCM 95th %tile Q(veh)

\$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

0.3

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| Int Delay, s/veh | 0.1 | | | | | |
|------------------------|------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | ^ |
| Traffic Vol, veh/h | 0 | 37 | 1046 | 39 | 0 | 2267 |
| Future Vol, veh/h | 0 | 37 | 1046 | 39 | 0 | 2267 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | ,# 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 4 | 2 | 2 | 3 |
| Mvmt Flow | 0 | 40 | 1137 | 42 | 0 | 2464 |

| Major/Minor | Minor1 | Ν | /lajor1 | Ν | /lajor2 | |
|----------------------|--------|------|---------|-------|---------|---|
| Conflicting Flow All | - | 590 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | 0 | *668 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuver | | *668 | - | - | - | - |
| Mov Cap-2 Maneuver | · - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | | | 0 | | 0 | |
| HCM LOS | В | | • | | Ŭ | |
| | 2 | | | | | |
| | | NDT | | (DL 1 | CDT | |
| Minor Lane/Major Mv | mt | NBT | NBRW | | SBT | |
| Capacity (veh/h) | | - | - | 668 | - | |
| HCM Lane V/C Ratio | | - | - | 0.06 | - | |
| HCM Control Delay (s | 5) | - | - | 10.7 | - | |
| HCM Lane LOS | | - | - | В | - | |

Notes

~: Volume exceeds capacity

HCM 95th %tile Q(veh)

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0.2

\$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

| Int Delay, s/veh | 0.1 | | | | | |
|------------------------|-------|------|------|------|------|----------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | | 1 | 朴朴 | | | ^ |
| Traffic Vol, veh/h | 0 | 39 | 2256 | 40 | 0 | 1950 |
| Future Vol, veh/h | 0 | 39 | 2256 | 40 | 0 | 1950 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage | , # 0 | - | 0 | - | - | 0 |
| Grade, % | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 42 | 2452 | 43 | 0 | 2120 |

| Major/Minor | Minor1 | Ν | /lajor1 | Ν | /lajor2 | |
|--|---------|-------|---------|---------------|---------|---|
| Conflicting Flow All | - | 1248 | 0 | 0 | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | 7.14 | - | - | - | - |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | 3.92 | - | - | - | - |
| Pot Cap-1 Maneuver | | *381 | - | - | 0 | - |
| Stage 1 | 0 | - | - | - | 0 | - |
| Stage 2 | 0 | - | - | - | 0 | - |
| Platoon blocked, % | | 1 | - | - | | - |
| Mov Cap-1 Maneuve | | *381 | - | - | - | - |
| Mov Cap-2 Maneuve | r - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, | s 15.6 | | 0 | | 0 | |
| HCM LOS | С | | | | | |
| | | | | | | |
| Minor Lane/Major Mv | mt | NBT | NBRW | 'Rl n1 | SBT | |
| | mt | IND I | NDRW | | | |
| Capacity (veh/h) HCM Lane V/C Ratio | | - | - | 381 | - | |
| | | - | - | 0.111 15.6 | - | |
| HCM Control Delay (HCM Lane LOS | 5) | - | - | 15.0 C | - | |
| HCM 95th %tile Q(ve | b) | - | - | 0.4 | - | |
| | 51) | - | - | 0.4 | - | |

Notes

~: Volume exceeds capacity

\$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon



APPENDIX E

Queue Analysis Worksheets

Kimley »Horn

096888037 Berkley Center Subdivision

| | ٦ | - | \mathbf{r} | ∢ | ← | • | 1 | Ť | 1 | Ŧ | |
|-------------------------|------|------|--------------|------|------|------|------|------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Group Flow (vph) | 93 | 177 | 157 | 305 | 96 | 58 | 109 | 930 | 284 | 1765 | |
| v/c Ratio | 0.39 | 0.74 | 0.38 | 0.95 | 0.25 | 0.12 | 0.67 | 0.50 | 0.68 | 0.75 | |
| Control Delay | 37.2 | 68.7 | 2.6 | 75.2 | 38.8 | 0.5 | 43.8 | 29.9 | 22.9 | 28.6 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 37.2 | 68.7 | 2.6 | 75.2 | 38.8 | 0.5 | 43.8 | 29.9 | 22.9 | 28.6 | |
| Queue Length 50th (ft) | 51 | 132 | 0 | 194 | 60 | 0 | 37 | 201 | 108 | 407 | |
| Queue Length 95th (ft) | 91 | 208 | 0 | #317 | 107 | 0 | #151 | 283 | 177 | 469 | |
| Internal Link Dist (ft) | | 861 | | | 391 | | | 203 | | 296 | |
| Turn Bay Length (ft) | 250 | | 250 | 300 | | 100 | 600 | | 225 | | |
| Base Capacity (vph) | 239 | 276 | 443 | 321 | 424 | 503 | 162 | 1861 | 578 | 2354 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.39 | 0.64 | 0.35 | 0.95 | 0.23 | 0.12 | 0.67 | 0.50 | 0.49 | 0.75 | |
| Intersection Summary | | | | | | | | | | | |

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. #

| | ۶ | - | $\mathbf{\hat{z}}$ | ∢ | - | • | 1 | 1 | 1 | Ŧ | |
|-------------------------|------|------|--------------------|------|------|------|------|------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Group Flow (vph) | 211 | 233 | 136 | 215 | 211 | 96 | 205 | 1870 | 161 | 1533 | |
| v/c Ratio | 0.67 | 0.84 | 0.39 | 0.72 | 0.76 | 0.27 | 0.80 | 0.82 | 0.81 | 0.73 | |
| Control Delay | 42.0 | 75.6 | 10.8 | 45.8 | 67.3 | 4.6 | 44.7 | 33.4 | 56.8 | 32.4 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 42.0 | 75.6 | 10.8 | 45.8 | 67.3 | 4.6 | 44.7 | 33.4 | 56.8 | 32.4 | |
| Queue Length 50th (ft) | 121 | 176 | 0 | 124 | 157 | 0 | 104 | 492 | 77 | 378 | |
| Queue Length 95th (ft) | 189 | #301 | 56 | 193 | #261 | 20 | #209 | 564 | #201 | 439 | |
| Internal Link Dist (ft) | | 861 | | | 391 | | | 203 | | 296 | |
| Turn Bay Length (ft) | 250 | | 250 | 300 | | 100 | 600 | | 225 | | |
| Base Capacity (vph) | 337 | 294 | 365 | 315 | 292 | 362 | 283 | 2281 | 200 | 2105 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.63 | 0.79 | 0.37 | 0.68 | 0.72 | 0.27 | 0.72 | 0.82 | 0.81 | 0.73 | |
| Intersection Summary | | | | | | | | | | | |

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. #

| | ۶ | - | \mathbf{r} | ∢ | + | • | 1 | Ť | 1 | Ļ | |
|-------------------------|------|------|--------------|------|------|------|--------------|------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Group Flow (vph) | 111 | 196 | 185 | 323 | 111 | 63 | 121 | 1076 | 297 | 2082 | |
| v/c Ratio | 0.45 | 0.78 | 0.44 | 1.03 | 0.28 | 0.13 | 0.76 | 0.60 | 0.76 | 0.90 | |
| Control Delay | 39.5 | 71.3 | 5.0 | 93.3 | 39.0 | 0.6 | 53. 9 | 32.8 | 32.6 | 35.7 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 39.5 | 71.3 | 5.0 | 93.3 | 39.0 | 0.6 | 53. 9 | 32.8 | 32.6 | 35.7 | |
| Queue Length 50th (ft) | 60 | 146 | 0 | ~206 | 69 | 0 | 45 | 250 | 130 | 533 | |
| Queue Length 95th (ft) | 105 | #244 | 22 | #367 | 121 | 0 | #177 | 340 | 223 | 609 | |
| Internal Link Dist (ft) | | 861 | | | 391 | | | 203 | | 296 | |
| Turn Bay Length (ft) | 250 | | 250 | 300 | | 100 | 600 | | 225 | | |
| Base Capacity (vph) | 245 | 276 | 443 | 315 | 424 | 503 | 159 | 1785 | 548 | 2326 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.45 | 0.71 | 0.42 | 1.03 | 0.26 | 0.13 | 0.76 | 0.60 | 0.54 | 0.90 | |
| Interception Summony | | | | | | | | | | | |

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.
95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

| | ٦ | - | $\mathbf{\hat{z}}$ | 4 | + | × | 1 | 1 | 1 | Ŧ | |
|-------------------------|------|------|--------------------|------|------|------|------|------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT | |
| Lane Group Flow (vph) | 248 | 266 | 160 | 231 | 245 | 106 | 234 | 2174 | 170 | 1799 | |
| v/c Ratio | 0.81 | 0.91 | 0.42 | 0.80 | 0.85 | 0.30 | 0.87 | 0.98 | 0.86 | 0.89 | |
| Control Delay | 52.1 | 85.1 | 10.4 | 52.4 | 75.9 | 5.6 | 51.7 | 46.7 | 65.4 | 40.9 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 52.1 | 85.1 | 10.4 | 52.4 | 75.9 | 5.6 | 51.7 | 46.7 | 65.4 | 40.9 | |
| Queue Length 50th (ft) | 146 | 205 | 0 | 135 | 186 | 0 | 126 | 630 | 82 | 480 | |
| Queue Length 95th (ft) | #239 | #362 | 61 | #234 | #324 | 29 | #262 | #749 | #213 | #568 | |
| Internal Link Dist (ft) | | 861 | | | 391 | | | 203 | | 296 | |
| Turn Bay Length (ft) | 250 | | 250 | 300 | | 100 | 600 | | 225 | | |
| Base Capacity (vph) | 318 | 295 | 386 | 300 | 292 | 362 | 283 | 2228 | 197 | 2011 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.78 | 0.90 | 0.41 | 0.77 | 0.84 | 0.29 | 0.83 | 0.98 | 0.86 | 0.89 | |
| Intersection Summary | | | | | | | | | | | |

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. #



APPENDIX F

Conceptual Site Plan

Kimley »Horn

096888037 Berkley Center Subdivision

